

# Ph1a Homework Solution 3

Fall 2009

Each homework problem is worth 5 points. Please disregard the point values listed on the problem itself. Use these instead.

## 3.1 QP3 (5 points)

### 3.1.a (0.5 points)

In terms of the lengths in the diagram, we have:

$$l_1 = (p_1 - x_1) + \pi R + (p_1 - p_2) = 2p_1 - x_1 - p_2 + \pi R$$

$$l_2 = p_2 + \pi R + (p_2 - x_2) = 2p_2 - x_2 + \pi R$$

### 3.1.b (1 point)

The free body diagrams are in Fig. 1.

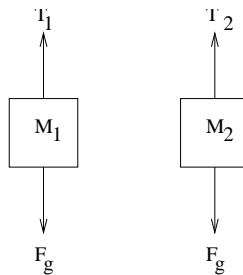


Figure 1: QP3.b

In the vertical direction, we have Newton's Laws:

$$m_1 a_1 = T_1 - m_1 g$$

$$m_2 a_2 = T_2 - m_2 g$$

### 3.1.c (1 point)

Taking two time derivatives of the equations in part a gives:

$$\frac{d^2 l_1}{dt^2} = 0 = -a_1 - \frac{d^2 p_2}{dt^2}$$

$$\frac{d^2 l_2}{dt^2} = 0 = 2 \frac{d^2 p_2}{dt^2} - a_2$$

From this, we get  $a_2 = -2a_1$ , or  $a_1 = k a_2$  where  $k = -\frac{1}{2}$ .

### 3.1.d (1 point)

We can get the relationship between the tensions by considering Newton's Laws applied to the (massless) 2<sup>nd</sup> pulley. For massless objects, the condition is that net force must be zero to avoid the unphysical result of infinite acceleration.

The force diagram is Fig. 2

$$m_{P2} a_{P2} = T_1 - 2T_2 - m_{P2} g$$

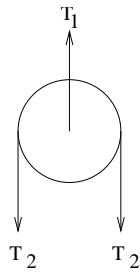


Figure 2: QP3.d

$$T_1 - 2T_2 = 0$$

So we get  $T_1 = 2T_2$ , or  $T_1 = k_2T_2$  with  $k_2 = 2$ .

**3.1.e (1 point)**

Solving for  $a_1$  and  $T_2$  is straight-forward:

$$T_2 = m_2 \left( \frac{a_1}{k} \right) + m_2g = m_2 \left( \frac{a_1}{k} + g \right)$$

$$m_1a_1 = (k_2T_2) - m_1g$$

$$m_1a_1 = m_2k_2 \left( \frac{a_1}{k} + g \right) - m_1g$$

$$a_1 = \frac{(m_2k_2 - m_1)kg}{km_1 - k_2m_2}$$

$$T_2 = \frac{m_1m_2g(k-1)}{km_1 - k_2m_2}$$

Using the correct values of  $k = -1/2$  and  $k_2 = 2$ , we get

$$a_1 = \frac{2m_2 - m_1}{m_1 + 4m_2}g \quad T_2 = \frac{3m_1m_2g}{m_1 + 4m_2}$$

Using the incorrect assumption of  $k = -1$  and  $k_2 = 1/3$ , we get

$$a_1 = \frac{m_2 - 3m_1}{3m_1 + m_2}g \quad T_2 = \frac{6m_1m_2g}{3m_1 + m_2}$$

**3.1.f (0.5 point)**

If  $m_1 = m_2$  the formula for  $a_2$  reduces to:

$$a_2 = \frac{a_1}{k} = \frac{(k_2 - 1)g}{k - k_2}$$

Thus  $a_2 = -\frac{2}{5}g$  (or  $a_2 = \frac{1}{2}g$  under the wrong assumption). The condition for no acceleration of the masses is that  $a_1$  (and hence  $a_2$  also) be zero.

$$a_1 = \frac{2m_2 - m_1}{m_1 + 4m_2}g = 0 \Rightarrow m_1 = 2m_2$$

Alternatively, under the wrong assumption:

$$a_1 = \frac{m_2 - 3m_1}{3m_1 + m_2}g = 0 \Rightarrow m_1 = \frac{1}{3}m_2$$

### 3.2 QP4 (5 points)

#### 3.2.a (1.5 points)

The free body diagrams are Fig. 3. The normal forces  $N_{ij}$  are the force of the  $i^{\text{th}}$  block on the  $j^{\text{th}}$  block, or just  $N_i$  for the force of the ground on block  $i$ .

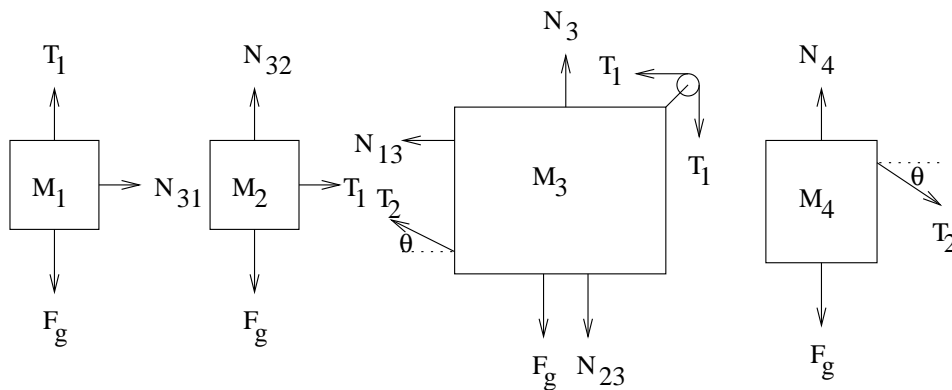


Figure 3: QP4.a

#### 3.2.b (1 point)

Newton's Second Law for  $m_1$  and  $m_2$ :

$$\begin{aligned} m_1 a_{1X} &= N_{31} & m_2 a_{2X} &= T_1 \\ m_1 a_{1Y} &= T_1 - m_1 g & m_2 a_{2Y} &= N_{32} - m_2 g \end{aligned}$$

#### 3.2.c (1 point)

Since there is no motion of  $m_2$  relative to  $m_3$ , we must have  $a_{2X} = a_{3X}$ . Also, we know  $a_{1Y} = 0$ . Thus:

$$\begin{aligned} T_1 &= m_1 g \\ a_{3X} = a_{2X} &= \frac{T_1}{m_2} = \frac{m_1}{m_2} g \end{aligned}$$

#### 3.2.d (0.5 points)

The whole system moves with the same horizontal acceleration,  $a = a_{3X}$ . The only external force is  $F$ , so we have:

$$\begin{aligned} F &= m_{\text{sys}} a_{\text{sys}} \\ F &= (m_1 + m_2 + m_3 + m_4) \frac{m_1}{m_2} g \end{aligned}$$

#### 3.2.e (0.5 points)

Newton's Second Law for  $m_4$  yields:

$$\begin{aligned} m_4 a_{4X} &= m_4 a = T_2 \cos \theta \Rightarrow T_2 = \frac{m_4 a}{\cos \theta} \\ m_4 a_{4Y} &= 0 = N_4 - m_4 g - T_2 \sin \theta \end{aligned}$$

$$N_4 = m_4 g + T_2 \sin \theta$$

$$N_4 = m_4 (g + a \tan \theta) = m_4 g \left( 1 + \frac{m_1}{m_2} \tan \theta \right)$$

**3.2.f (0.5 point)**

Since pulley is massless, the net force is zero. See Fig. 4.

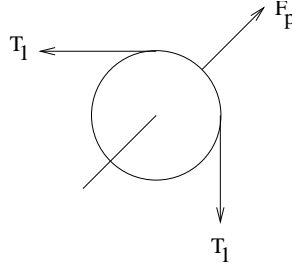


Figure 4: QP4.f

Clearly,  $\vec{F}_P = T_1(\hat{x} + \hat{y})$ . So  $|F_P| = \sqrt{2}T_1 = \sqrt{2}m_1g$ , and it is directed at  $\phi = \tan^{-1}[F_{PY}/F_{PX}] = 45^\circ$ .

### 3.3 Frautschi 7.16 (5 points)

#### 3.3.a (2 points)

Let  $\vec{F}_{12}$  be the gravitational force  $m_1$  feels because of  $m_2$ ,  $\vec{F}_{13}$  be the gravitational force  $m_1$  feels because of  $m_3$ , and  $\vec{F}_1 = \vec{F}_{12} + \vec{F}_{13}$  be the total force. Use the coordinate system as in the problem,

$$\begin{aligned}\vec{F}_{12} &= Gm_1m_2 \left( -\frac{1}{2}\hat{i} - \frac{\sqrt{3}}{2}\hat{j} \right) / a^2 \\ \vec{F}_{13} &= Gm_1m_3 \left( \frac{1}{2}\hat{i} - \frac{\sqrt{3}}{2}\hat{j} \right) / a^2 \\ \vec{F}_1 &= Gm_1 \left( (-m_2 + m_3)\hat{i} - \sqrt{3}(m_2 + m_3)\hat{j} \right) / 2a^2\end{aligned}$$

Similarly for  $m_2$ ,

$$\begin{aligned}\vec{F}_{21} &= Gm_2m_1 \left( \frac{1}{2}\hat{i} + \frac{\sqrt{3}}{2}\hat{j} \right) / a^2 \\ \vec{F}_{23} &= Gm_2m_3\hat{i} / a^2 \\ \vec{F}_2 &= Gm_2 \left( \left( \frac{m_1}{2} + m_3 \right)\hat{i} + \frac{\sqrt{3}}{2}m_1\hat{j} \right) / a^2\end{aligned}$$

and  $m_3$ ,

$$\begin{aligned}\vec{F}_{31} &= Gm_3m_1 \left( -\frac{1}{2}\hat{i} + \frac{\sqrt{3}}{2}\hat{j} \right) / a^2 \\ \vec{F}_{32} &= Gm_3m_2(-\hat{i}) / a^2 \\ \vec{F}_3 &= Gm_3 \left( \left( -\frac{m_1}{2} - m_2 \right)\hat{i} + \frac{\sqrt{3}}{2}m_1\hat{j} \right) / a^2\end{aligned}$$

#### 3.3.b (1.5 points)

Let the position of  $m_1$  be  $p_1$  and similarly for  $p_2$  and  $p_3$ . Call the point through which the axis should pass be  $Z$ , the center of mass of the whole system be  $M$ , and the center of mass of  $m_2$  and  $m_3$  be  $M_{23}$ . Notice that the three points,  $p_1$ ,  $M$ , and  $M_{23}$  must line up, so  $\overrightarrow{p_1M_{23}} // \overrightarrow{p_1M}$ .

Let the centripetal force of  $m_1$  be  $\vec{F}_1^c$ . We want to use the condition that  $\vec{F}_1^c$  is parallel with  $\vec{F}_1$ , denoted again by  $\vec{F}_1^c // \vec{F}_1$ , to find out where  $Z$  is. We can prove that  $Z=M$ , because we know for this special case the three masses are arranged equidistance to each other,

$$\frac{\vec{F}_1 // \overrightarrow{p_1M_{23}}}{\vec{F}_1^c // \overrightarrow{p_1Z}}$$

So that  $Z$  must lie on the line  $\overrightarrow{p_1M_{23}}$ .

Use similar reasoning for  $\overrightarrow{m_2}$  and  $\overrightarrow{m_3}$ , we conclude that  $Z$  must lie on both  $\overrightarrow{p_2M_{13}}$  and  $\overrightarrow{p_3M_{12}}$ . The intersection of the three lines,  $\overrightarrow{p_1M_{23}}$ ,  $\overrightarrow{p_2M_{13}}$ , and  $\overrightarrow{p_3M_{12}}$ , is the center of mass,  $M$ . So  $Z=M$ .

If you like, you can find the equation of the line  $p_1M$ , which has the slope of  $-\sqrt{3}\frac{m_2+m_3}{m_3-m_2}$ , as can be seen from the expression of  $\vec{F}_1$  in part(a), and it passes the point  $p_1 : (0, \frac{\sqrt{3}a}{2})$ . So

$$p_1M : y - \frac{\sqrt{3}a}{2} = -\sqrt{3}\frac{m_2+m_3}{m_3-m_2}x$$

Similarly for the equation of line  $p_2M$  and  $p_3M$ ,

$$p_2M : y = \sqrt{3} \frac{m_1}{m_1 + 2m_3} (x + a/2)$$

$$p_3M : y = -\sqrt{3} \frac{m_1}{m_1 + 2m_2} (x - a/2)$$

And the intersection is  $(\frac{a(m_3 - m_2)}{2(m_1 + m_2 + m_3)}, \frac{\sqrt{3}am_1}{2(m_1 + m_2 + m_3)})$

Later, in Chapter 11.3, we will recognize this as the center of mass.

### 3.3.c (1.5 points)

Let  $\vec{r}_M$  be the position vector of the center of mass and  $vecr_1$  be the position vector of  $m_1$ , then

$$\vec{F}_1^c = m_1 \omega^2 (\vec{r}_M - \vec{r}_1)$$

Using the  $x - y$  coordinate, we get

$$\vec{r}_M - \vec{r}_1 = \frac{a(m_3 - m_2)}{2(m_1 + m_2 + m_3)} \hat{i} + \frac{\sqrt{3}am_1}{2(m_1 + m_2 + m_3)} \hat{j} - \frac{\sqrt{3}a}{2} \hat{j},$$

So

$$\vec{F}_1^c = m_1 \omega^2 \left( \frac{a(m_3 - m_2)}{2(m_1 + m_2 + m_3)} \hat{i} + \left( \frac{\sqrt{3}am_1}{2(m_1 + m_2 + m_3)} - \frac{\sqrt{3}a}{2} \right) \hat{j} \right)$$

Since  $\vec{F}_1^c = \vec{F}_1$ , we can compare with the expression for  $\vec{F}_1$  in part(a) to get

$$\frac{\omega^2 a}{m_1 + m_2 + m_3} = \frac{G}{a^2}$$

Therefore,

$$\omega = \sqrt{\frac{G}{a^3} m_1 + m_2 + m_3}$$

The same answer should be derived from  $\vec{F}_i^c = \vec{F}_i$  for  $i = 2, 3$ .

## 3.4 Frautschi 7.17 (5 points)

### 3.4.a (1.5 point)

Let the tension at the lowest point be  $T_b$ , and it is positive when pointing inward, or upward in this case. Also let the mass be  $m$ , and the radius be  $r$ . We have

$$T_b - mg = m \frac{v^2}{r}$$

$$T_b = mg + m \frac{v^2}{r}$$

$$T_b = 0.5 \times (9.8 + 3^2/1) = 9.4 \text{ Newton}$$

### 3.4.b (1.5 point)

Let the tension at the top be  $T_t$  and it is positive when pointing inward, or downward in this case.

$$T_t + mg = m \frac{v^2}{r}$$

$$T_t = -mg + m \frac{v^2}{r}$$

Since it moves with constant speed, then  $T_b$  has a larger absolute value than  $T_t$ .

$$|T_b| > |T_t|$$

Therefore, the rod is more likely to break when the mass is at the bottom.

**3.4.c (2 point)**

If the rod remains under tension at the top, that means it is pointing inward, or downward. So  $T_t$  has to be positive.

$$\begin{aligned}T_t &= -mg + m\frac{v^2}{r} \geq 0 \\ \frac{v^2}{r} &\geq g \\ v &\geq \sqrt{rg} = \sqrt{1 \times 9.8} = 3.13\text{m/s}\end{aligned}$$

So the minimum speed is  $3.13\text{m/s}$