

Ae105 Final Presentation

AAReST:

Autonomous Assembly of a Reconfigurable Space Telescope

1 June 2015

AAReST Mission Overview

Manan Arya

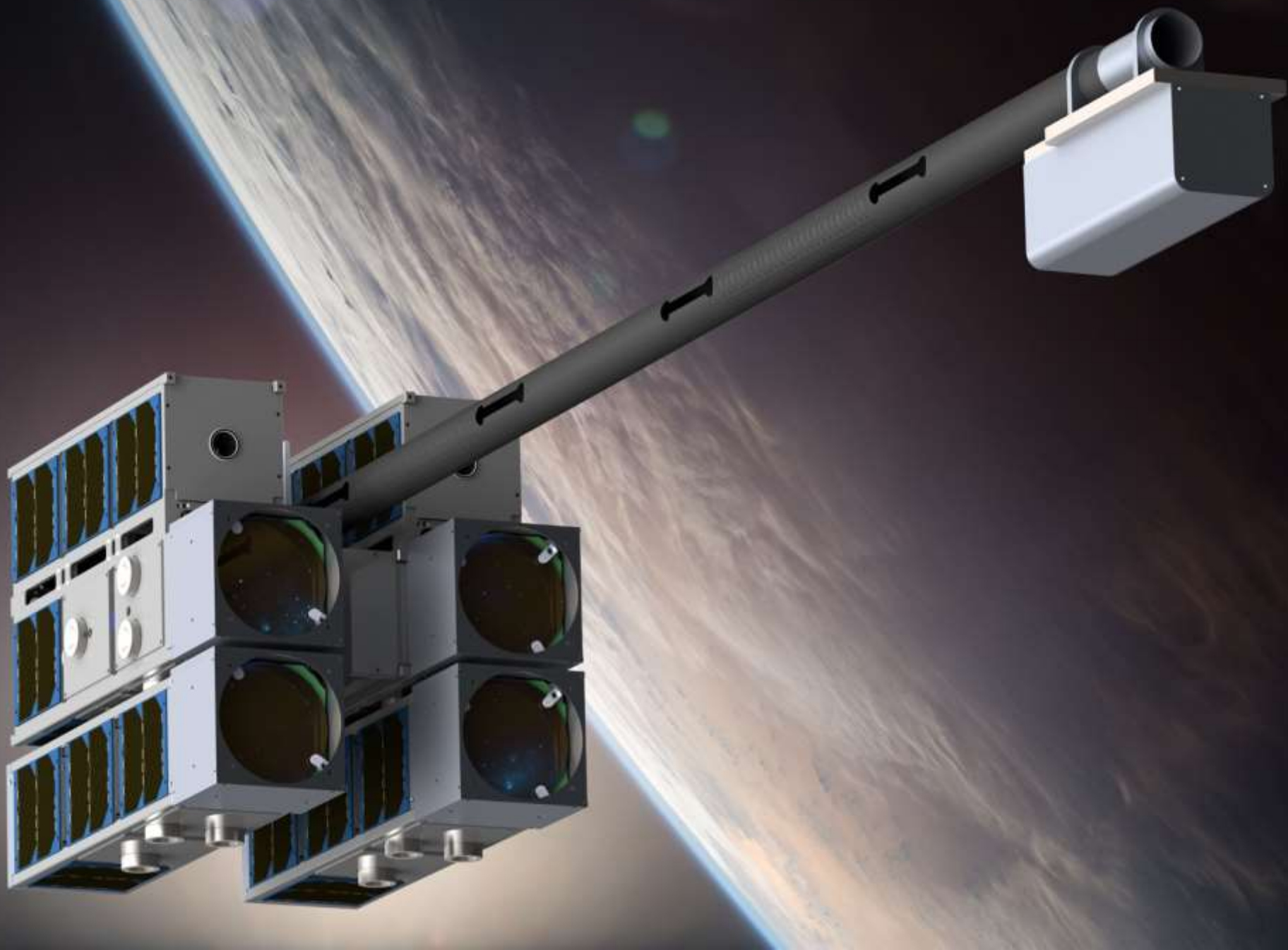
Building Large Space Telescopes

- Mirror dia. of current and planned space telescopes limited by constraints of a single launch
 - Hubble (1990): Ø 2.4 m
 - JWST (2018): Ø 6.5 m
 - ATLAST (2020+): Ø 8-16 m
- New paradigms needed for Ø 30 m+ segmented primary:
 - Autonomous assembly in orbit
 - Active ultralight mirror segments
- Active mirrors relax tolerances for assembly and manufacturing, correct thermal distortions
- Modular, robust, low-cost architecture



AAReST Objectives

- Demonstrate key technologies:
 - Autonomous assembly and reconfiguration of modular spacecraft carrying mirror segments
 - Active, lightweight deformable mirrors operating as segments in a primary
- Operate for as long as necessary to accomplish the objectives (~90 days)
- Gather engineering data to enable development of the next system



AAReST Spacecraft



AAReST Spacecraft

CoreSat

Power, Comm., Telescope ADCS

U. of Surrey



AAReST Spacecraft

MirrorSat (x2)

Reconfigurable free-flyers
U. of Surrey

CoreSat

Power, Comm., Telescope ADCS
U. of Surrey



AAReST Spacecraft

MirrorSat (×2)

Reconfigurable free-flyers
U. of Surrey

CoreSat

Power, Comm., Telescope ADCS
U. of Surrey

Deformable Mirrors (×2)

Active mirror segments
Caltech



AAReST Spacecraft

MirrorSat (x2)

Reconfigurable free-flyers
U. of Surrey

CoreSat

Power, Comm., Telescope ADCS
U. of Surrey

Reference Mirrors (x2)

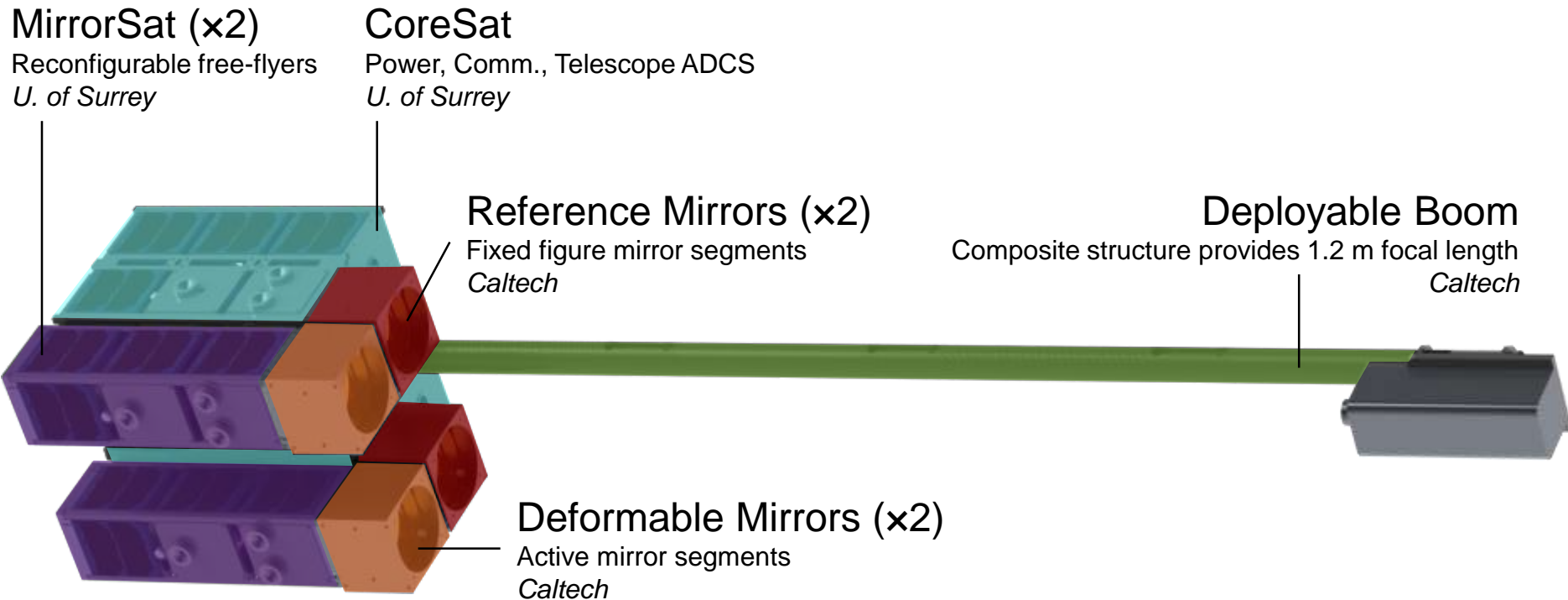
Fixed figure mirror segments
Caltech

Deformable Mirrors (x2)

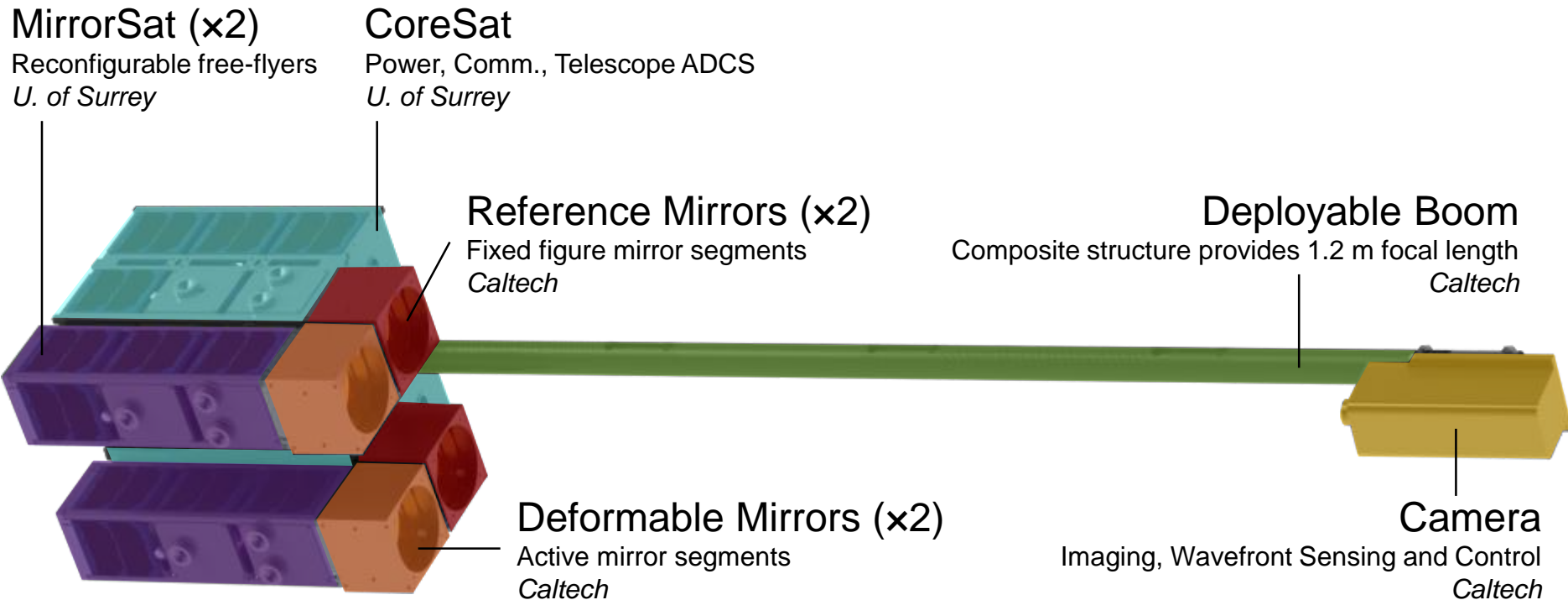
Active mirror segments
Caltech



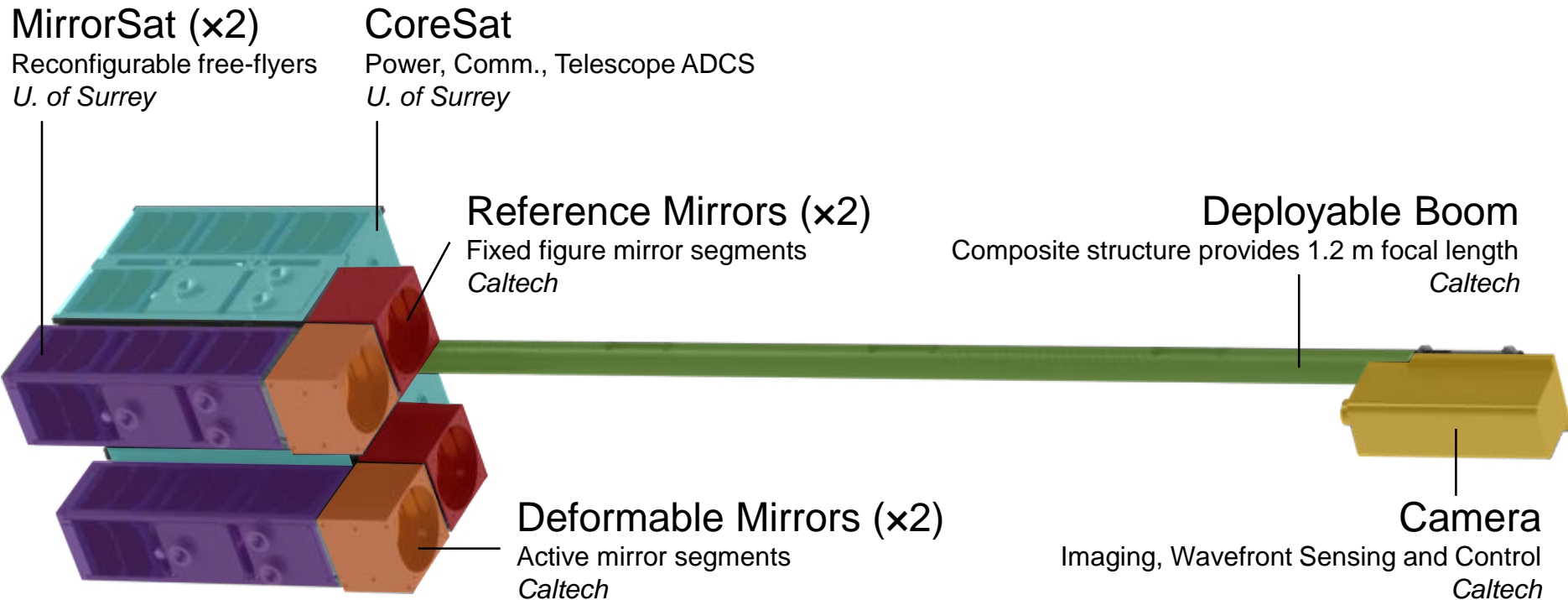
AAReST Spacecraft



AAReST Spacecraft



AAReST Spacecraft



Mass: <40 kg
 CoreSat: 20 × 30 × 35 cm
 MirrorSat: 10 × 10 × 30 cm
 Boom: Ø 38 mm, 1.5 m long

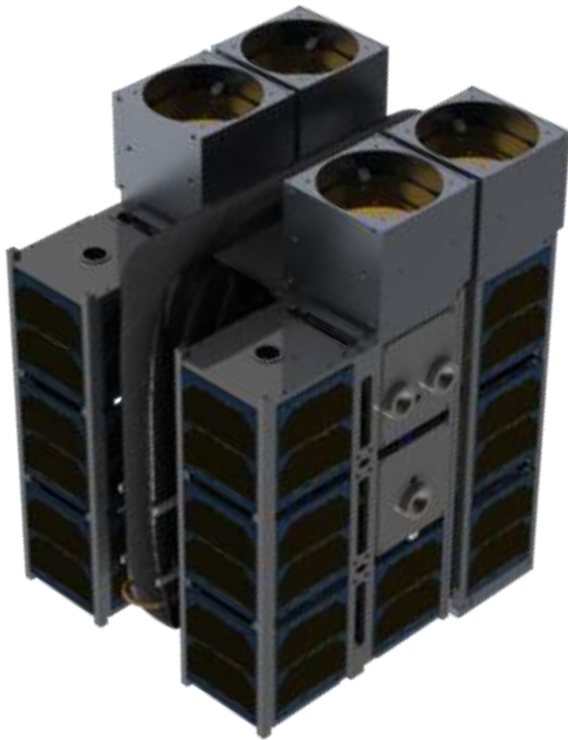
Prime focus telescope
 465 nm – 615 nm bandpass
 0.3 deg. field of view
 1.2 m focal length

UHF down (9600 bps)
 VHF up (1200 bps)
 S-Band ISL

Ref. orbits:
 ~650 km SSO
 ISS (400 km,
 52 deg. incl.)

Concept of Operations

1. Launch	2. Telescope Deployment	3. Telescope Calibration & Imaging	4. Reconfiguration	5. Telescope Recalibration & Imaging	6. Extended Mission
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Launch in a compact, stowed volume

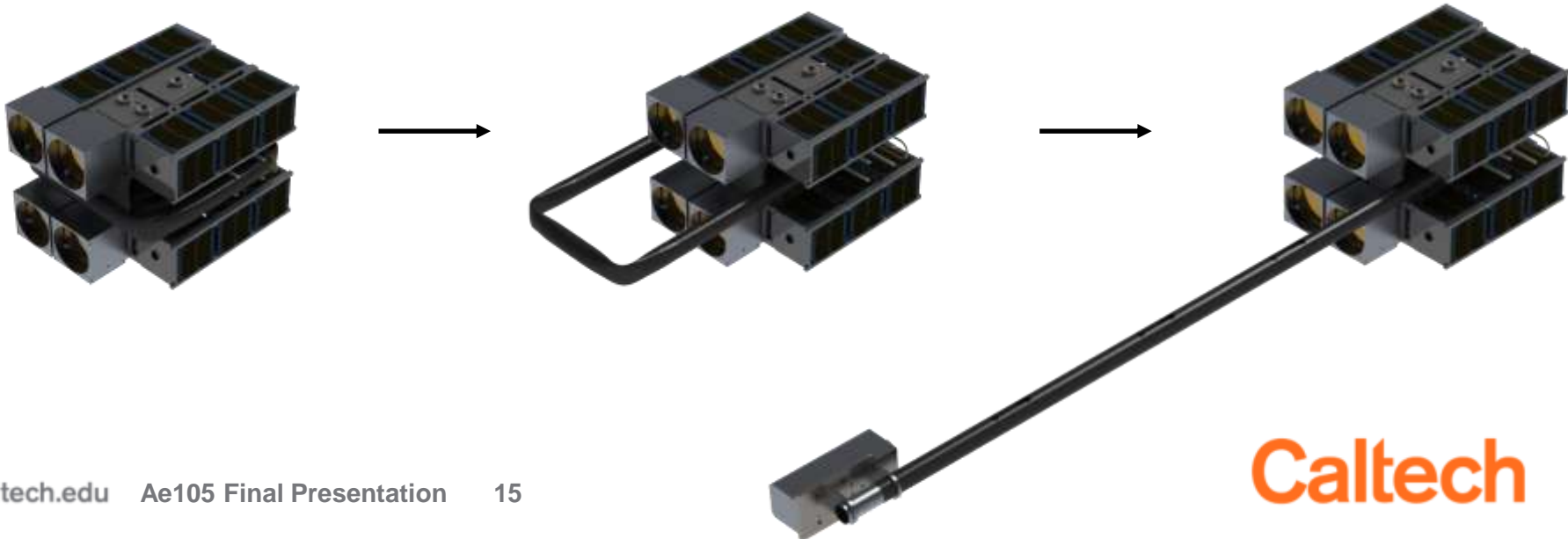
- 30 cm × 35 cm × 45 cm

Concept of Operations

1.	2.	3.	4.	5.	6.
Launch	Telescope Deployment	Telescope Calibration & Imaging	Reconfiguration	Telescope Recalibration & Imaging	Extended Mission

- Turn on, verify satellite components
- Stabilize attitude, temperature

- Deploy boom in two stages:
 1. Boom segments unfold
 2. Camera is released
- Uncage deformable mirrors



Concept of Operations

1.	2.	3.	4.	5.	6.
Launch	Telescope Deployment	Telescope Calibration & Imaging	Reconfiguration	Telescope Recalibration & Imaging	Extended Mission

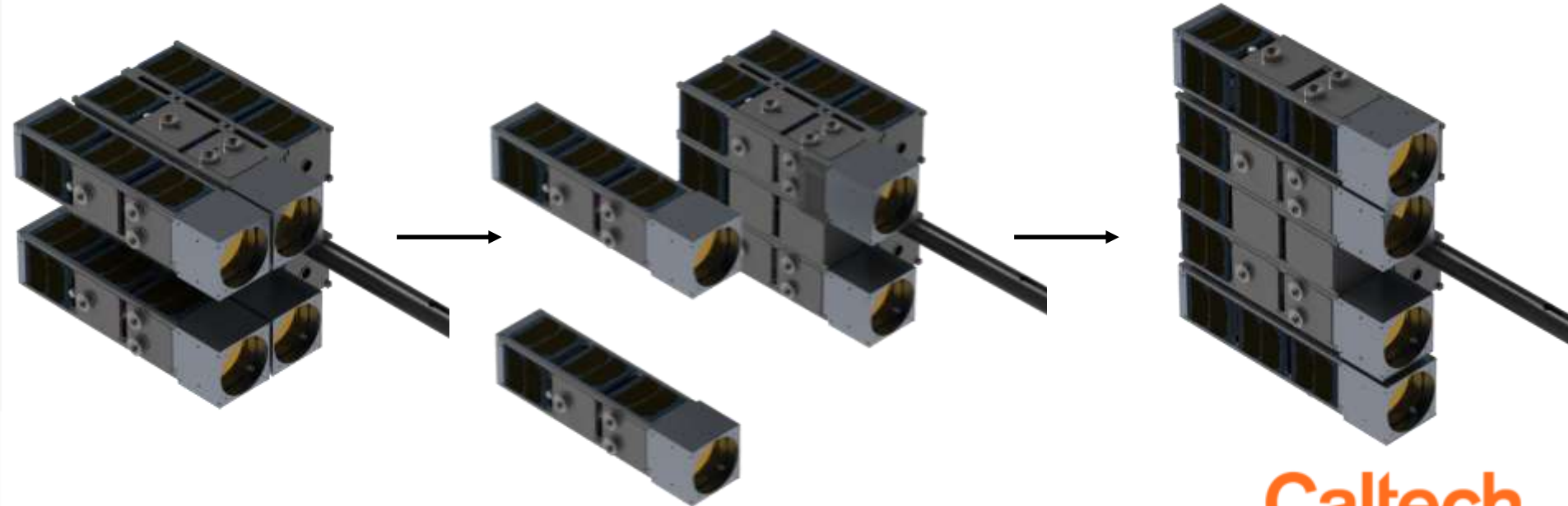


- Telescope points to a bright reference star
- Calibrate:
 - Segment tip/tilt/piston
 - Deformable mirror surface figure
- Camera provides feedback for segment calibration

Concept of Operations

1.	2.	3.	4.	5.	6.
Launch	Telescope Deployment	Telescope Calibration & Imaging	Reconfiguration	Telescope Recalibration & Imaging	Extended Mission

- MirrorSats release from CoreSat (one at a time)
- Fly out ~1 m
- Re-dock into “wide” configuration



Concept of Operations

1.	2.	3.	4.	5.	6.
Launch	Telescope Deployment	Telescope Calibration & Imaging	Reconfiguration	Telescope Recalibration & Imaging	Extended Mission



- Telescope points to a bright reference star
- Calibrate:
 - Segment tip/tilt/piston
 - Deformable mirror surface figure
- Camera provides feedback for segment calibration

Concept of Operations

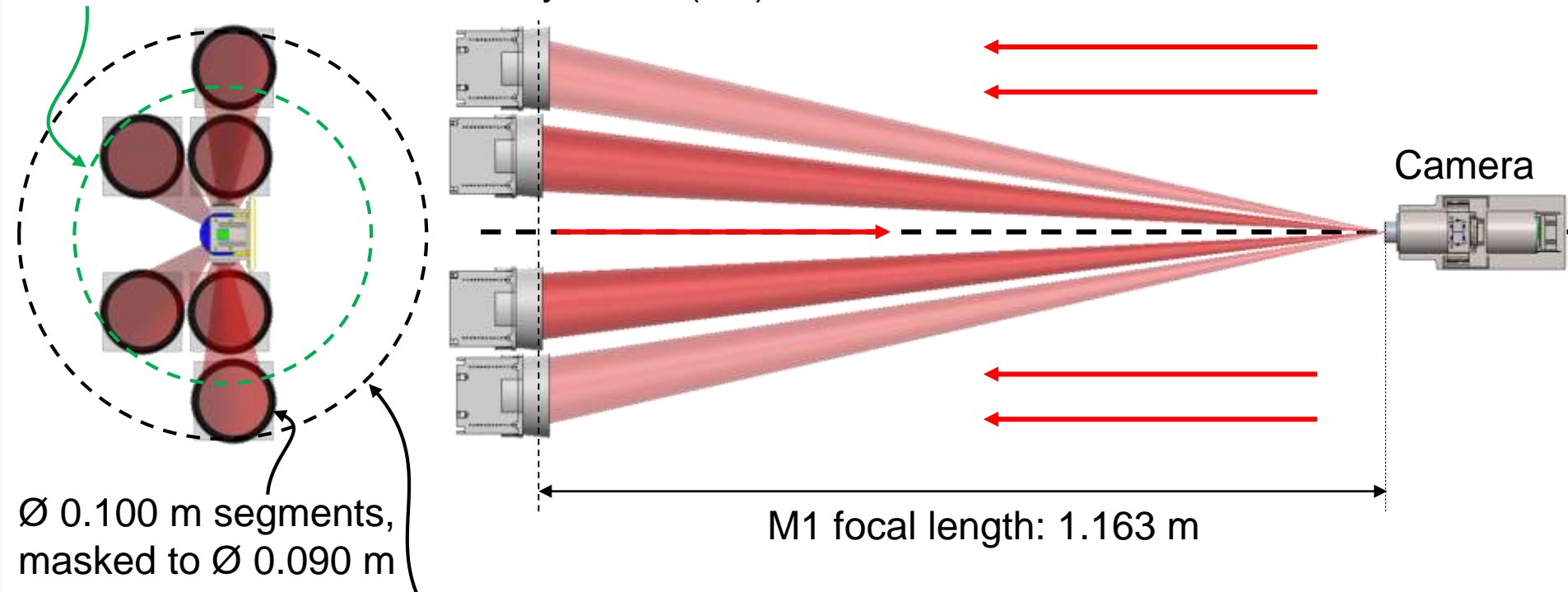
1. Launch	2. Telescope Deployment	3. Telescope Calibration & Imaging	4. Reconfiguration	5. Telescope Recalibration & Imaging	6. Extended Mission
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- Co-align star images from different segments to improve SNR
 - Pre-cursor to co-phasing
- Produce images of extended sources (e.g. Moon, Earth) for outreach

AAReST Optical Overview

Ø 0.405 m aperture
(narrow), $f/D = 2.87$

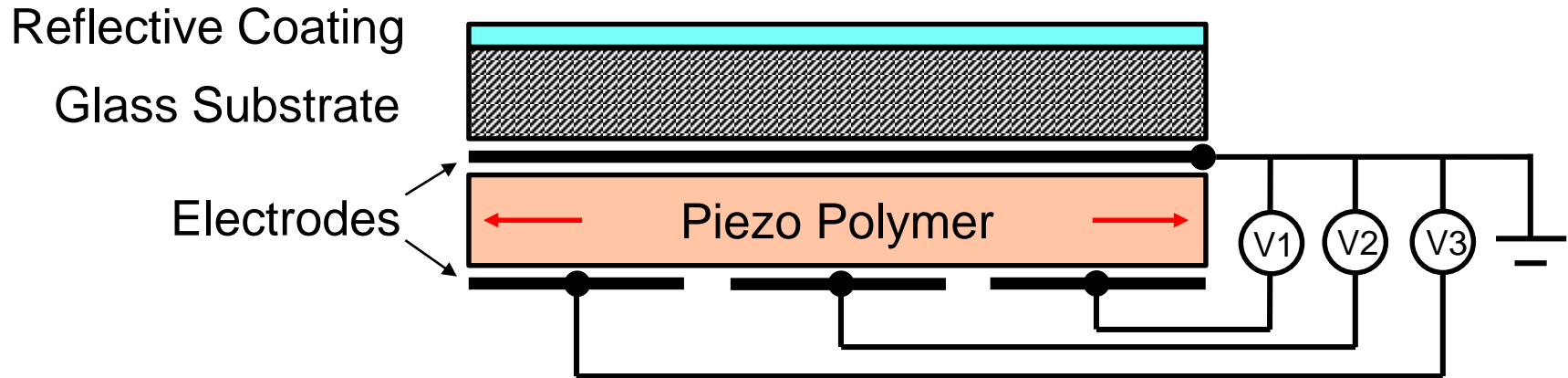
Primary Mirror (M1)



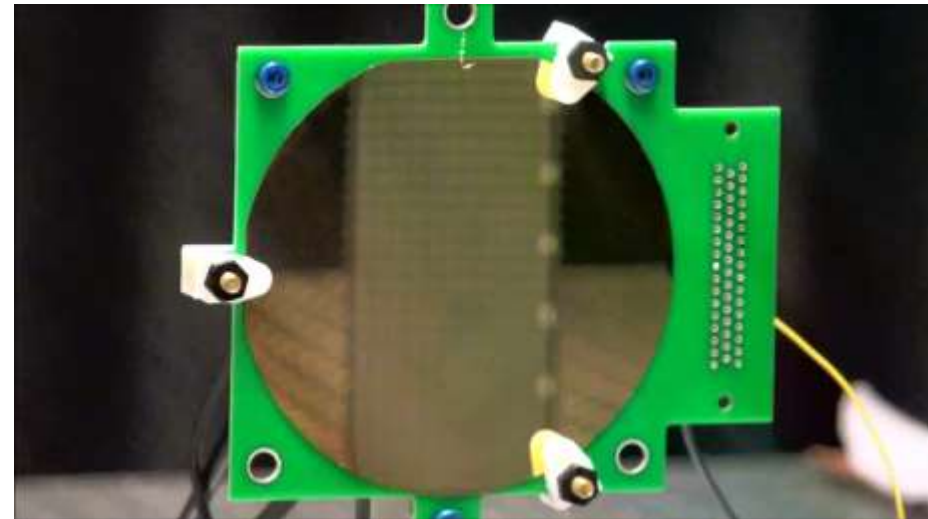
Ø 0.530 m aperture
(wide), $f/D = 2.19$

- Full Field of View : 0.3°
- Optical bandwidth: 465-615 nm (540 nm center)

Deformable Mirror Overview



- Thin active laminate
 - Polished glass wafer
 - Piezoelectric polymer backside
 - Reflective front surface
- Surface-parallel actuation
- Custom electrode pattern



AAReST History

2008 November: Large Space Apertures KISS workshop

2010 June: Ae105

- Initial mission design; mission requirement definition

2011 June: Ae105

- Spacecraft configuration revision: prime focus design
- Docking testbed commissioning

2012 June: Ae105

- Composite boom design and experiments
- Reconfiguration and docking experiments

2012 September: Mission Concept Review

2012 October: Division of responsibilities

- Surrey: Reconfiguration and docking
- Caltech: Deformable mirror and telescope payload

2013 June: Ae105

- Detailed camera design
- Thermal modeling

2013 September: Preliminary Design Review

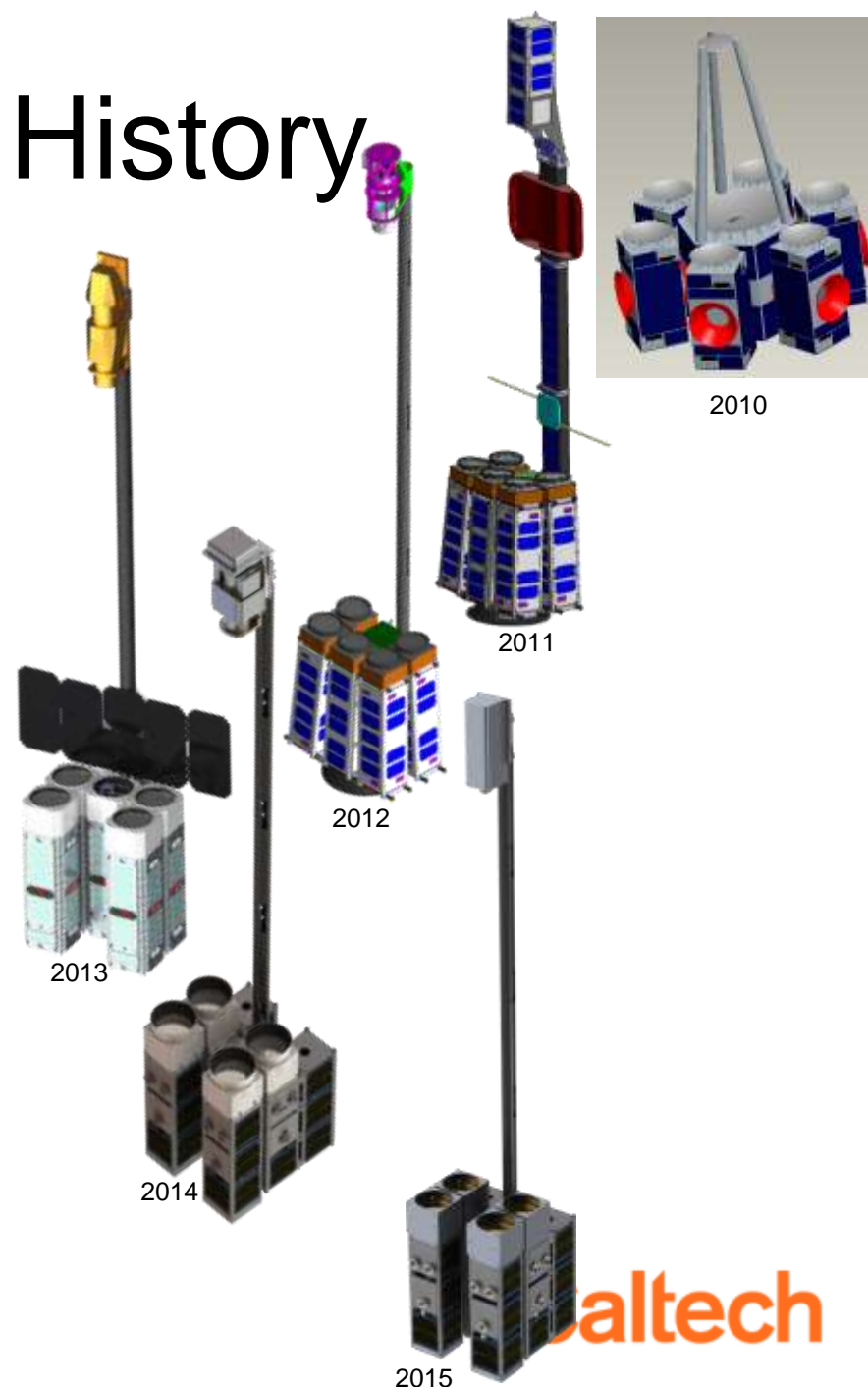
2014 June: Ae105

- Camera opto-mechanical prototype
- Boom gravity offload deployment testing
- Mirror vibro-acoustic experiments
- TVAC chamber commissioning
- Telescope testbed commissioning

2014 September: Detailed Design Review

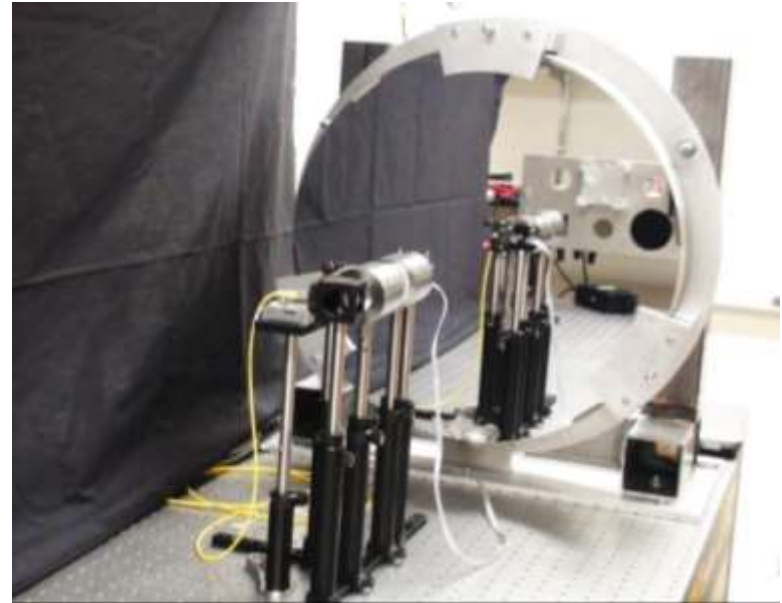
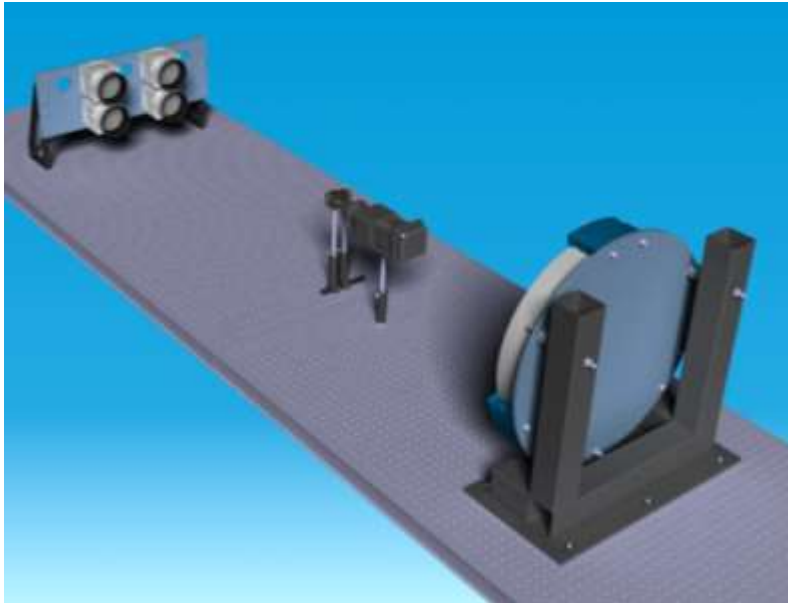
2015 June: Ae105

- Engineering models/prototypes of boom, camera
- Mirror thermal characterization
- Software and algorithms prototyping and testing

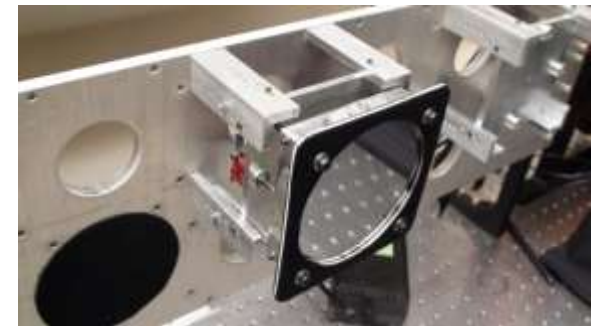


2014 Ae105 Accomplishments

Telescope Testbed Commissioning



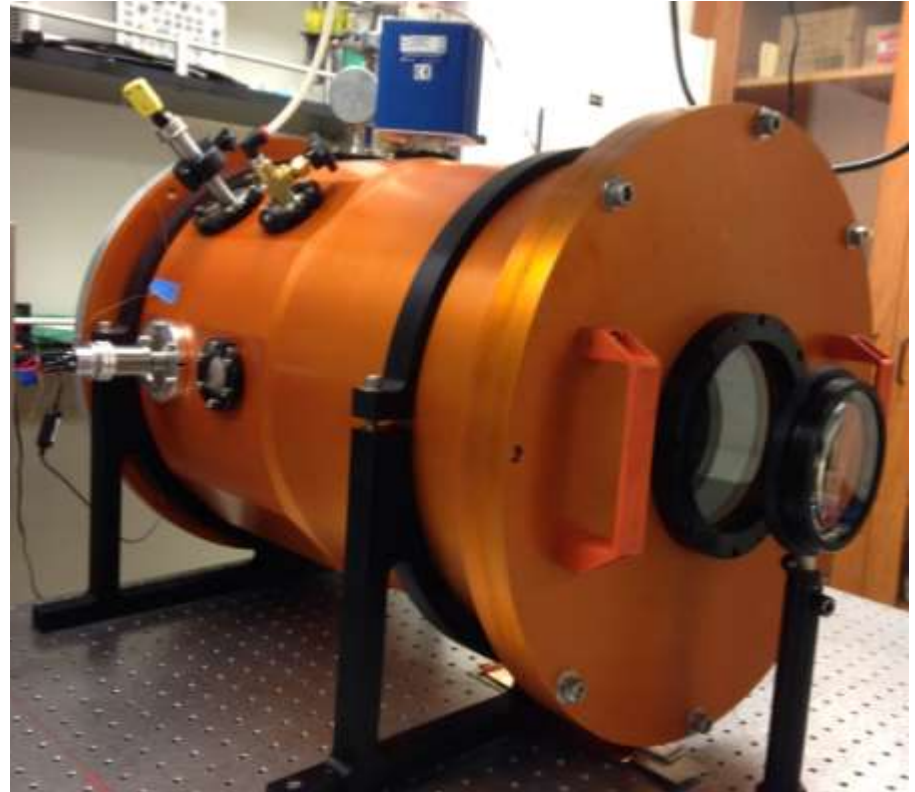
- Full-scale telescope testbed
- Autocollimation to simulate incoming starlight
- To test mirror + camera hardware, and calibration software



2014 Ae105 Accomplishments

TVAC Chamber Commissioning

- Need deformable mirrors to be thermally balanced
- Built a TVAC chamber to study mirror thermal deformations
- Optical window allows mirror figure to be measured at all times



2014 Ae105 Accomplishments

Boom Stage 2 Gravity Offload Testing



Presentation Outline

1. Boom Subsystem Validation
 - Stage 1 deployment testing & long-term storage effects
2. Mirror Thermal Deformation Testing
 - Designing a thermally balanced mirror segments
3. Mirror Box Mechanical Design
 - Designing mirror mounting and launch restraint systems
4. Camera Prototyping
 - Opto-mechanical prototype manufacturing and testing
5. Mirror Calibration Algorithms
 - Mirror segment search, pointing, and surface figure control
6. On-Board Software
 - Telescope software architecture design and implementation
 - 15 min. presentations + 5 min. discussion

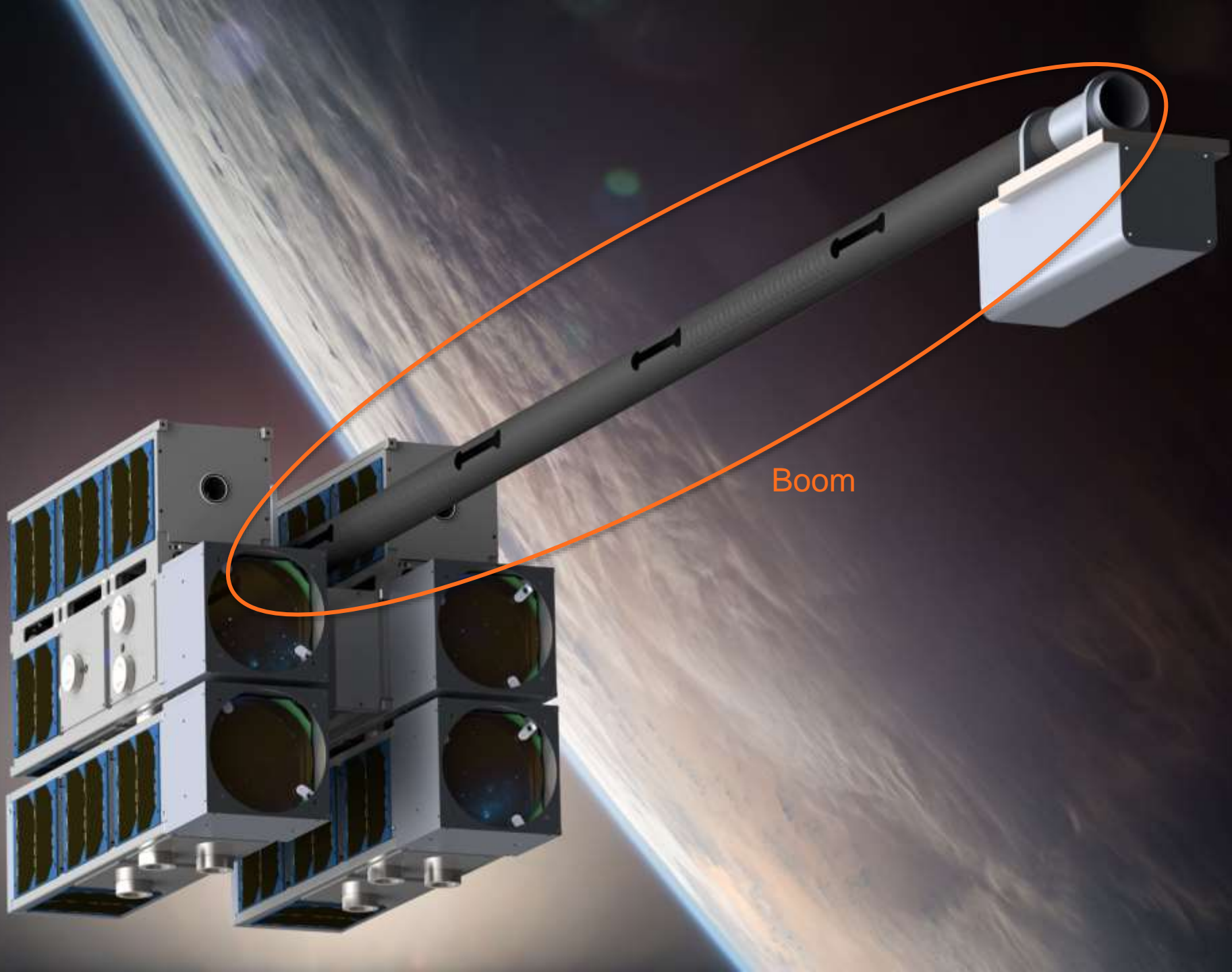
Boom Subsystem Validation

Serena Ferraro

Christophe Leclerc

Kirsti Pajunen

Mentor: Arturo Mateos



Boom

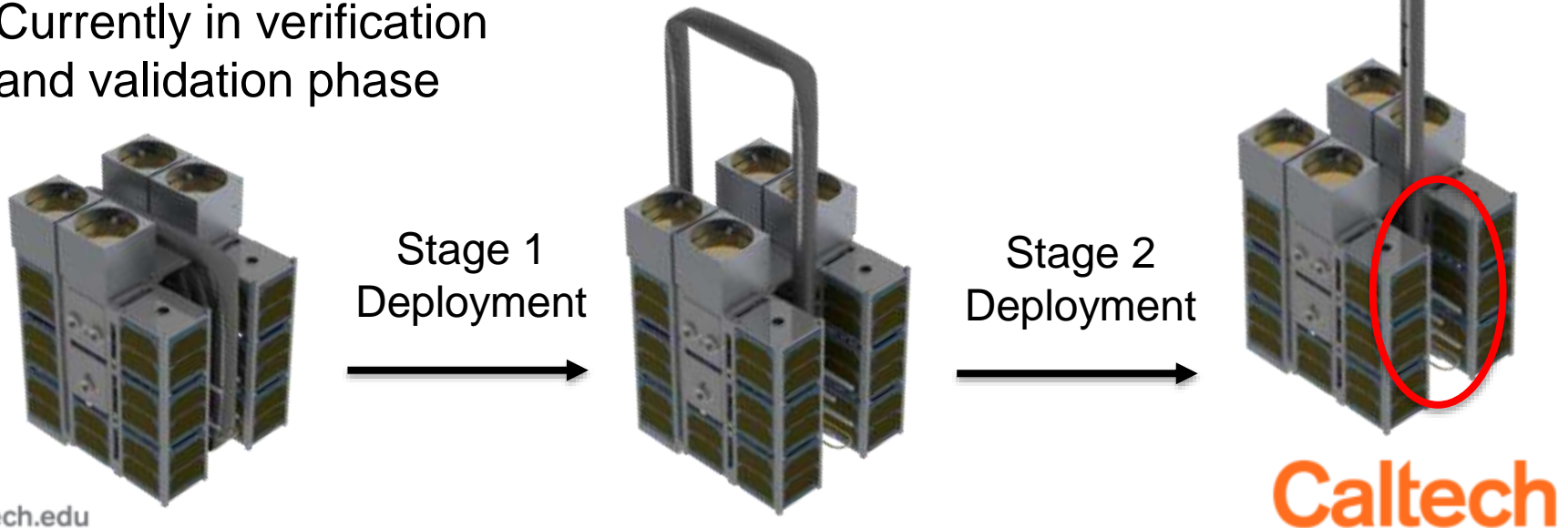
Boom Subsystem Overview

Purpose:

- Guarantee successful deployment of the composite boom
- Ensure alignment of optical systems after deployment

Team Responsibilities:

- Evaluate deployment sequence
- Design and test boom and boom-CoreSat interfaces
- Currently in verification and validation phase

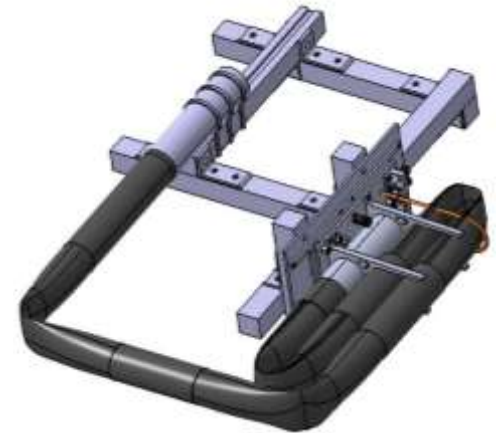
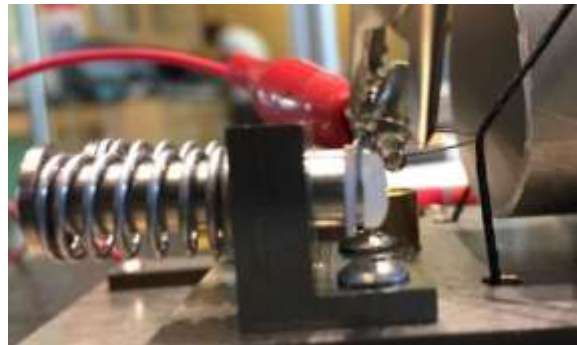


Tasks



1. Long-term storage behavior characterization

2. Manufacturing and testing of Boom-CoreSat Interfaces
(kinematic mount and separation device)



3. Stage 1 deployment experiments

Long-term Storage Behavior

Objective: Ensure boom retains sufficient potential energy for deployment after long-term storage

- Composite: AstroQuartz, carbon fiber, and cyanate ester resin
- Cyanate ester resin was selected due to low moisture absorption and outgassing

Approach:



Manufacture hinges
[$\pm 45_{AQ}$ / 0_{3CF} / 90_{CF} / $\pm 45_{AQ}$]



Characterize viscoelastic properties and perform accelerated aging tests



Examine mechanical response

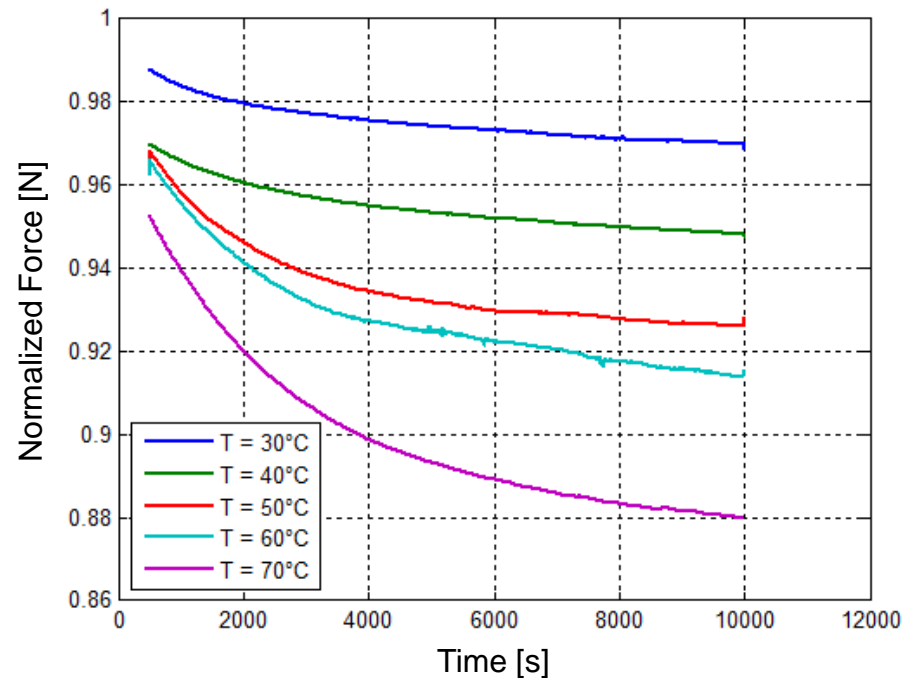
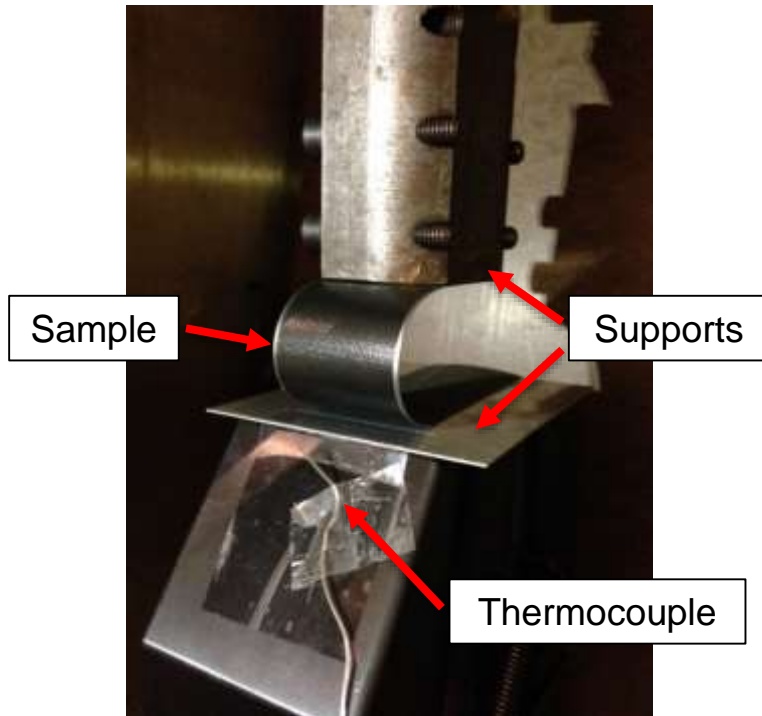
Long-term Storage Behavior

Viscoelastic Properties

Test Method:

- Sample buckled and positioned inside a preheated thermal chamber
- Supports kept at fixed distance to simulate stored radius of curvature
- Reaction force exerted by the sample measured with load cell

Results: Obtained force-time relations over chosen range of temperatures, examine the time-temperature superposition for this specific composite and generate a master curve



Long-term Storage Behavior

Viscoelastic Properties

How did we obtain a master curve?

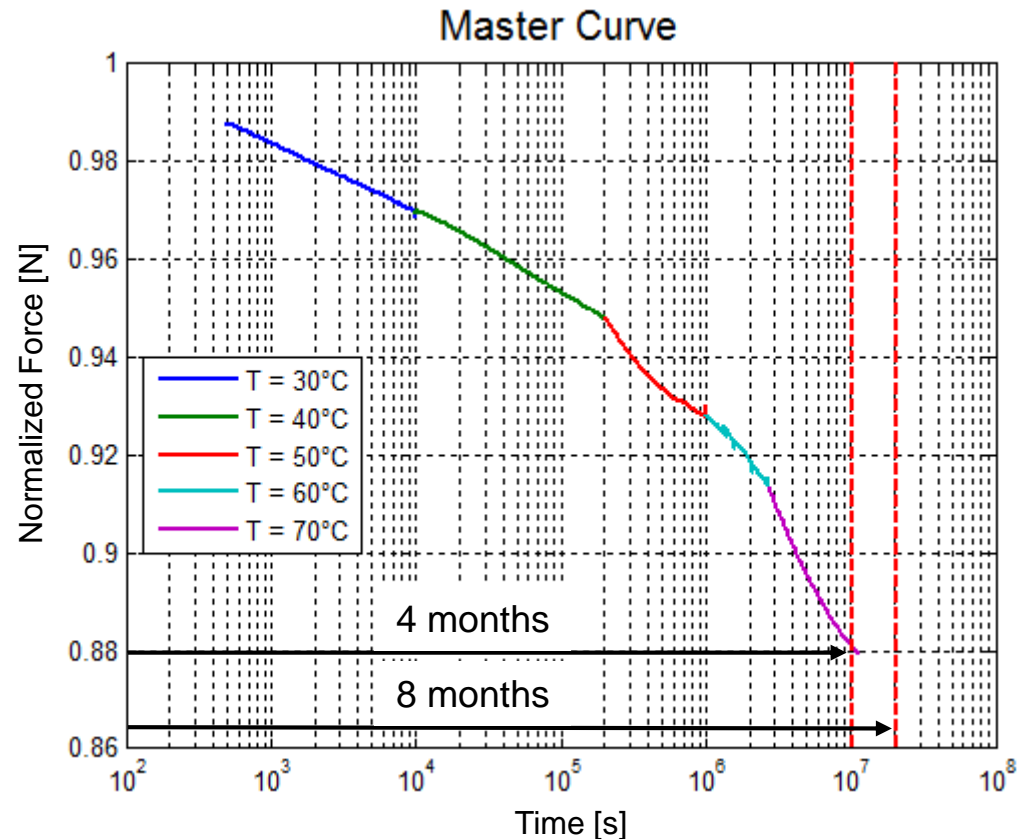
- Experimental curves shifted on a logarithmic time scale with respect to reference curve at 30°C

Why is the master curve useful?

- Samples need to be aged 157 minutes at 70 °C in order to reach 4 months of storage time
- Expect **~10%** decrease in reaction force

What can be observed?

- Only 10 more minutes of aging at 70 °C would correspond to 8 months of storage time
- From curve trend, 8 months storage would lead to ~12% total decrease in reaction force



Long-term Storage Behavior

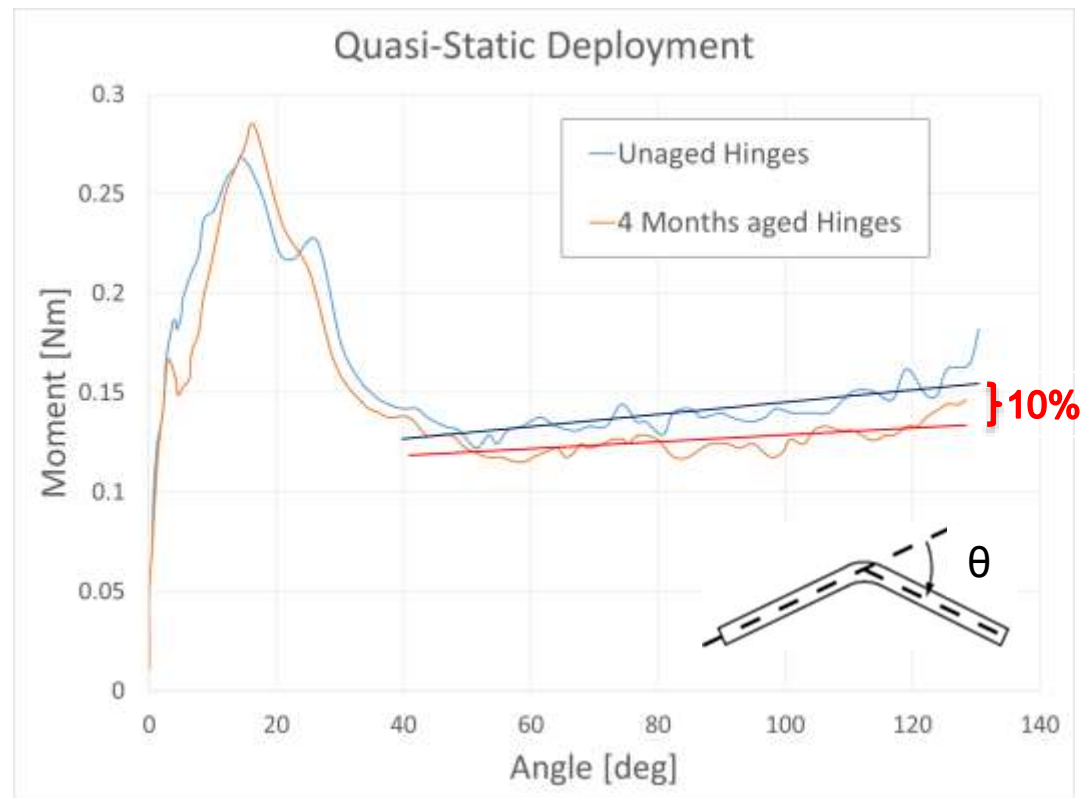
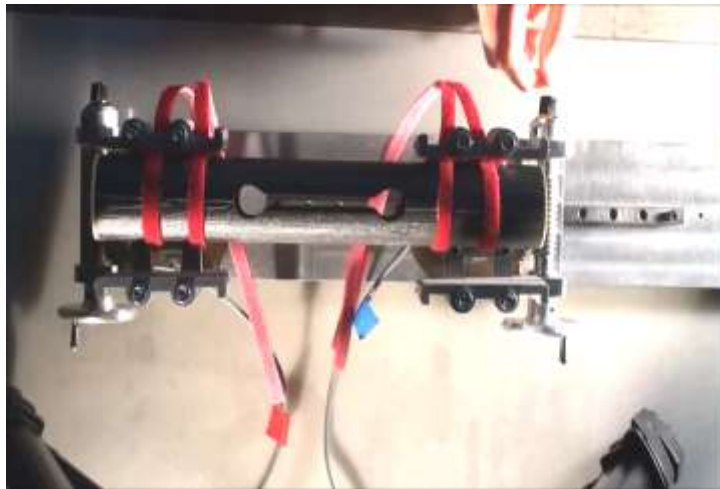
Mechanical Response

Objective: Measure the moment exerted by the hinge with respect to the hinge configuration, which is determined by its angle

Results: ~10% decrease in moment if behavior at the peak is neglected

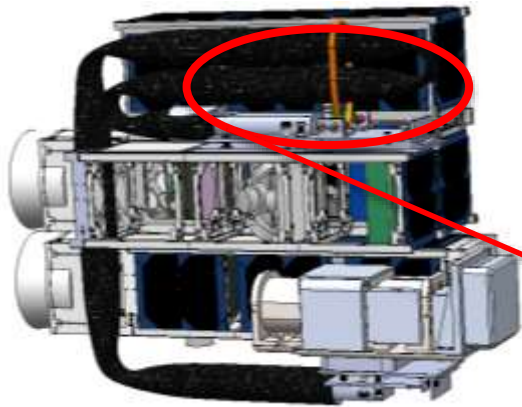
Conclusions:

- Quasi-static deployment test confirms master curve prediction
- Reduced moment did not prevent successful hinge deployment
- Information obtained from this test and master curve indicates that longer storage time will not compromise hinge deployment



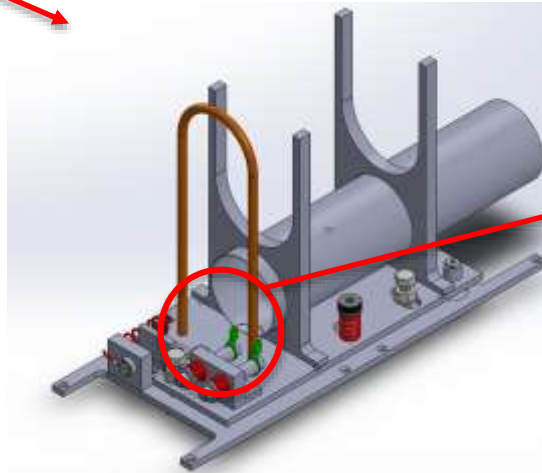
Boom-CoreSat Interfaces

Objective: Validate last year's designs through manufacturing and testing & suggest improvements

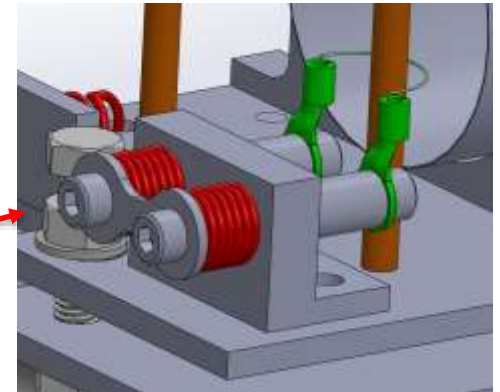


Kinematic Mount allows adjustment of camera relative to CoreSat before final storage

- Corrects for misalignments



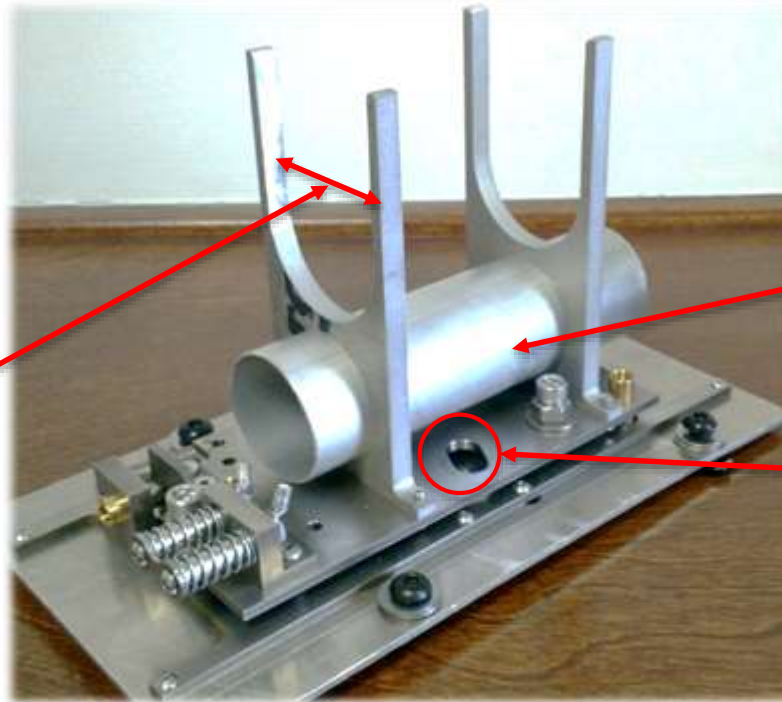
Separation Device constrains boom during storage and releases stage 1 during deployment



Boom-CoreSat Interfaces: Manufacturing

- Manufactured first prototypes from existing designs
- Some modifications were necessary in order to be tested:

Wider brackets to allow boom storage and deployment



Addition of **set screws** to fix the mandrel

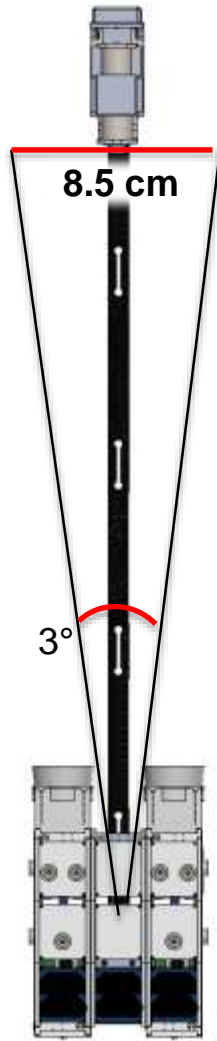
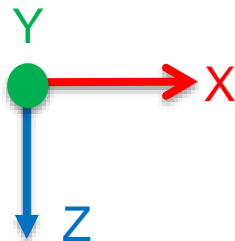
Larger slots to obtain adjustment range

Boom-CoreSat Interfaces: Testing

Kinematic Mount

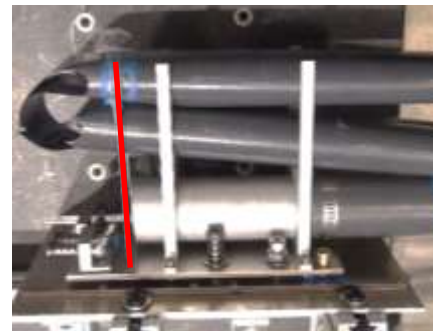
Axis	Degrees of Rotation	Camera Lens Displacement
x	4°	11.3 cm
y	3°	8.5 cm
z	6°	1.0 cm

- More than enough adjustability in all 3 axes of rotation

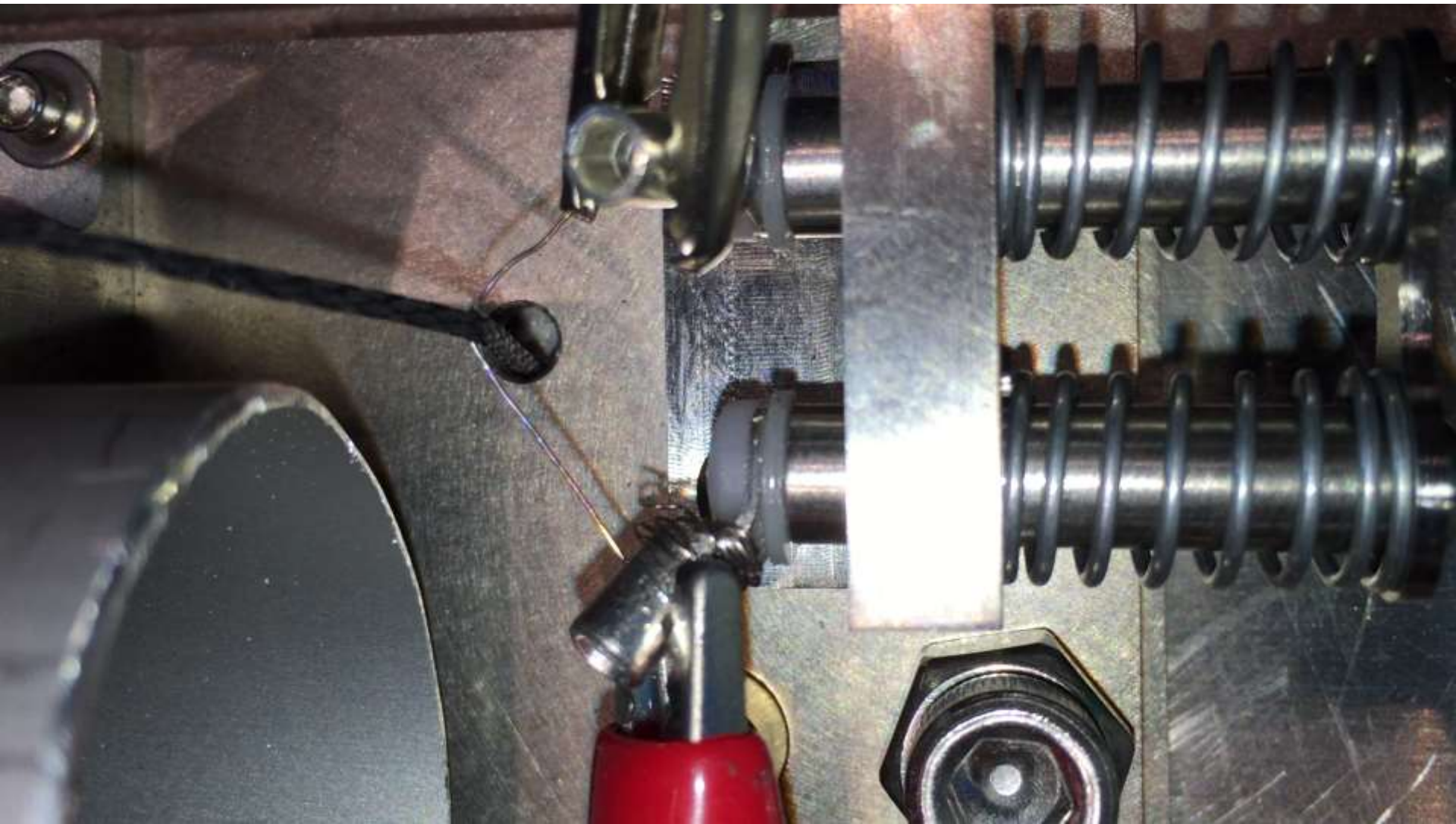


Separation device

- Ran multiple trials at various currents
- Several Vectran configurations and tensions (need angled cable)
- 9 sec** cut time for **1.6 A**
- Tension does not affect cutting time
- Reliable:** no failure in 26 tests



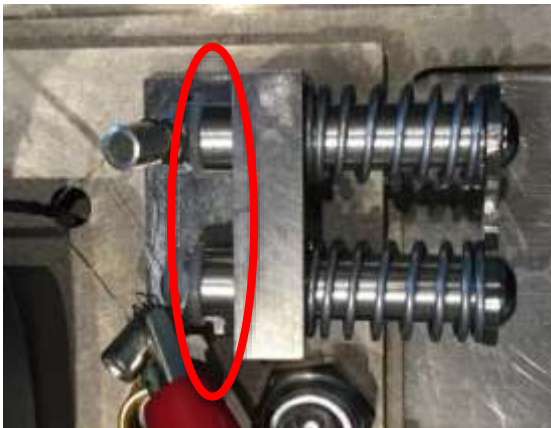
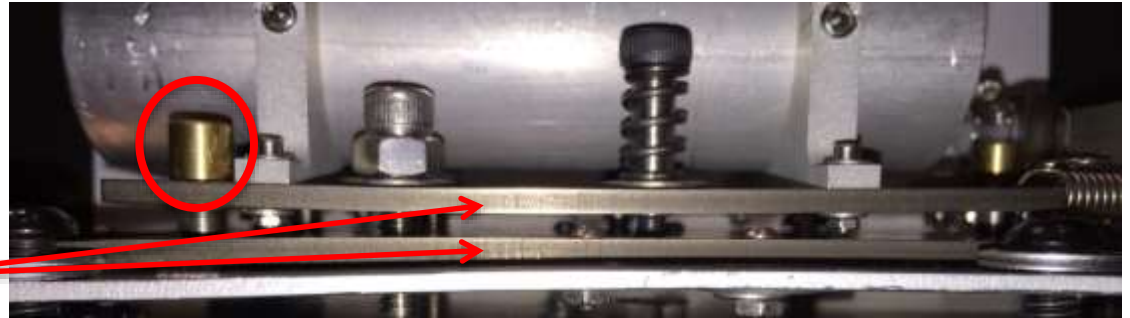
Separation Device Testing



Boom-CoreSat Interfaces: Future Improvements

Kinematic mount

- Placement of the Vectran cable
- Resolution of plate bending issue
- Attachment of boom on mandrel



Separation device

- Larger displacement is required to maintain tension
- Addition of redundancy

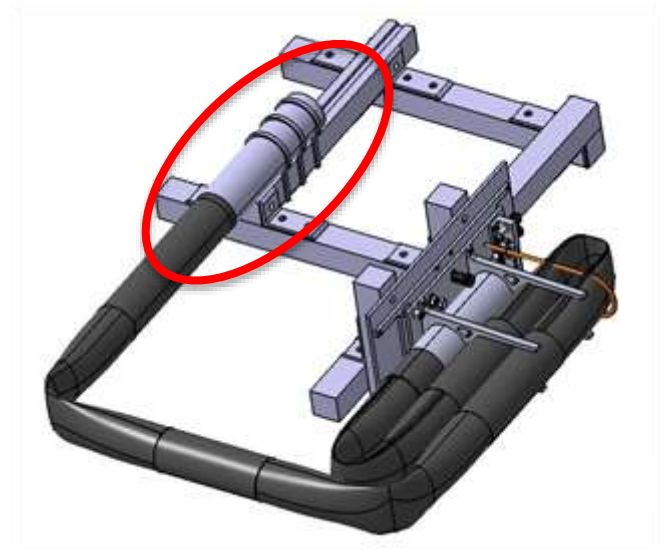
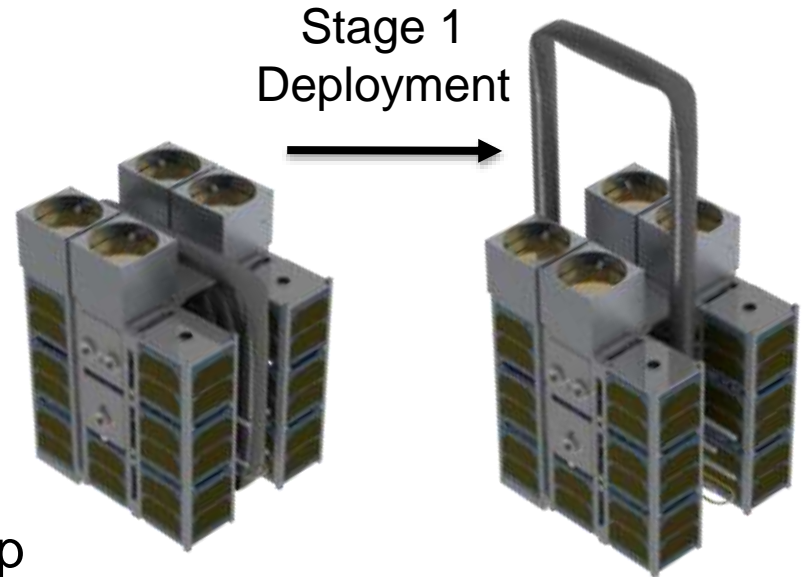
Stage 1 Deployment Test

Motivation:

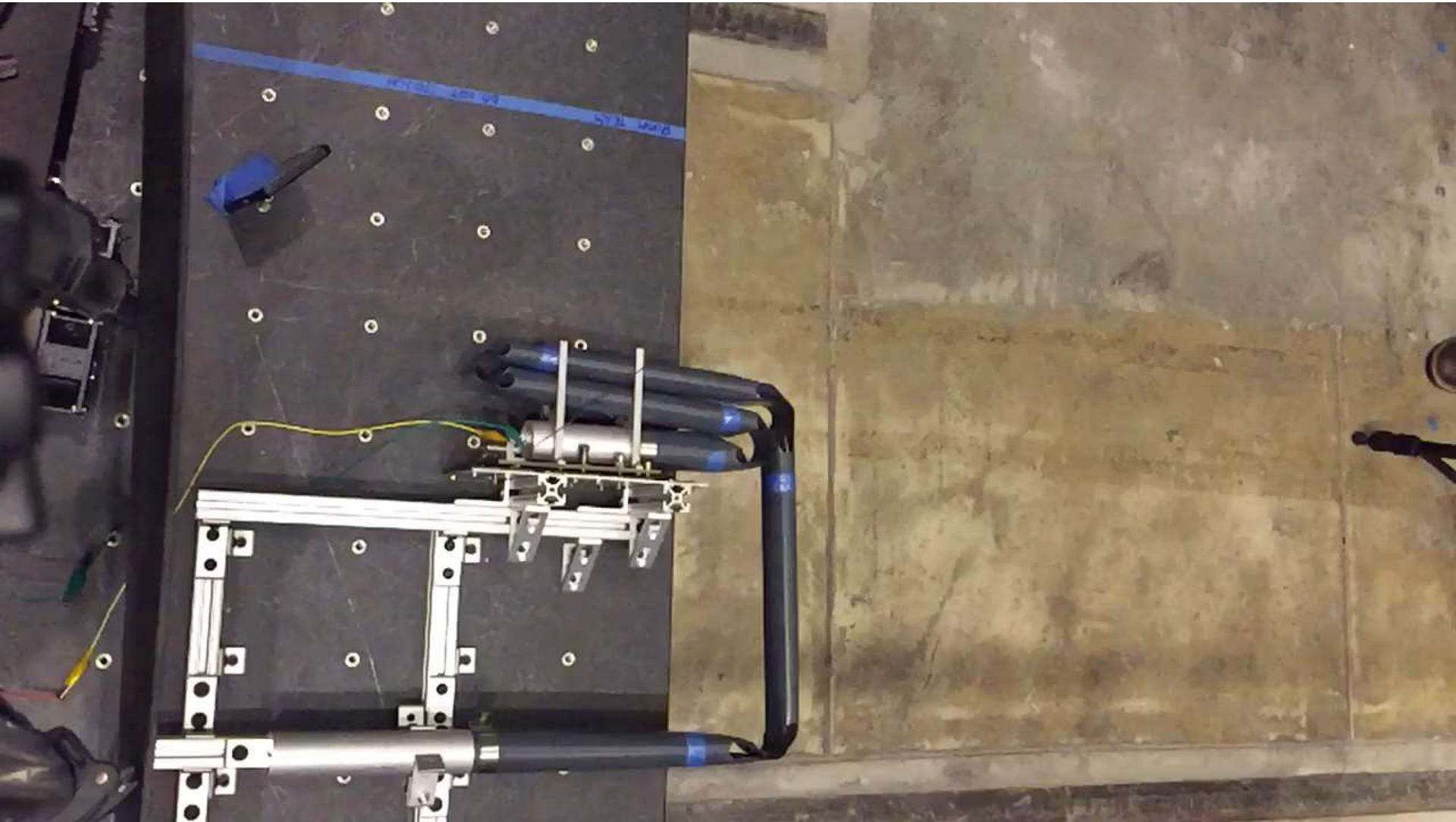
Ensure reliable and repeatable stage 1 deployment during which the boom follows the prescribed trajectory

Objectives:

- Design and build a highly modular setup
 - Possibility to add boom-camera interface
- Validate stage 1 deployment kinematics
- Validate kinematic mount
- Test separation device
- Find final position of stage 1 deployment



Stage 1 Deployment Test: Video 1



Stage 1 Deployment Test: Video 2



Stage 1 Deployment Test: Results

- **Repeatable** initial condition obtained for stage 2 deployment experiments
- Small lateral deflection occurred due to previous geometric optimization
 - Bending moment of **15 Nm** exerted on camera-CoreSat interface
 - Experimental setup more rigid than final boom-camera interface
- Boom-CoreSat interfaces worked as expected



Summary of Completed Work

Long-Term Storage

- Generated a master curve for cyanate ester resin
- Moment exerted by hinges decreased ~10% after 4 months storage
- Aging did not prevent single hinge deployment

Boom-CoreSat Interfaces

- Manufactured and tested interfaces
- *Kinematic Mount*: Ample range of motion achieved to align optical systems
- *Separation Device*: Reliably cuts Vectran wire for stage 1 deployment

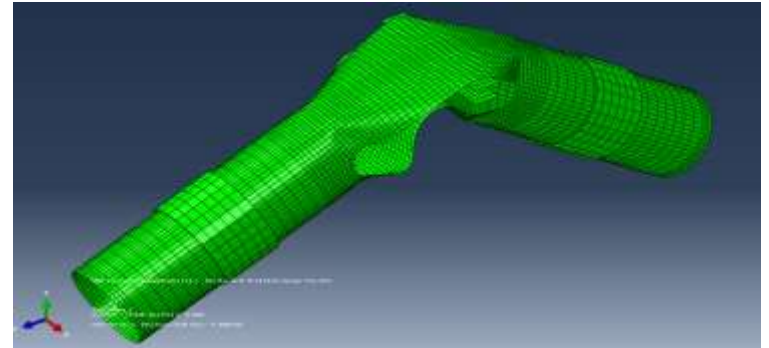
Stage Experiments

- Multiple successful stage 1 deployments using interface prototypes
- Characterization of the initial conditions for stage 2 deployment

Future Work

Long-Term Storage

- Compare results with FEM simulations from previous years
- Analyze full boom deflection after deployment



Boom-CoreSat Interfaces

- Perform separation device tests in vacuum chamber
- Analyze kinematic mount design from thermal and structural standpoint and make necessary modifications

Stage Experiments

- Complete stage 1 and 2 experiments
- Further analyze the effect of the bending moment exerted on camera-CoreSat interface

Outgassing

- Identify outgassing level of boom composite and contaminants

Questions?

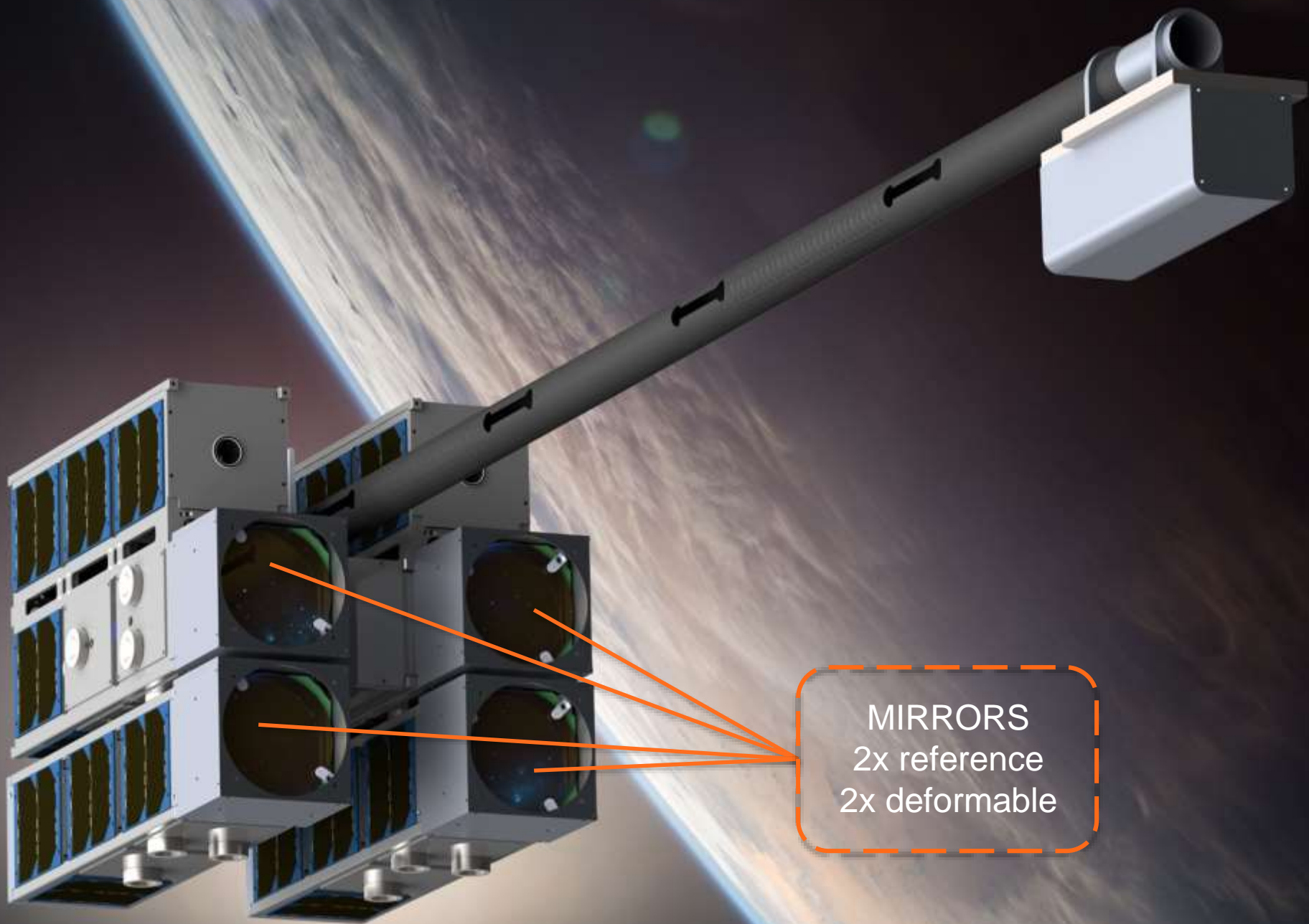
Study of mirror deformations under thermal loading

Nicolas Meirhaeghe

Pranav Nath

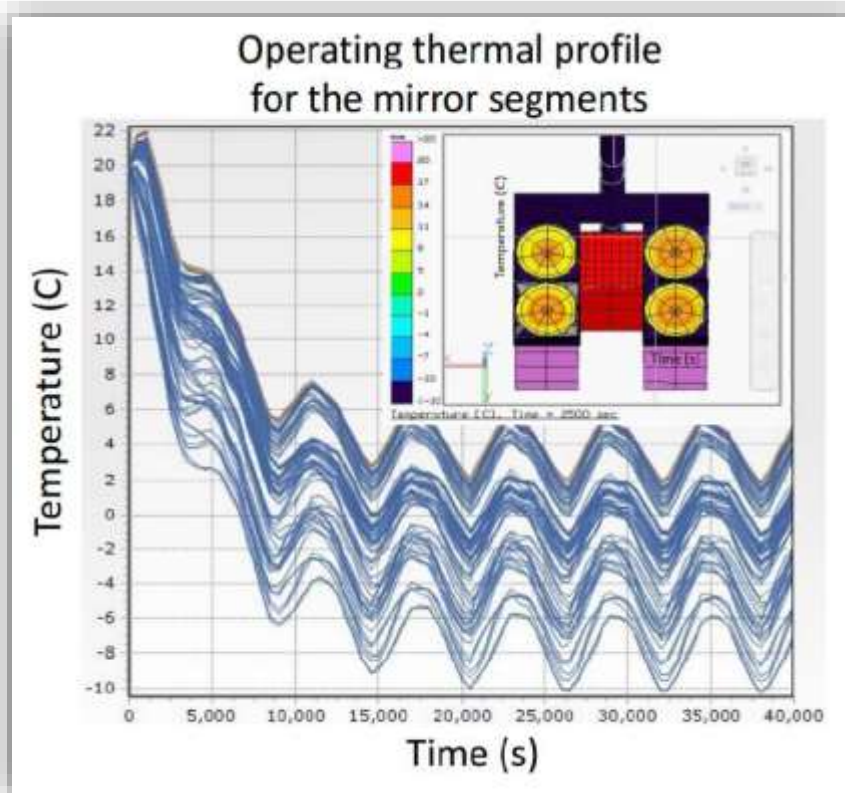
J.P. Voropaieff

Mentor: Christian Kettenbeil



MIRRORS
2x reference
2x deformable

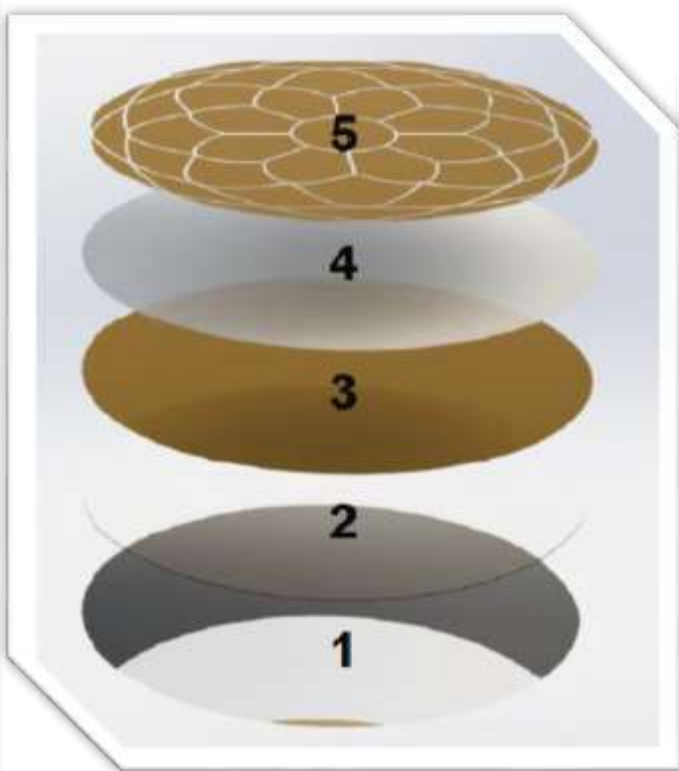
Thermal environment



Temperature range:
[-6°C; 10°C]

Simulation of on-orbit thermal loads (SSO)

Mirror Structure

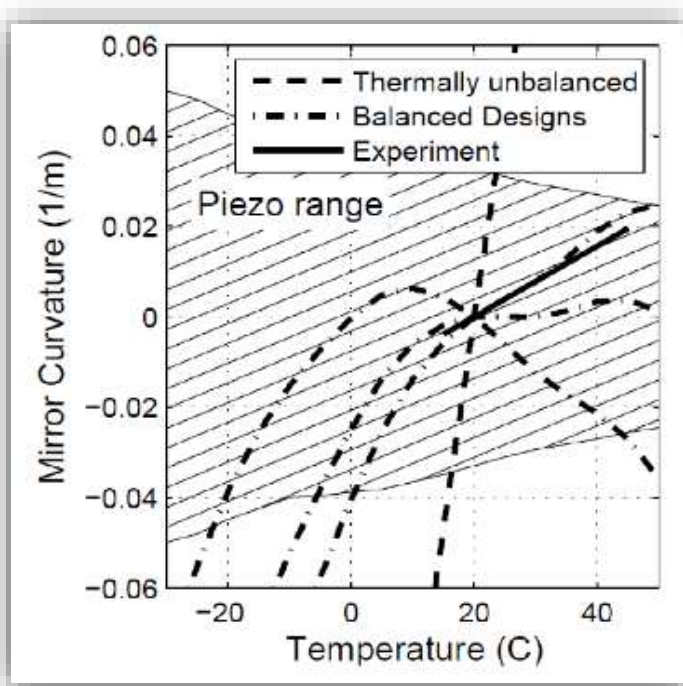


Layer Architecture of the Deformable Mirror (DM)

Position	Mirror layer	Material	Thickness (μm)	Order	Method(s)
1	reflective surface	Al, Ag, or Au	0.1	2	sputtering evaporation
2	substrate	Si or Glass	200	1	(slumping)
	adhesion	Ti	0.01	3	sputtering evaporation
3	ground	Au	0.1	4	sputtering evaporation
	adhesion	Ti	0.01	5	sputtering evaporation
4	active	P(VDF-TrFE)	20	6	spin coating
	adhesion	Ti	0.01	7	sputtering evaporation
5	electrodes	Au	0.1	8	sputtering +ion mill

Composition of each layer

Limitations of the active layer



Piezo Capabilities

Position	Mirror layer	Material	Thickness (μm)	Order	Method(s)
1	reflective surface	Al, Ag, or Au	0.1	2	sputtering evaporation
2	substrate	Si or Glass	200	1	(slumping)
	adhesion	Ti	0.01	3	sputtering evaporation
3	ground	Au	0.1	4	sputtering evaporation
	adhesion	Ti	0.01	5	sputtering evaporation
4	active	P(VDF-TrFE)	20	6	spin coating
	adhesion	Ti	0.01	7	sputtering evaporation
5	electrodes	Au	0.1	8	sputtering + ion mill

Piezo compensates for:

- 1) Thermal deformations
- 2) Wavefront errors
- 3) Electronic drift
- 4) Manufacturing errors, etc...

Goal of the project

“ Ensuring operability of the deformable mirrors under on-orbit thermal loading conditions ”

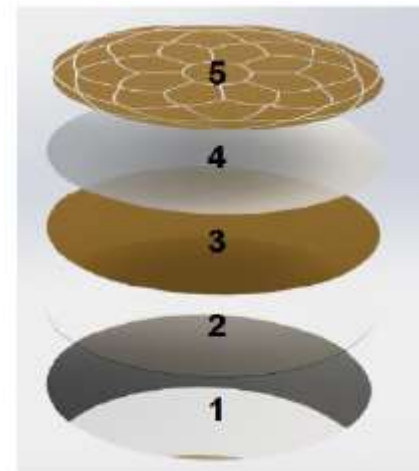
- Keep thermal deformations within piezo range (+ margin)
- Operating temperature range [-20°C; 20°C]
 - Based on simulation (+ margin)
- Survivability range [-60°C; 50°C]
 - Account for:
 - ✓ Drop in temperature when electronics is off
 - ✓ Potential overheating under extreme conditions

Objectives of the project

1) Characterization of pre-designed mirror samples

- Testing of 4 different « recipes »
- Only reflective layer composition varies

Sample	Chromium [nm]	Aluminum [nm]	# of Layers	Total Thickness [μm]
1	50	500	3	1.65
2	50	250	6	1.8
3	50	500	4	2.2
4	50	250	8	2.4



Objectives of the project

2) Validation of a theoretical model for thermal deformation

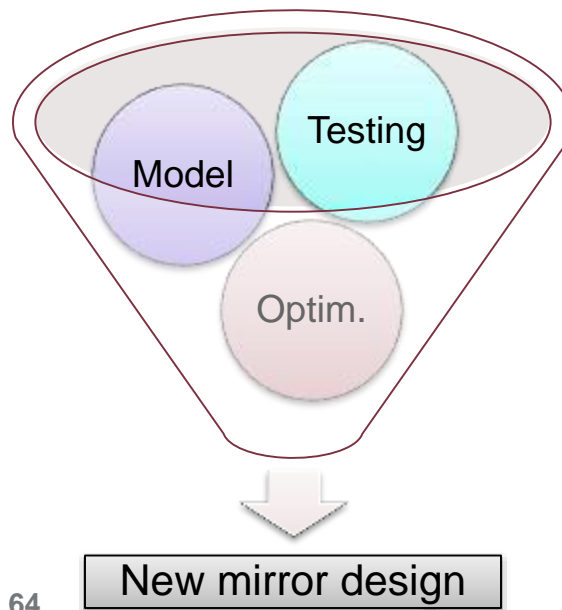
- Simplified model (*Stoney's Formula*)
- Relates radius of curvature of mirror to material properties of each layer and temperature loading

$$\kappa = \frac{6\Delta T}{t_s^2 M_s} \sum_i s_i (\alpha_i - \alpha_s) M_i t_i ,$$

Objectives of the project

3) Optimization of mirror composition

- Cost function: curvature change over operating range
- Free parameter: thickness of reflective layer
- Design recommendations for new mirror



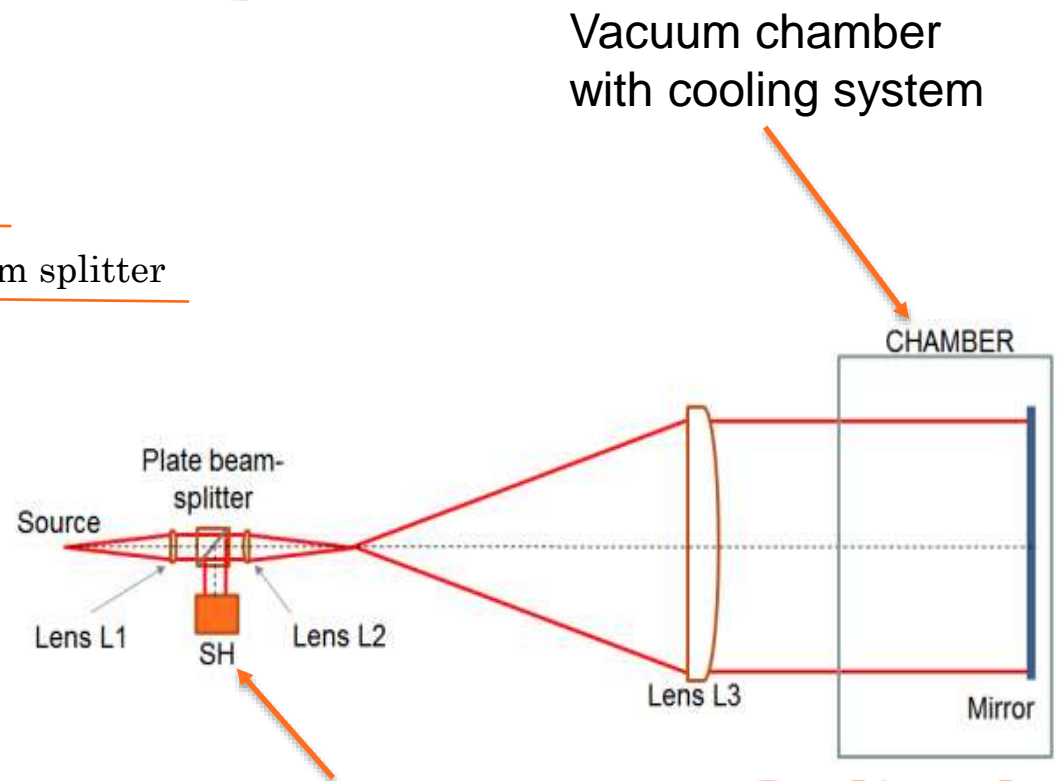
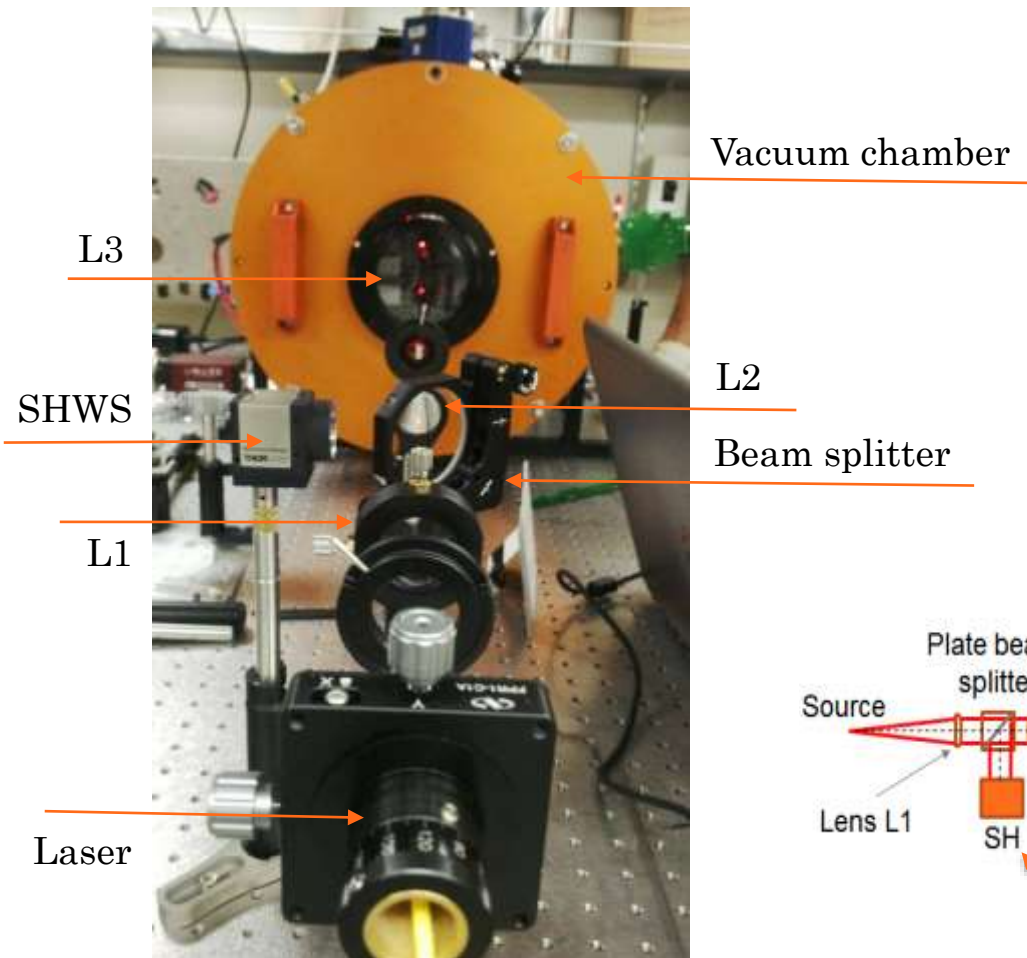
Objectives of the project

4) Testing of the new design

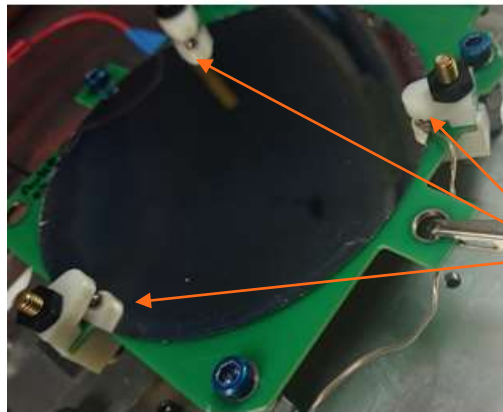
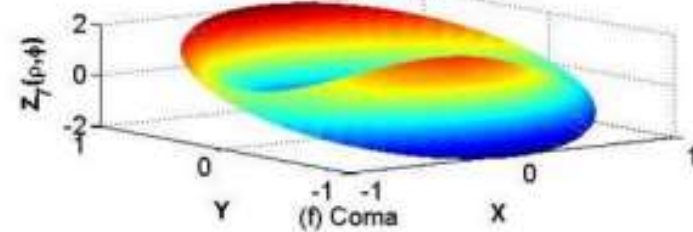
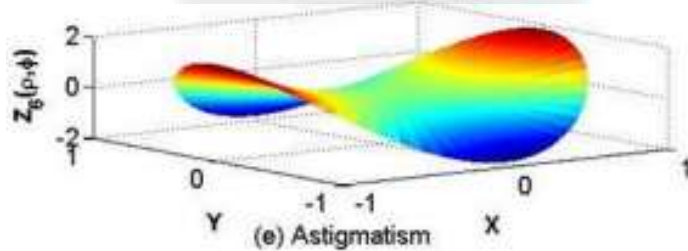
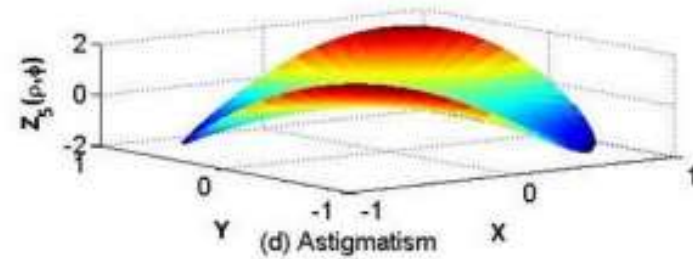
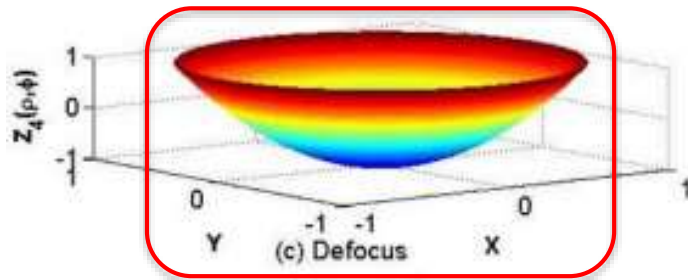
- Check if optimization yielded better performances
- Verify that requirement is met



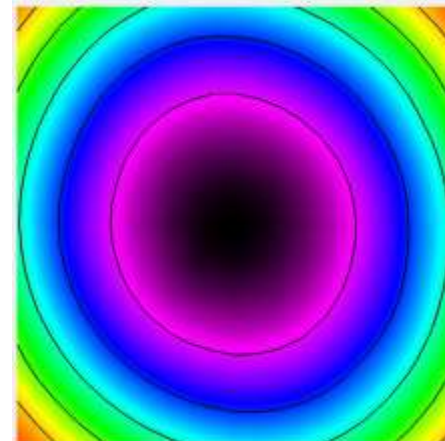
Experimental setup



Mirror deformation: defocus

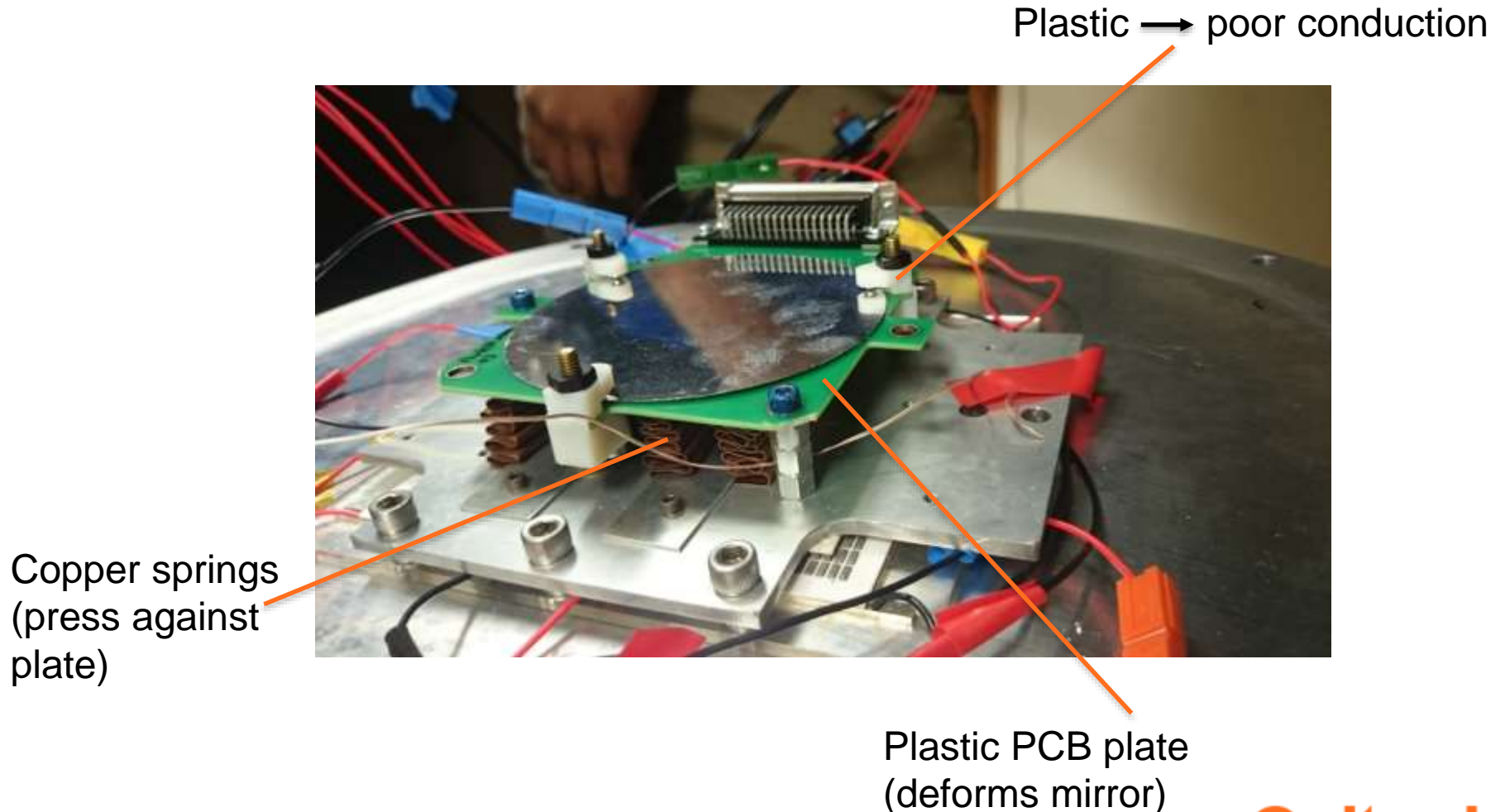


Kinematic
mounts



SHWS
measurement
of Sample 1

Problems with the old setup

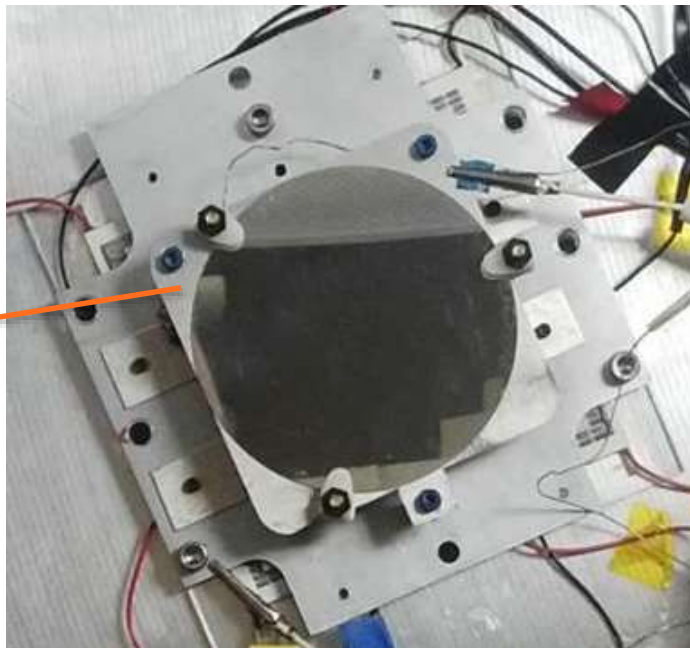


Improvements

- New setup
 - Better conduction
 - Included radiation shield
 - Aluminum plate stiffer

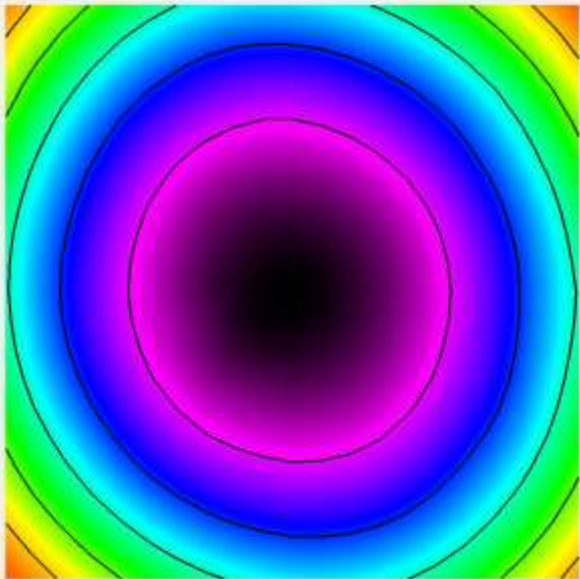
After improvements:
-4°C on mirror

Aluminum
plate



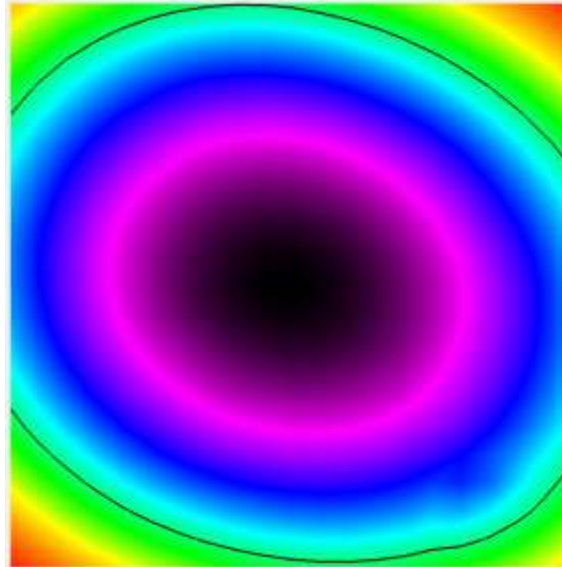
Sample Testing

- Sample 3 shows too much initial astigmatism (Z4 & Z6)



Z 4 (2 / -2)	-0.159
Z 5 (2 / 0)	2.281
Z 6 (2 / 2)	0.243

Sample 1



Z 4 (2 / -2)	-0.536
Z 5 (2 / 0)	3.055
Z 6 (2 / 2)	-0.761

Sample 3

Samples 2 and 4 were much more astigmatic

- Only sample 1 used for analysis

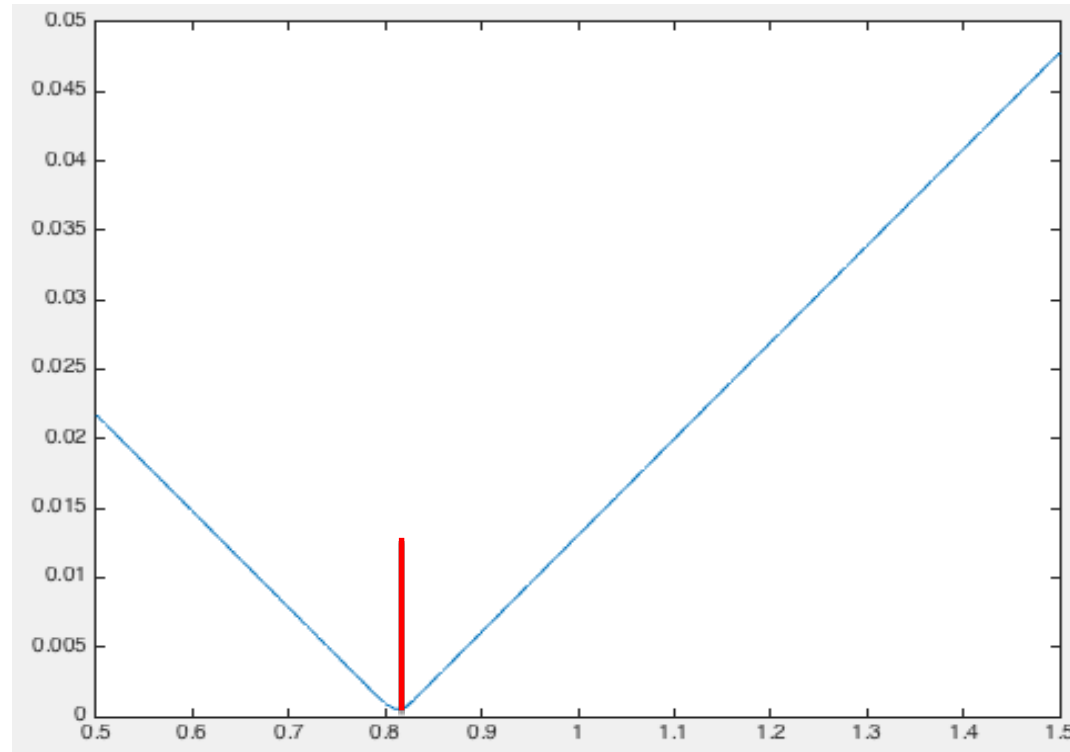
Results and Analysis

Determination of Material Properties

Stoney's Formula
$$\kappa = \frac{6\Delta T}{t_s^2 M_s^2} \sum_i s_i (\alpha_i - \alpha_s) M_i t_i$$

Cost function : $\varepsilon_{abs}(\Delta T, E_{Al}, \alpha_{Al}, E_{Cr}, \alpha_{Cr}) = |\kappa_{theoretical}(\Delta T, E_{Al}, \alpha_{Al}, E_{Cr}, \alpha_{Cr}) - \kappa_{experimental}(\Delta T)|$

Error
between
data
and
model



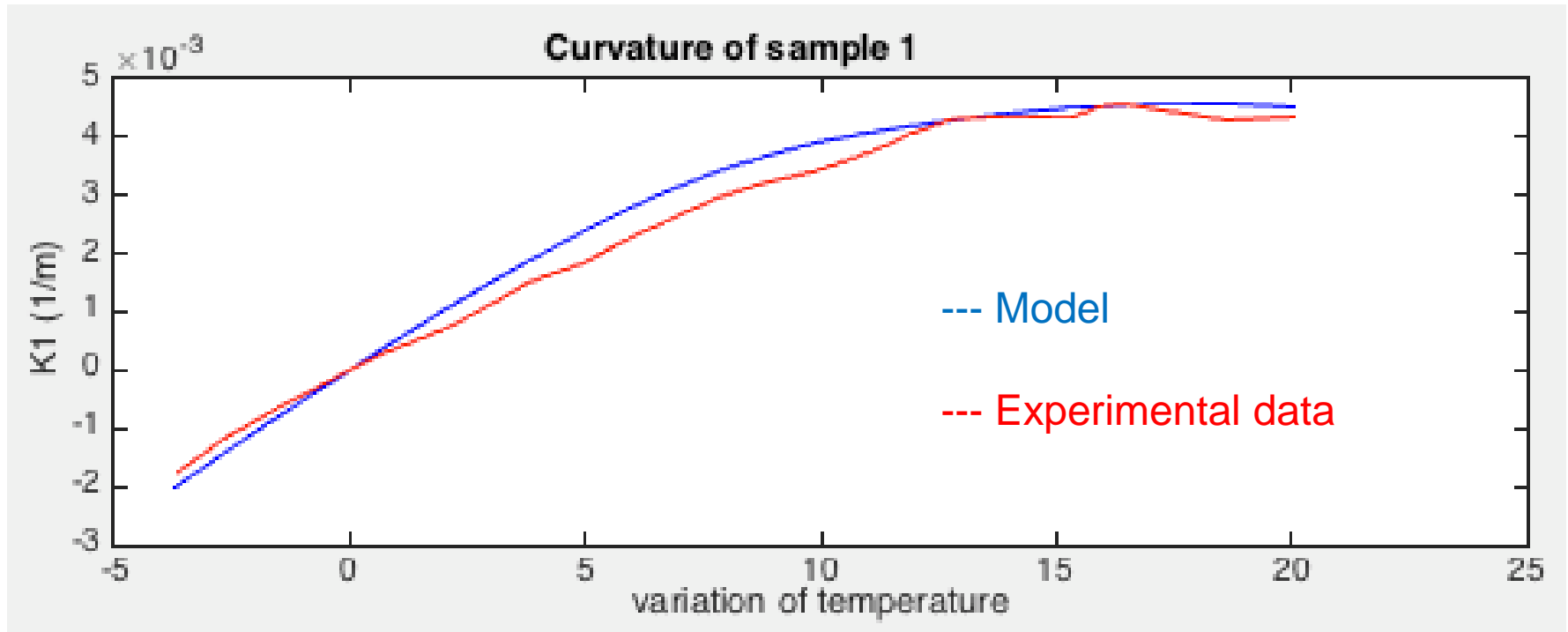
Range expected :

- $E_{Al} = [50; 70 \text{ GPa}]$
- $E_{Cr} = [140; 250 \text{ GPa}]$
- $\alpha_{Al} = [18; 23 \cdot 10^{-6} \text{ K}^{-1}]$
- $\alpha_{Cr} = [4.5; 5.5 \cdot 10^{-6} \text{ K}^{-1}]$

Results of curve-fit:

- $E_{Al} = a * E_{Al,bulk} = 56.7 \text{ GPa}$
- $E_{Cr} = 202.5 \text{ GPa}$
- $\alpha_{Al} = 20.1 \cdot 10^{-6} \text{ K}^{-1}$
- $\alpha_{Cr} = 4.9 \cdot 10^{-6} \text{ K}^{-1}$

Model Validation



- Maximum relative error = 24%
- Mean relative error = 11%

Error due to:

- Initial curvature of sample
- 3D effects

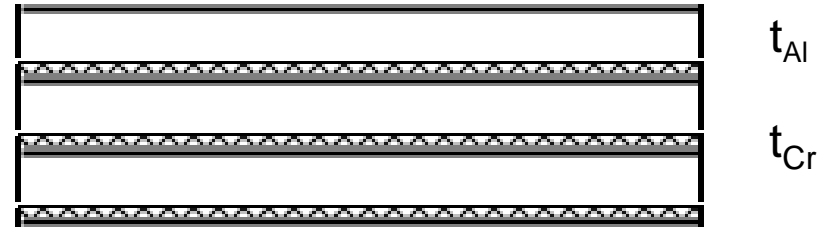
Model validated

Optimization strategy

Design choices

- Reflective layer composition: Aluminum + Chromium (stiffer)
 - 3 sublayers of Al
 - 3 sublayers of Cr

- Ratio Al/Cr = 10 \longrightarrow $t_{Cr} = t_{Al} / 10$

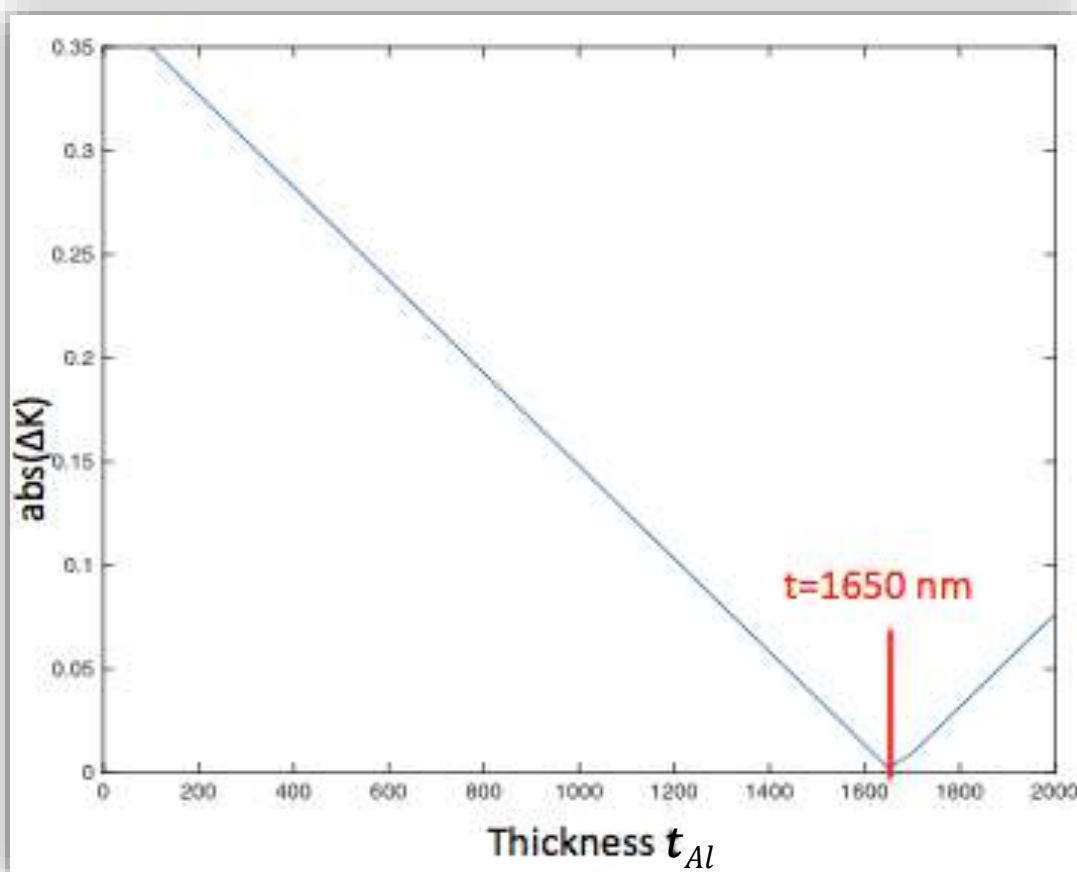


$$|\kappa(t, \Delta T)| = \left| \frac{6\Delta T}{t_s^2 M_s^2} \left(3t(\alpha_{Al} - \alpha_s)M_{Al} + 3\frac{t}{10}(\alpha_{Cr} - \alpha_s)M_{Cr} \right) - \frac{6\Delta T}{t_s^2 M_s^2} \sum_j (\alpha_j - \alpha_s)M_j t_j \right|$$

Cost function: $\varepsilon(t) = \max_{\Delta T} (|\kappa(t, \Delta T)|)$

Optimization of reflective layer

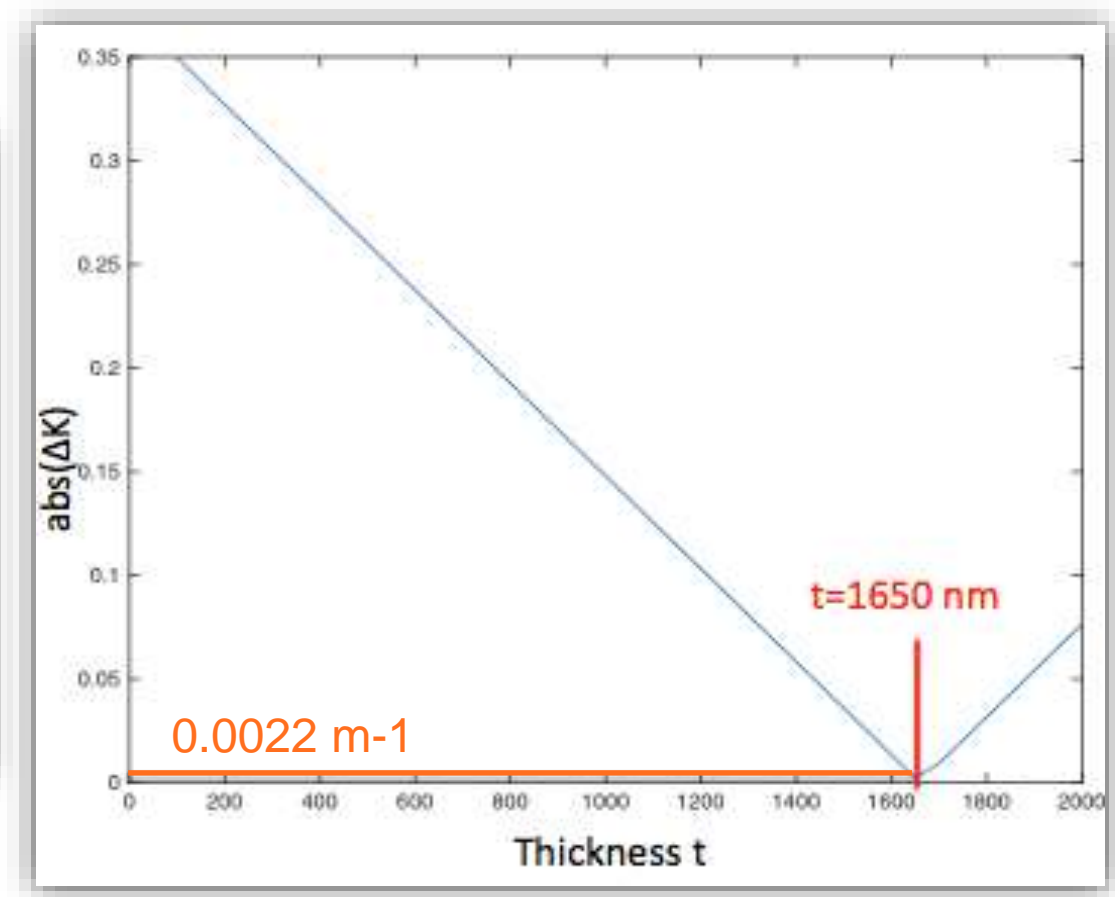
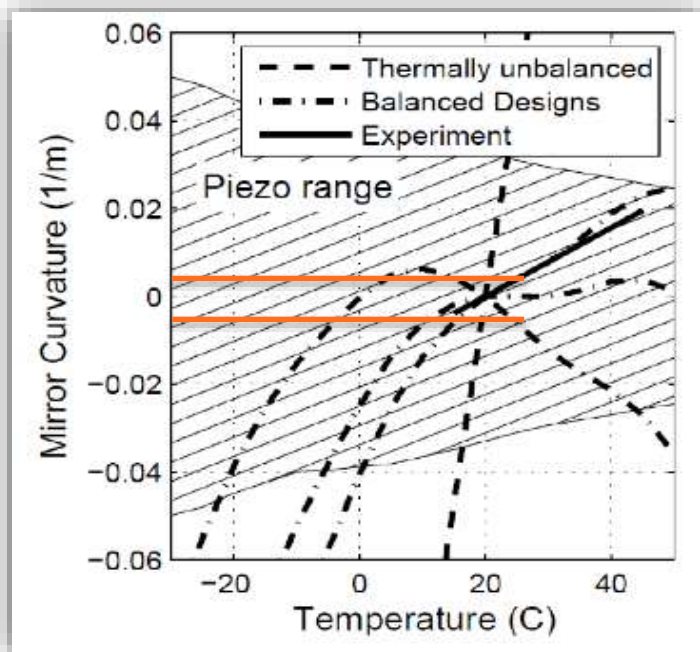
$$\varepsilon(t_{Al}) = \max_{\Delta T} (|\kappa(t_{Al}, \Delta T)|)$$



Final Design Recommendation
for composition of reflective layer:

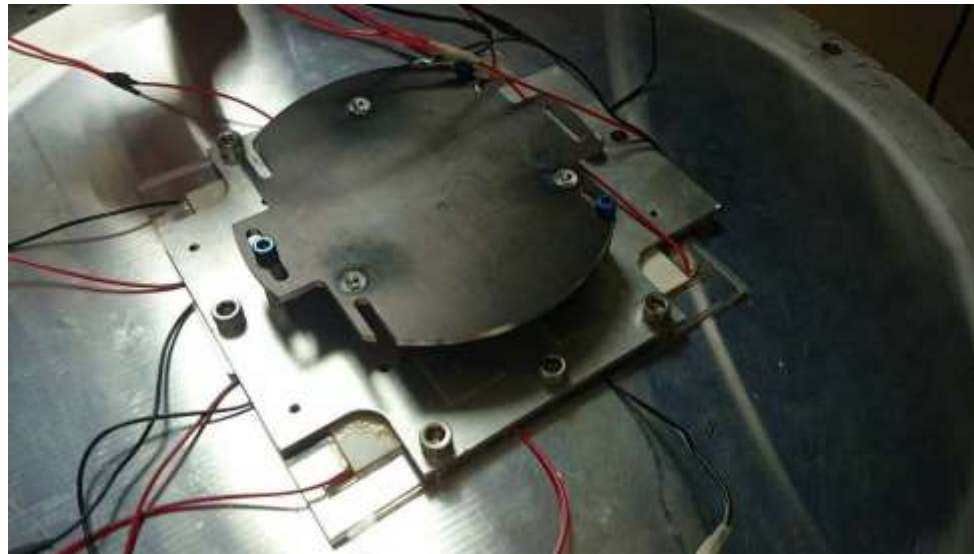
- 3 sublayers of Aluminum of thickness $t_{Al} = 1.65 \mu\text{m}$
 - 3 sublayers of Chromium of thickness $t_{Cr} = 0.165 \mu\text{m}$
- Overall thickness :
 $t_{\text{Reflective}} = 5.445 \mu\text{m}$

Requirements are met



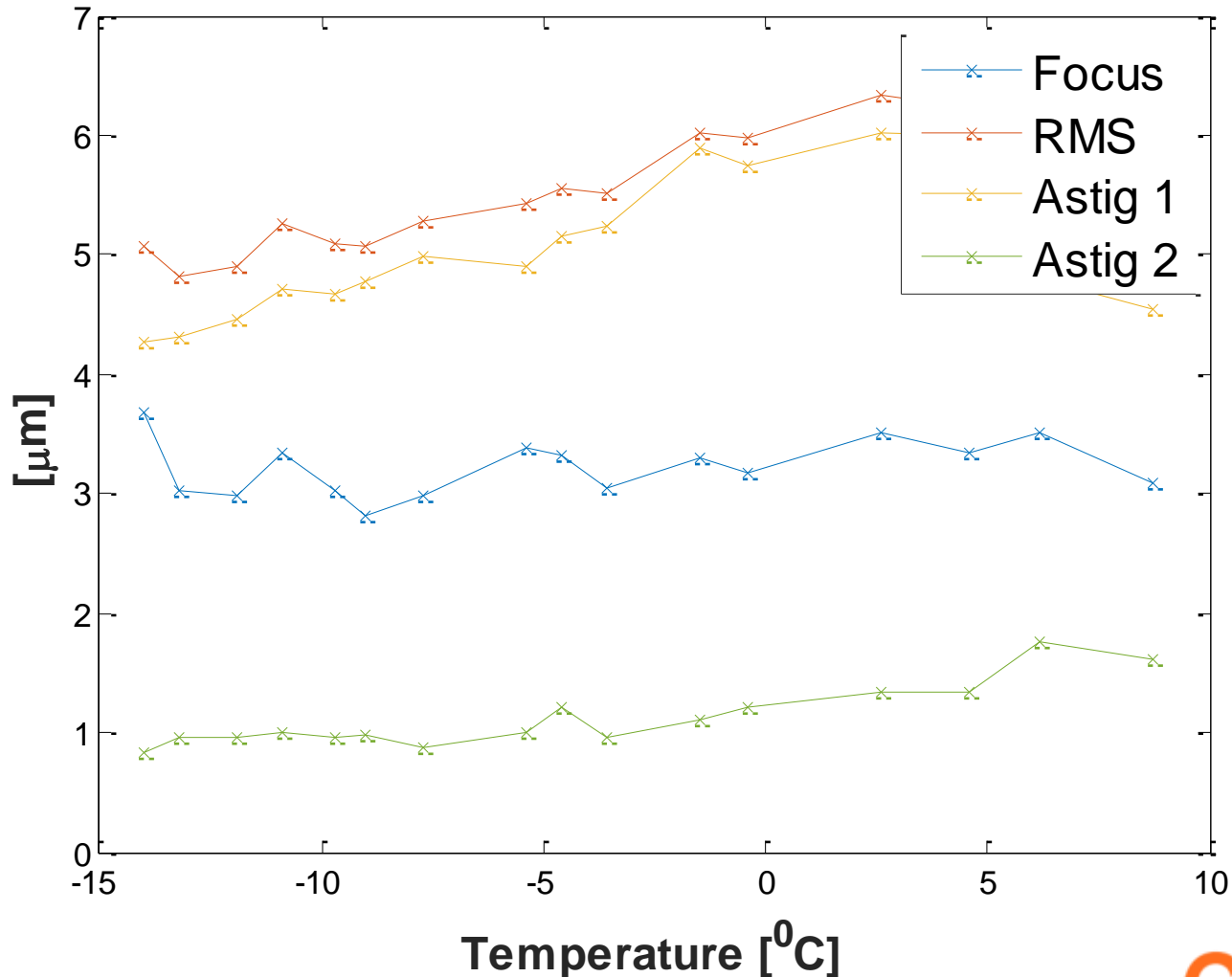
Testing of new design

- Latest setup (reached -16°C on mirror)



- Reversed Hartmann

Results for new design



Conclusion

Work completed:

- ✓ Testing and characterization of mirror samples
- ✓ Developed Simulation tool
- ✓ Optimization of mirror layering
- ✓ Design recommendation
- ✓ Testing of new design

Future work:

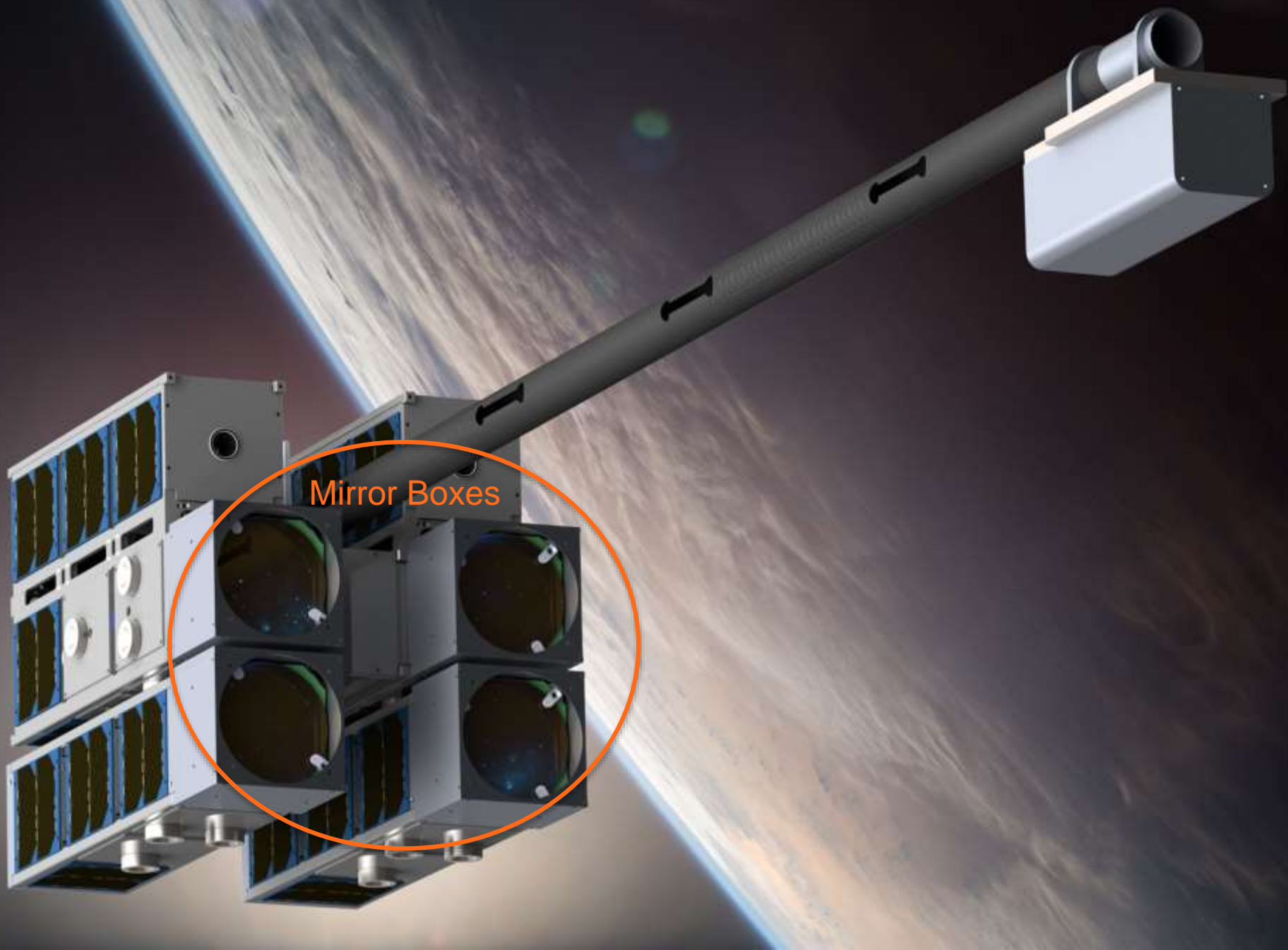
- Improvement of cooling capacities
- More testing of latest design
- Error budget

Mirror Box

Tatiana Roy

Albert Yang

Mentor: Lee Wilson



Mirror Boxes

Two Types of Mirror Boxes

- Mirror box contains all required infrastructure for telescope mirrors
 - Two reference (rigid) mirrors and two deformable mirrors in total
 - Will focus primarily on the deformable mirrors

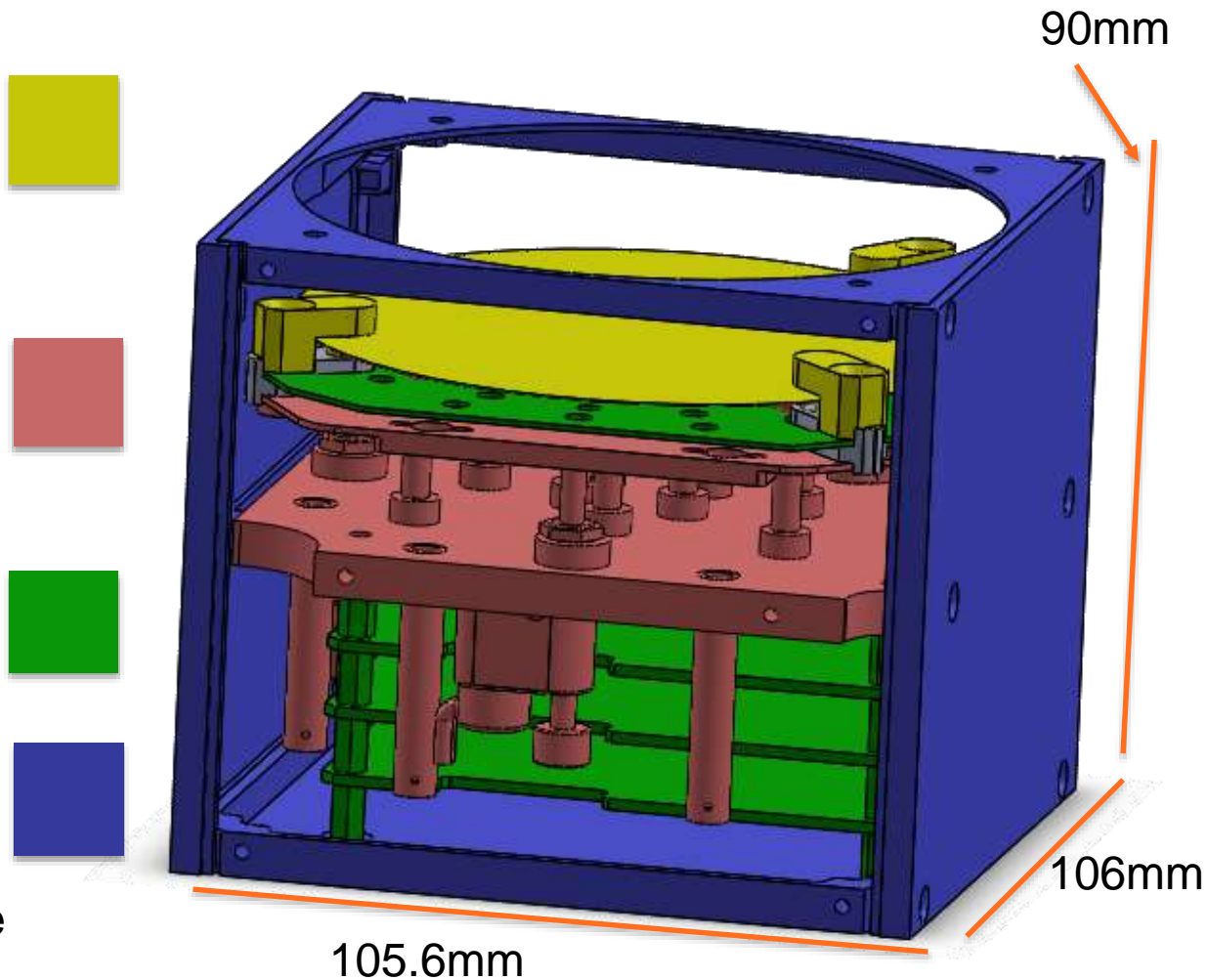
Reference Mirrors



Deformable Mirrors

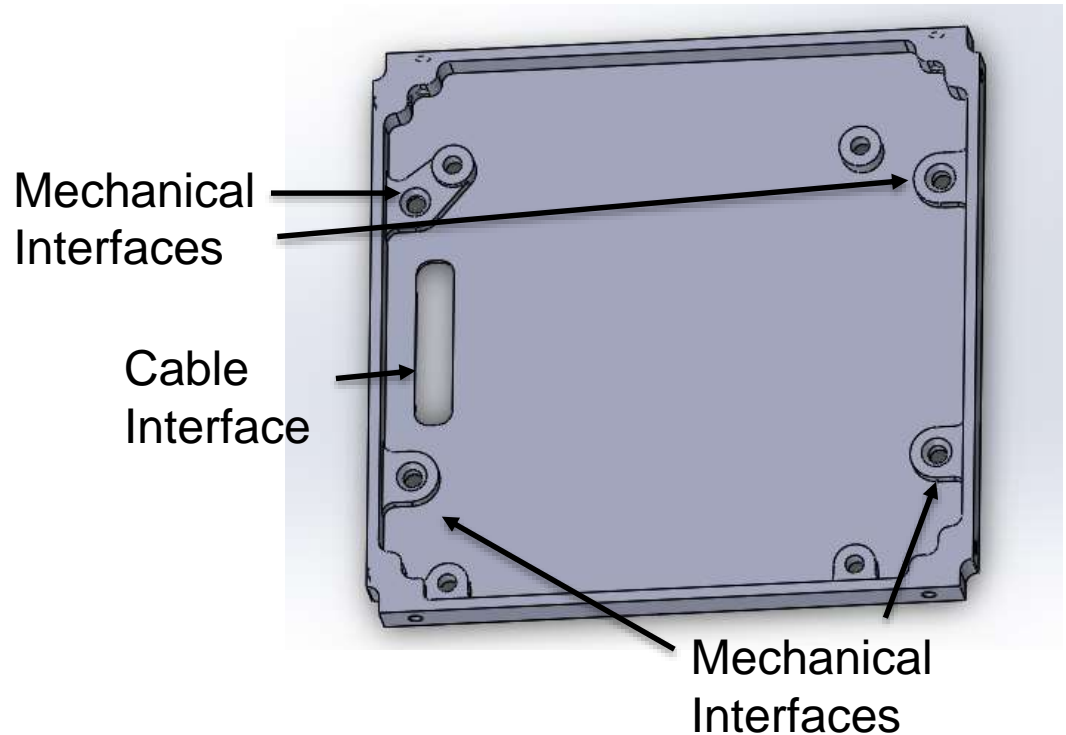
Box Subsystems

- **Mirrors**
 - Mirrors subsystem holds the mirror in place
- **Picomotors**
 - Piston/tip/tilt the mirror
- **Electronics**
 - House electronics
- **Frame**
 - Hold all mirror box elements and interface with CoreSat



CoreSat Interface

- Must match with pre-established Surrey mechanical and electrical interfaces

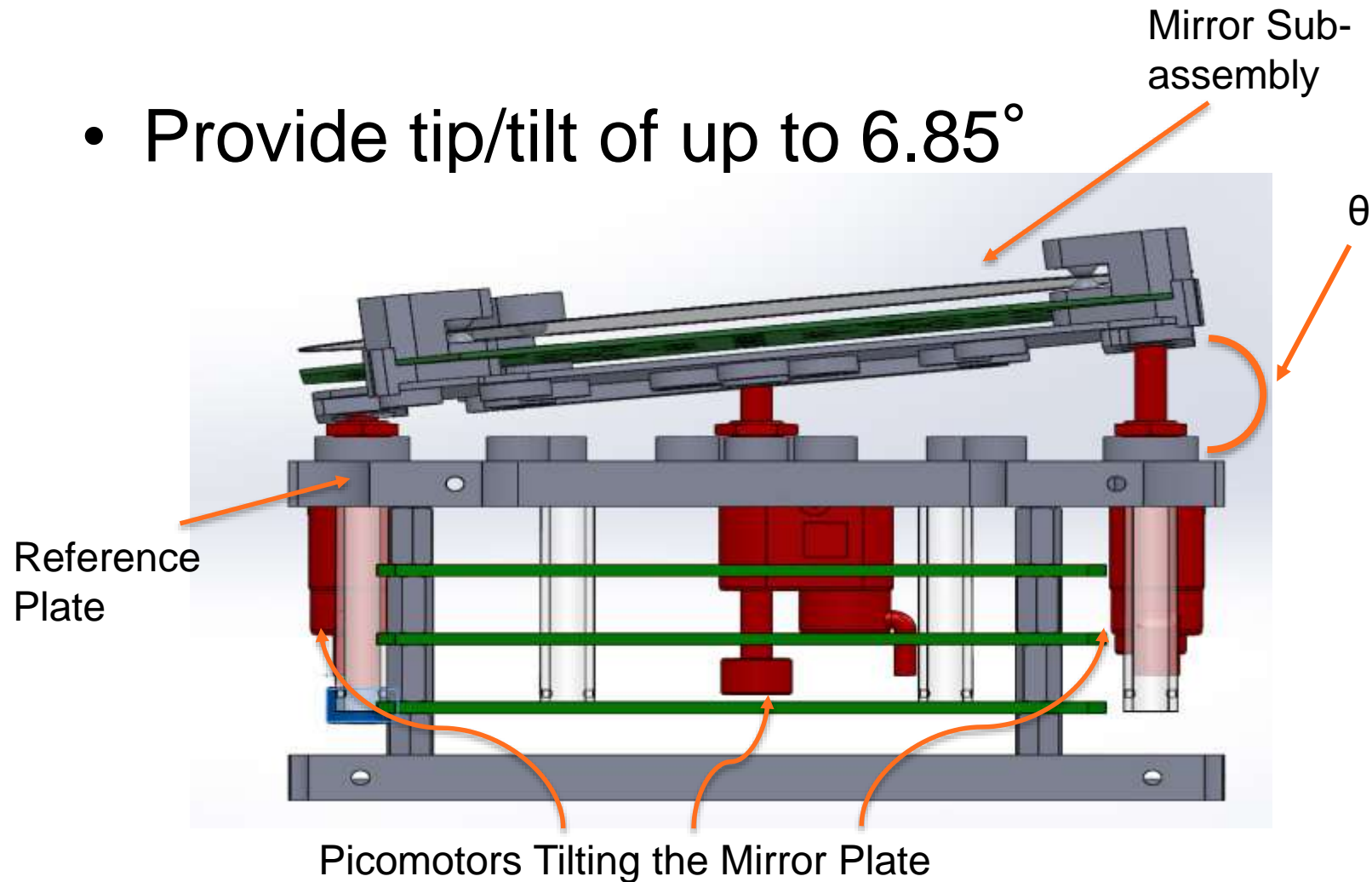


Functional Requirements

- Survive launch loads
- Provide mechanical support for a set of deformable mirrors, rigid mirrors, and mirror electronics
- Allow mirror to operate within the required range of tip, tilt, and piston positions,

Performance Requirements

- Provide tip/tilt of up to 6.85°



Mass Budget

- Mass Requirement: <680g per box
- Current Best Estimate:

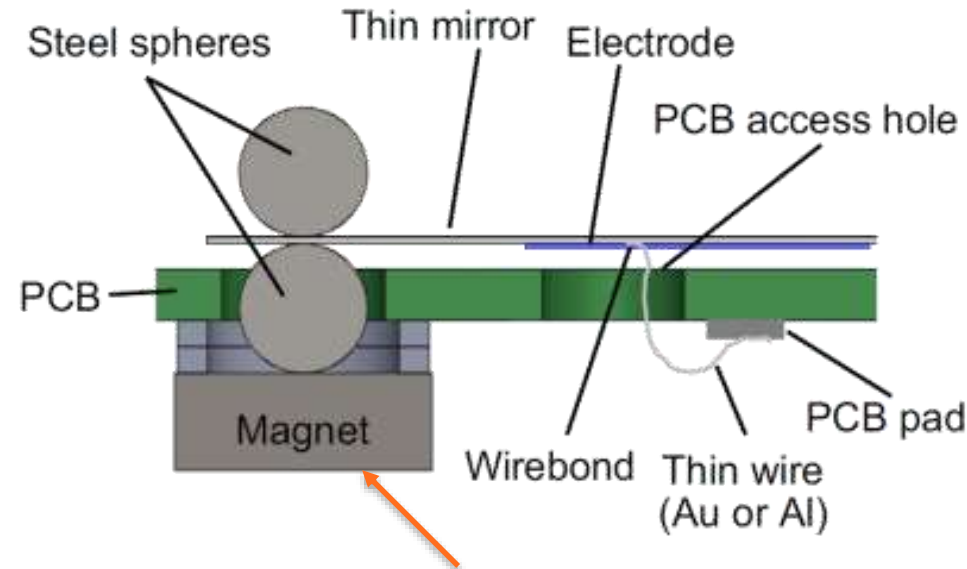
Subsystem	Current Mass (g)	% total	Contingency (g) (30%)	Total (g)
Mirror*	28	5.5	9	37
Picomotors	263	51.7	79	342
Electronics	38	7.5	12	50
Frame	180	35.4	54	234
Total Mass	509		154	663

Addressing Requirements

- Mirror Mounts
 - Updated mount design to solve pinching issue
 - Tested new mount design
- Damping Columns
 - Designed damping columns to interface with mirror box and mitigate launch loads
 - Chose damping material
- Updated mirror box design

Mirror Mount: Old Design

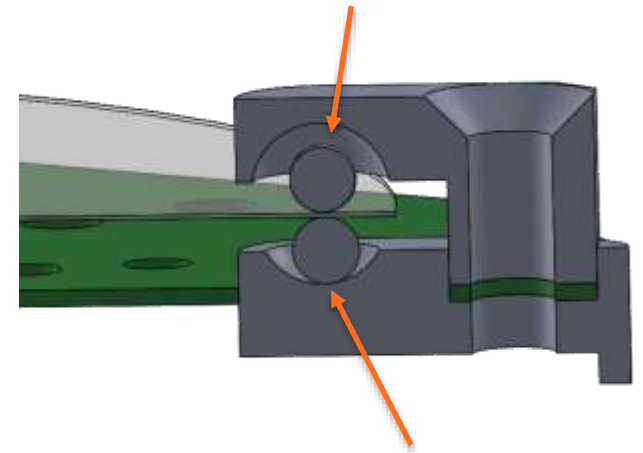
- Curved mirror is extremely thin. Mirror is prone to deformation near mounting sites
 - Old mounts designed for flat mirrors
 - Curved mirrors need different mounts
 - Changes in shape will lead to reduced overall performance



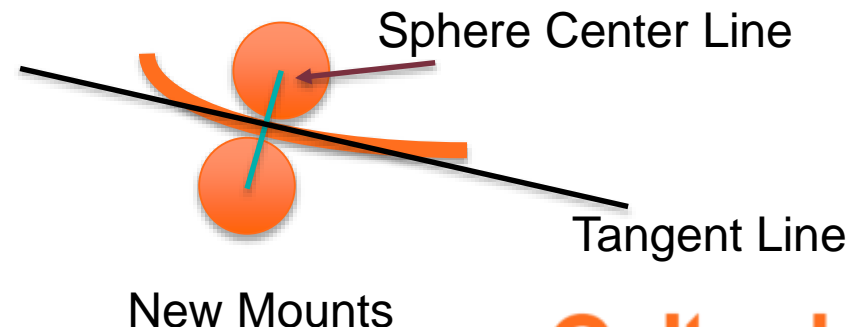
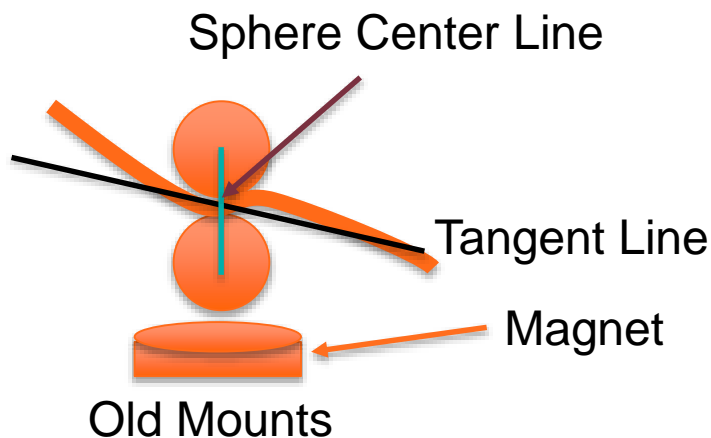
Mirror Mount: New Design

- Designed new mount
 - Single point of contact on each side of the mirror
 - Top cage required to retain magnet

Magnet/Cage minimum clearance

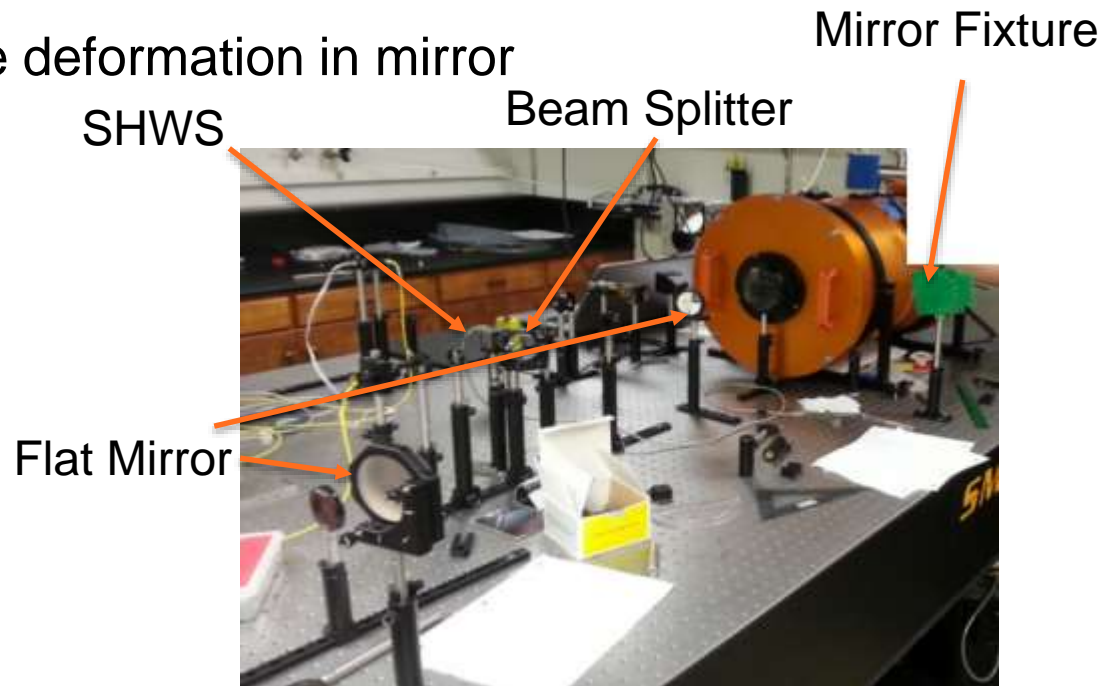
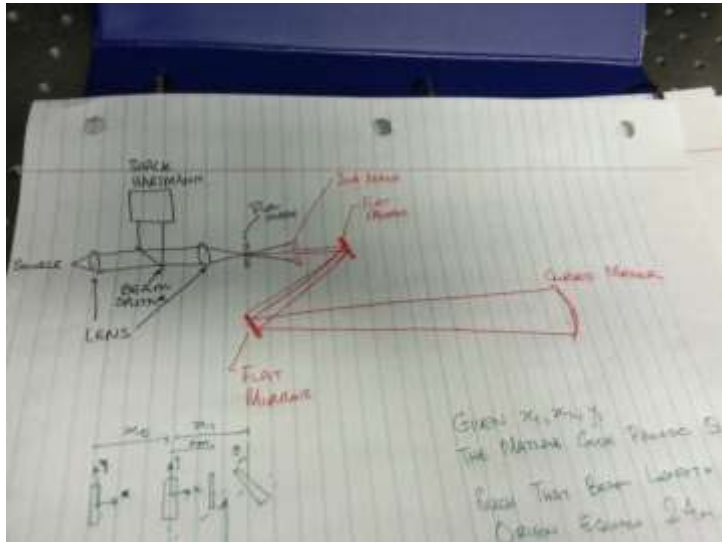


Fixed with epoxy

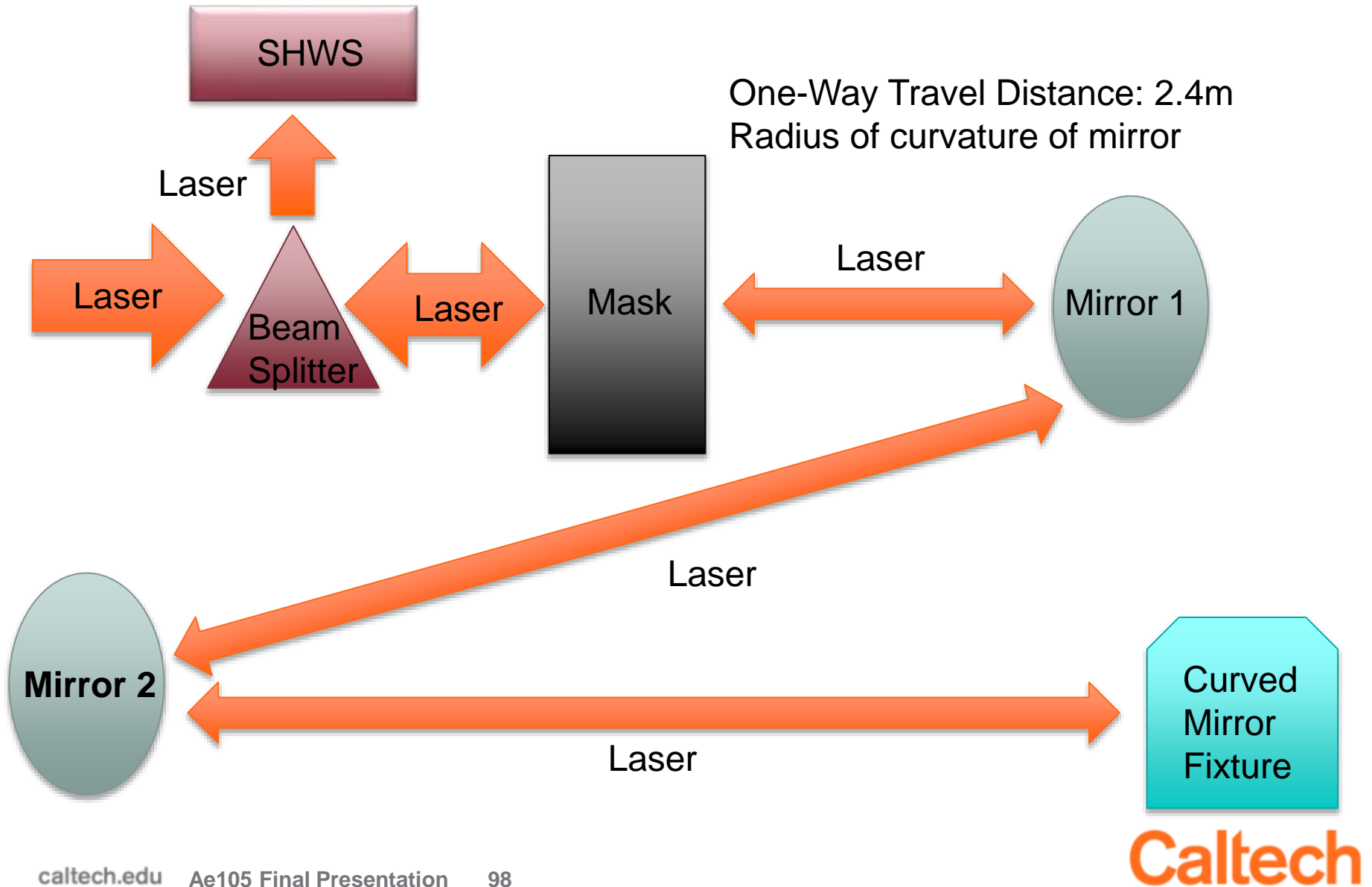


Testing Mirror Deformations

- Zernike coefficients were calculated using SHWS to measure deformations
 - Need 2.4m (radius of curvature) path to SHWS
 - Independent test also conducted
 - Looking for trefoil shape deformation in mirror



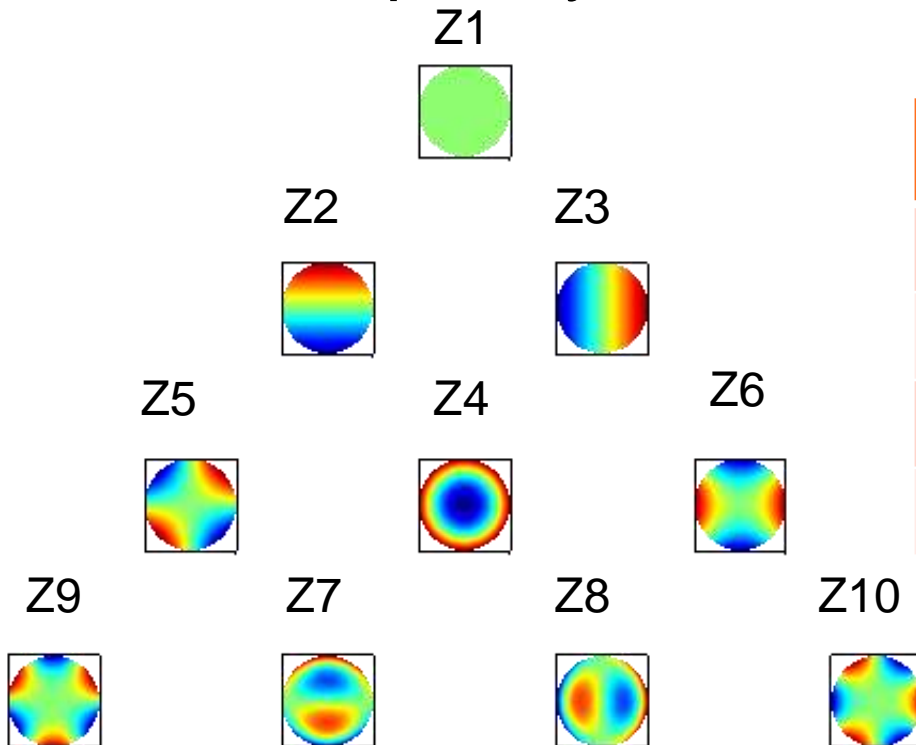
Mirror Deformation Testing Setup



Mirror Mount Deformation Results

- Mirror had high Z4 and Z5 values
- Z9 and Z10 are not present in our test

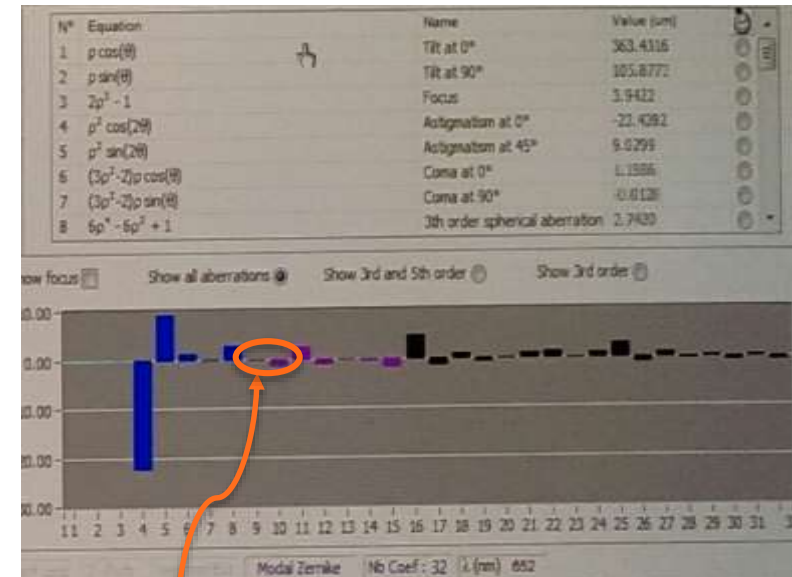
Consequently, mirror mounts do not deform mirror



Zernike	Tested	Name
4	.7	Defocus
5	2.5	Oblique Astigmatism
9	<.1	Vertical Trefoil
10	<.1	Oblique Trefoil

Mirror Mount Characterization

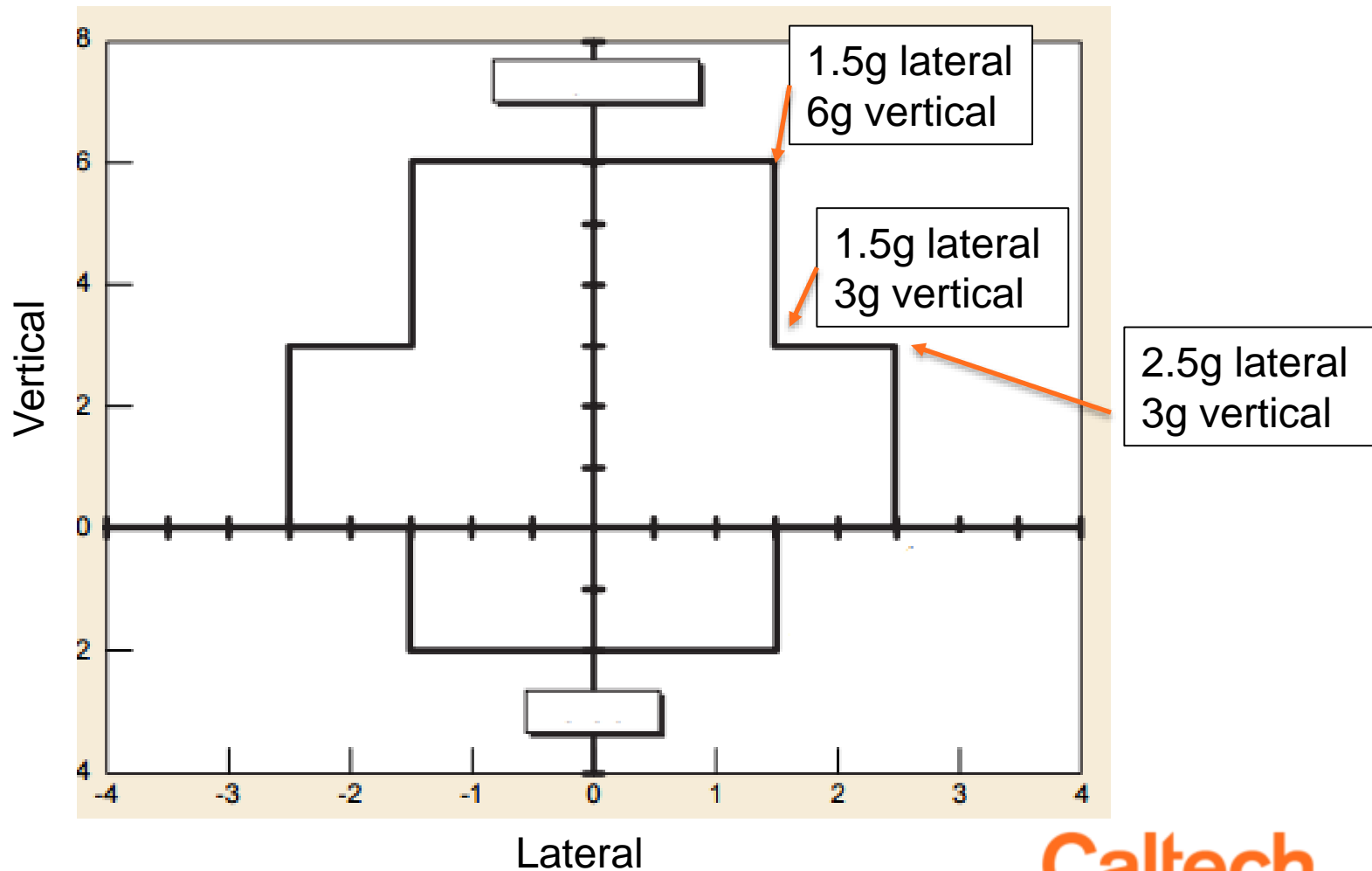
- A test was also performed on a Haso SHWS by Caltech Post-Doc Steve Bongiorno
 - Performed on different mirror, manufactured to have less errors
 - Concluded mirror aberration was dominated by astigmatism, and not by any trefoil shape



Launch Survival

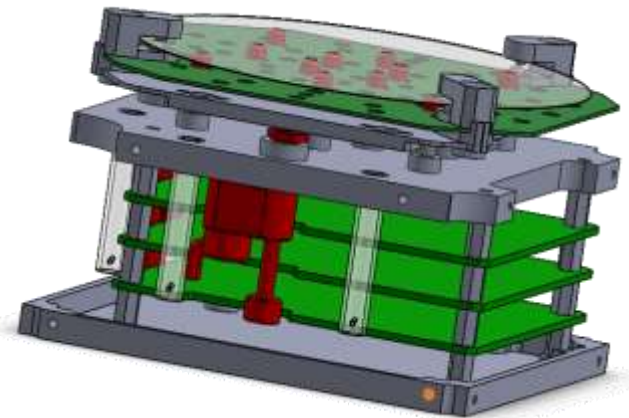
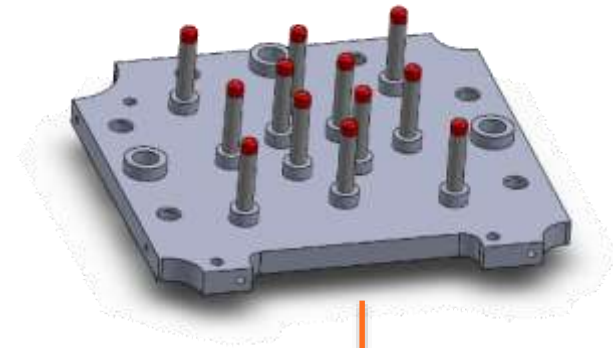
- Large vibration loads during launch: Mirror will vibrate and possibly shatter

From Delta IV
Handbook

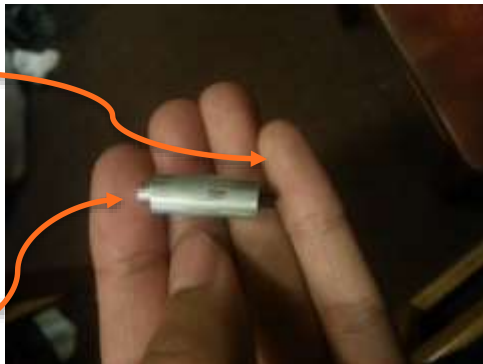


Damping Columns

- Damping columns attenuate vibrational energy by physical contact during launch
 - Damping columns are separated from the mirror after launch



Set screw in
a tapped hole



Extruded Tip for Damping Material

Damping Material

- Chose Red Silicone foam as damping material
 - Reported CVCM (collected volatile condensable materials) of <0.005 (lowest possible)
 - Rated for -100°F to 400°F (required -50°F to 50°F)

Threads Into Reference Plate

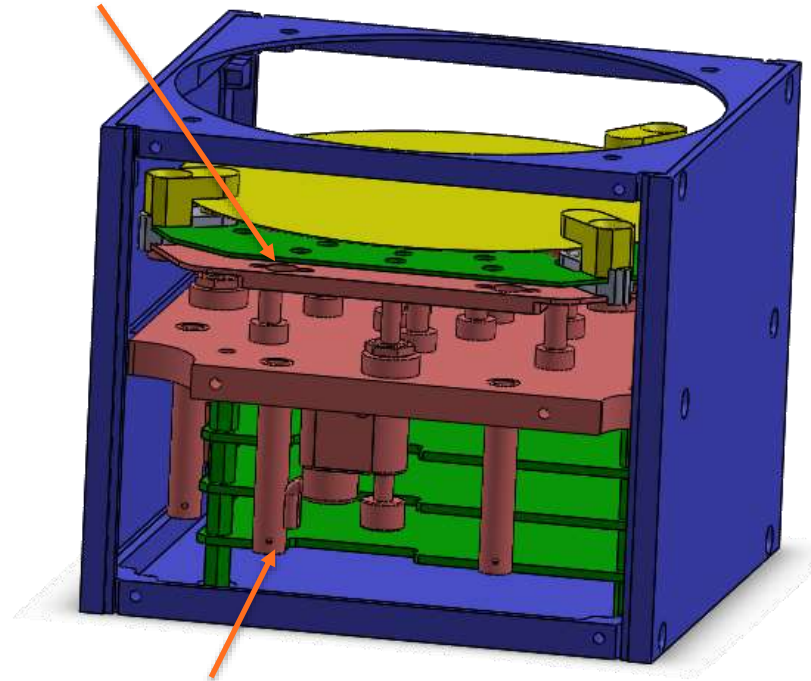


Damping Material at Top

Updated CAD: Spring Tubes

- Keep mirror plate connected to reference plate while still allowing for normal picomotor operation
- Springs housed by tubes connect reference plate and mirror plate

One end attaches at mirror plate



One end attaches at bottom of tube

Summary of Mirror Box Progress

- Designed new mirror mounts to solve mirror pinching issue
 - Prototyped new mounts and characterized with SHWS test
 - Showed no appreciable deformation
- Designed damping columns and chose damping material
 - Fabricated sample damping column
- Updated CAD to reflect design changes

Further Work Required

- Finish launch vibration survivability test
 - Finish profiling vibration table to make sure it can reach the frequencies required
- More SHWS tests with different configurations for the mirror
 - Test mirror with current mount vs. no mount
- Design and assemble reference mirror box

Questions?

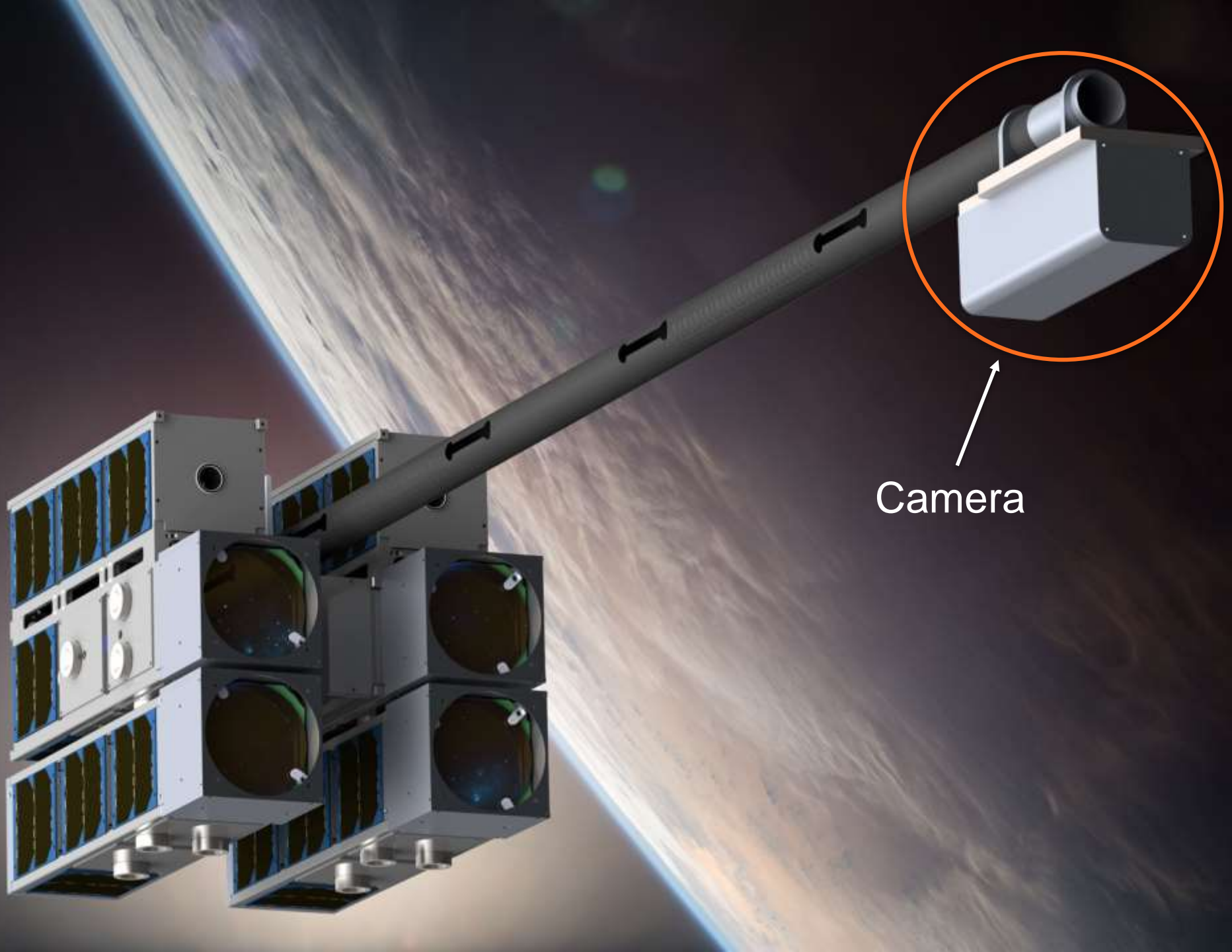
Camera Prototyping

Kevin Bonnet

Christopher Chatellier

Monica Li

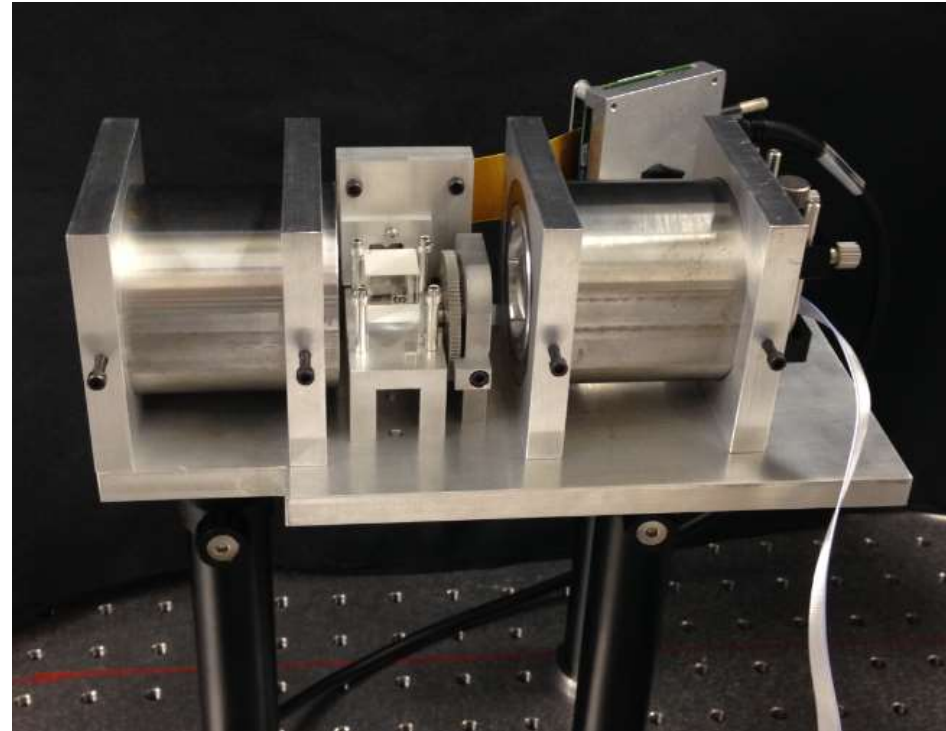
Mentor: Maria Sakovsky



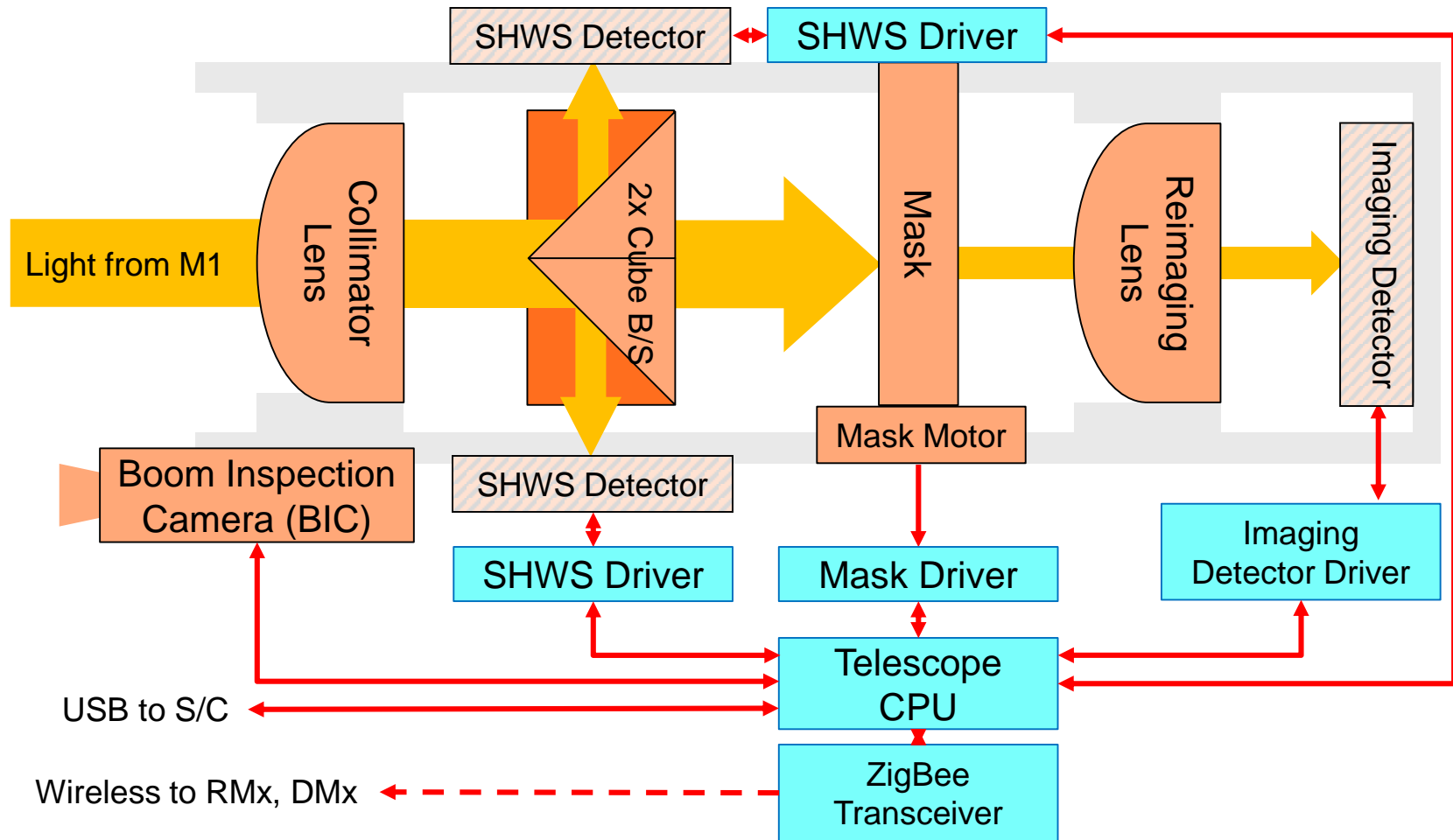
Camera

Overview

1. System Definition
2. Requirements
3. Camera Design
4. Prototype Testing
5. Future Work



System Definition



System Requirements

Functional:

- Work with reconfigurable primary mirror (**Mask Mech**)
- Provide feedback during primary mirror calibration (**SHWS**)
- Science imaging (**Entire Subsystem**)

Performance:

- *80% encircled energy radius < 90% diffraction limit*
- *0.3° full field-of-view*
- *Bandwidth: 465 – 615 nm*
- *SNR > 100*

Constraints:

- Mass < 4kg (Currently **3.82 kg**)
- Volume < 10 × 10 × 35 cm (Currently **8.0 x 9.6 x 23.2 cm**)
- Power < 5W (Currently ~ **7.1W peak power**)

Task Overview

Camera Mechanical

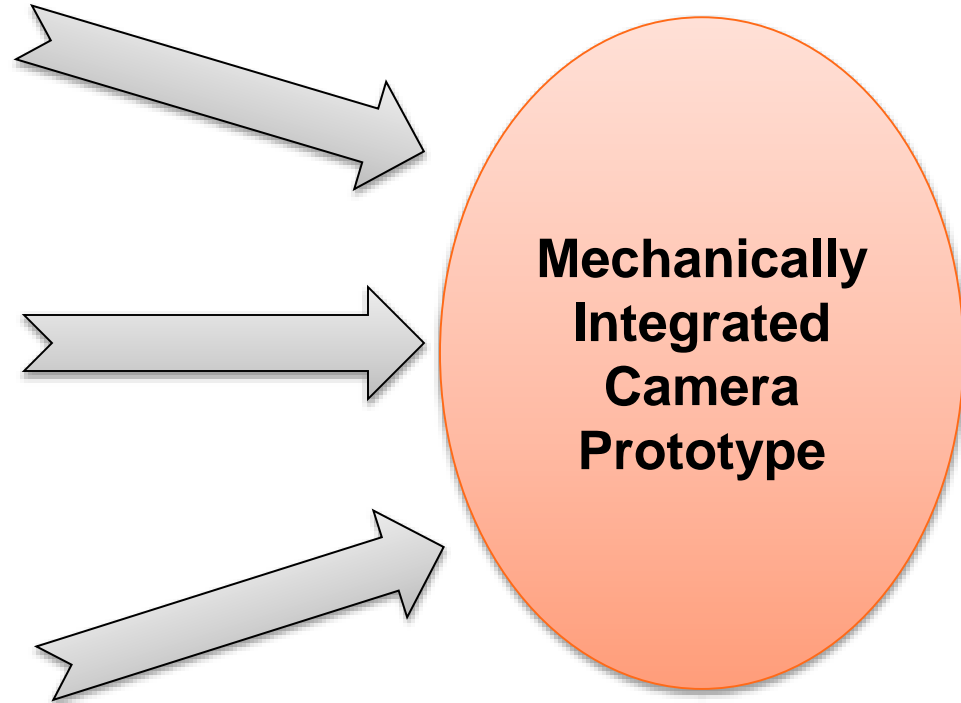
- Mask Mechanism
- Beam Splitter
- Component Interfaces

SHWS & Optics

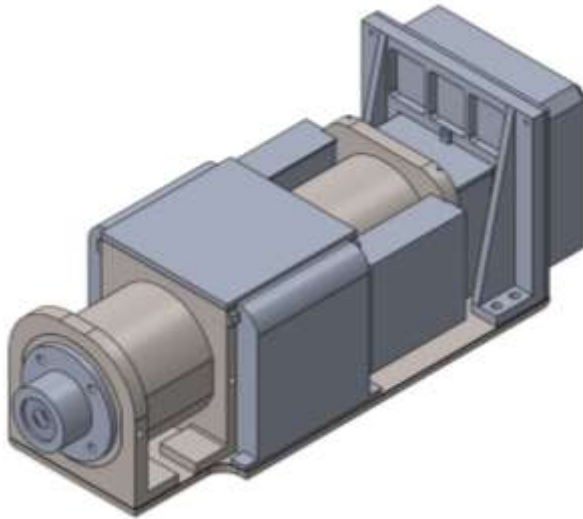
- Mount Design
- Alignment & Calibration

Camera Prototype

- Manufacture & Integrate
- Verification & Validation

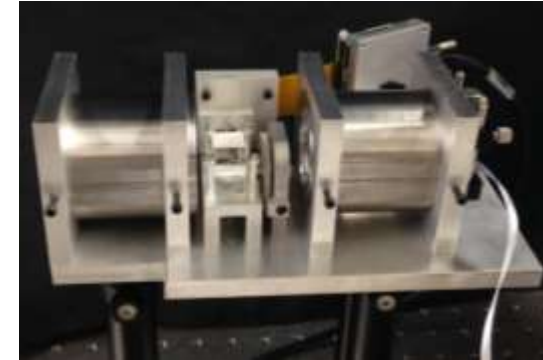
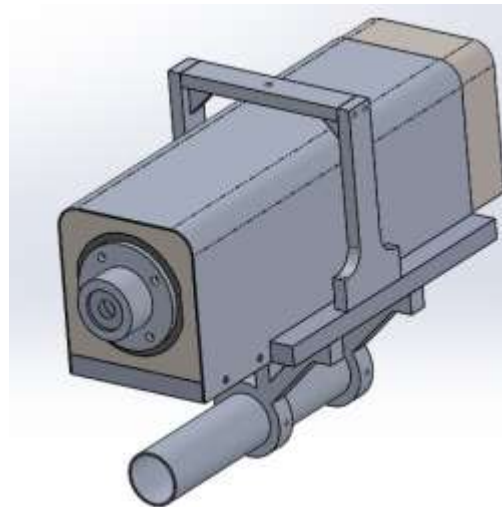


Camera Design



Initial Design

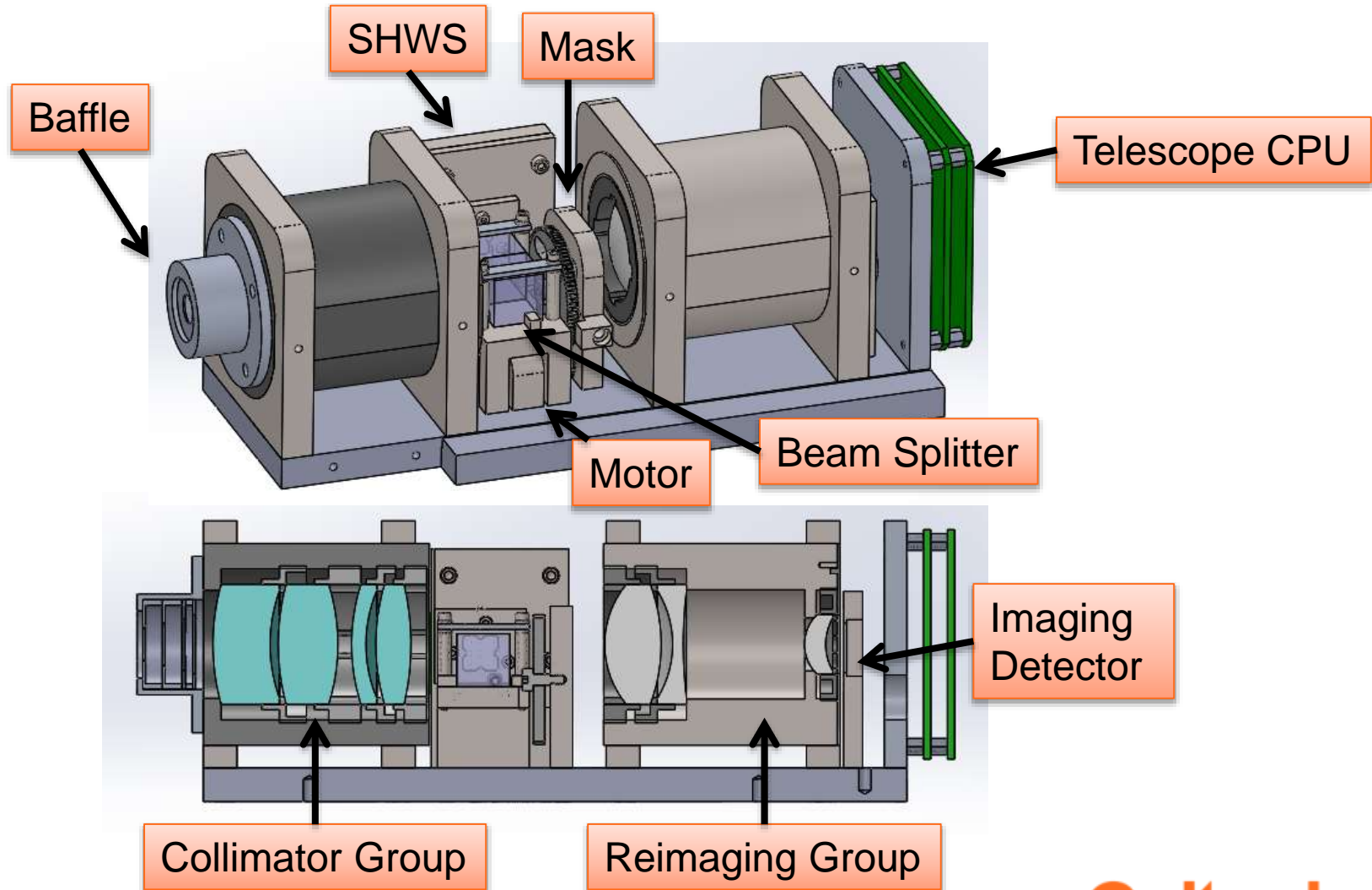
- Mechanical re-design after optical modeling
- Manufacture collimator & reimaging groups
- Mass ~ 2.9 kg



Current Design

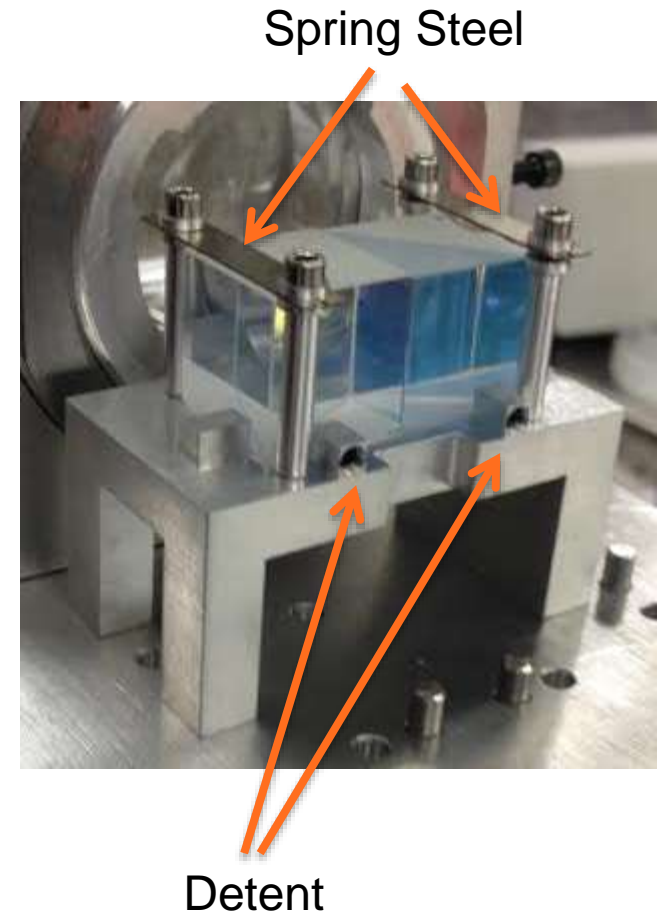
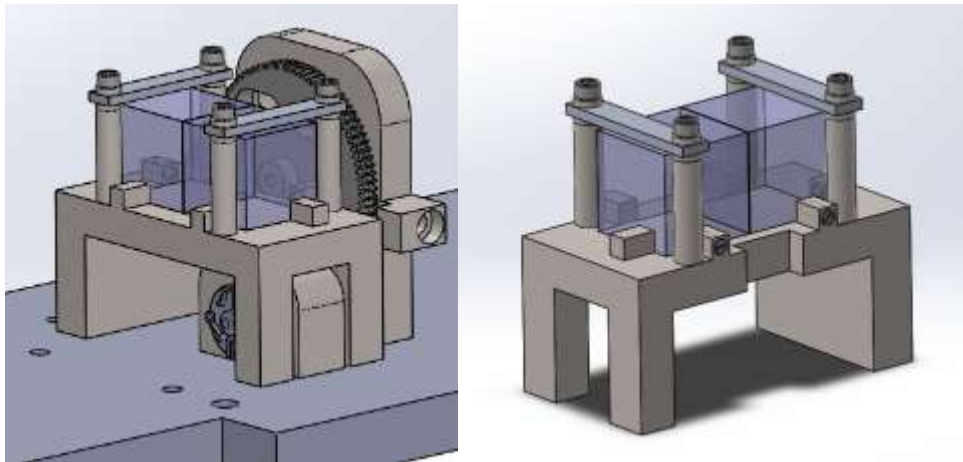
- Modifications due to interface design
- Finalized & manufactured prototype
- Initial Design for external interfaces
- Mass ~ 3.8 kg (with 10% margin)

Camera Mechanical



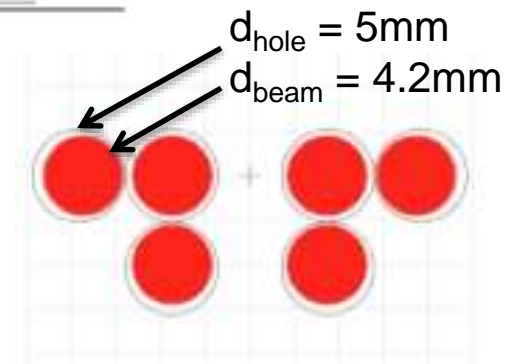
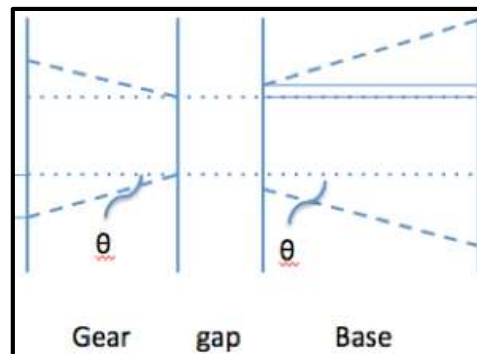
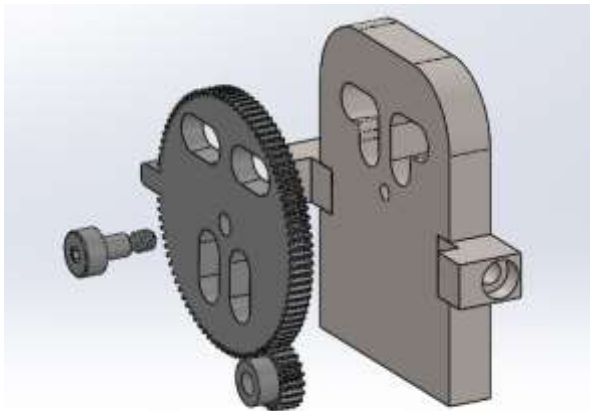
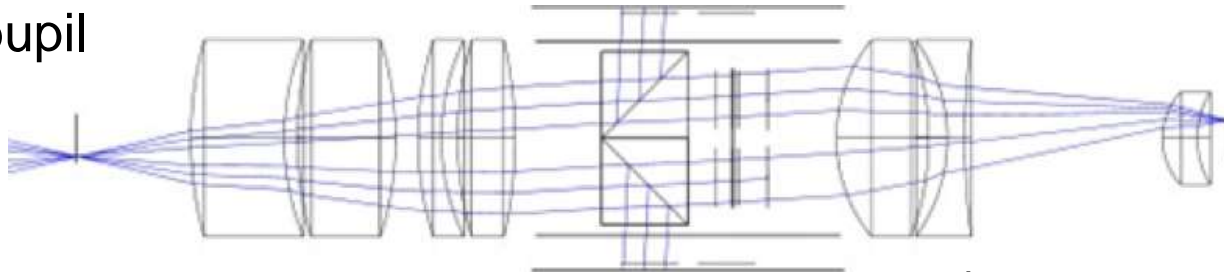
Beam Splitter Assembly

- Designed for integration of neighboring components
- Utilized detents and spring steel to allow for thermal expansion



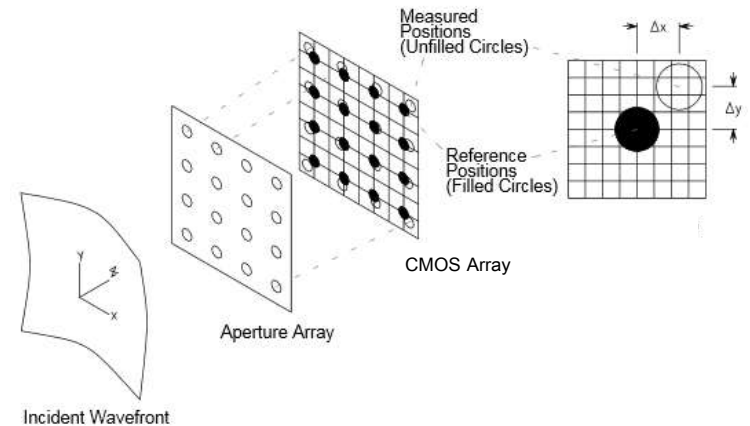
Mask Mechanism

- Designed for change between two configurations
- Used ray tracing software to determine optical path at max field angle (4° from pupil conjugate)

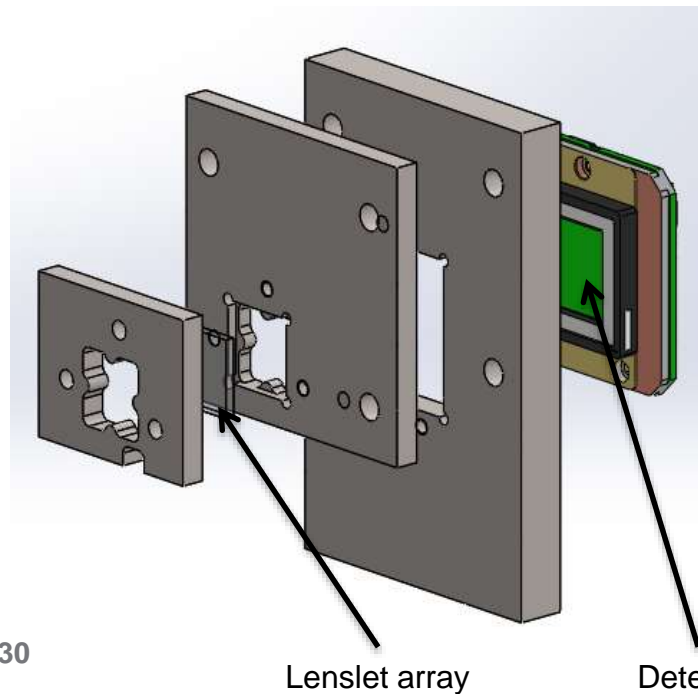


Shack-Hartmann Wavefront Sensor

- Designed a mount to account for:
 - Small space available
 - Mass
 - Alignment constraints
- Sank lenslet array into plate with RTV for padding



Spiricon Inc. (2004). Hartmann Wavefront Analyzer Tutorial [Online].
Available: http://www.ophiropt.com/user_files/laser/beamprofilers/tutorial-hartman.pdf

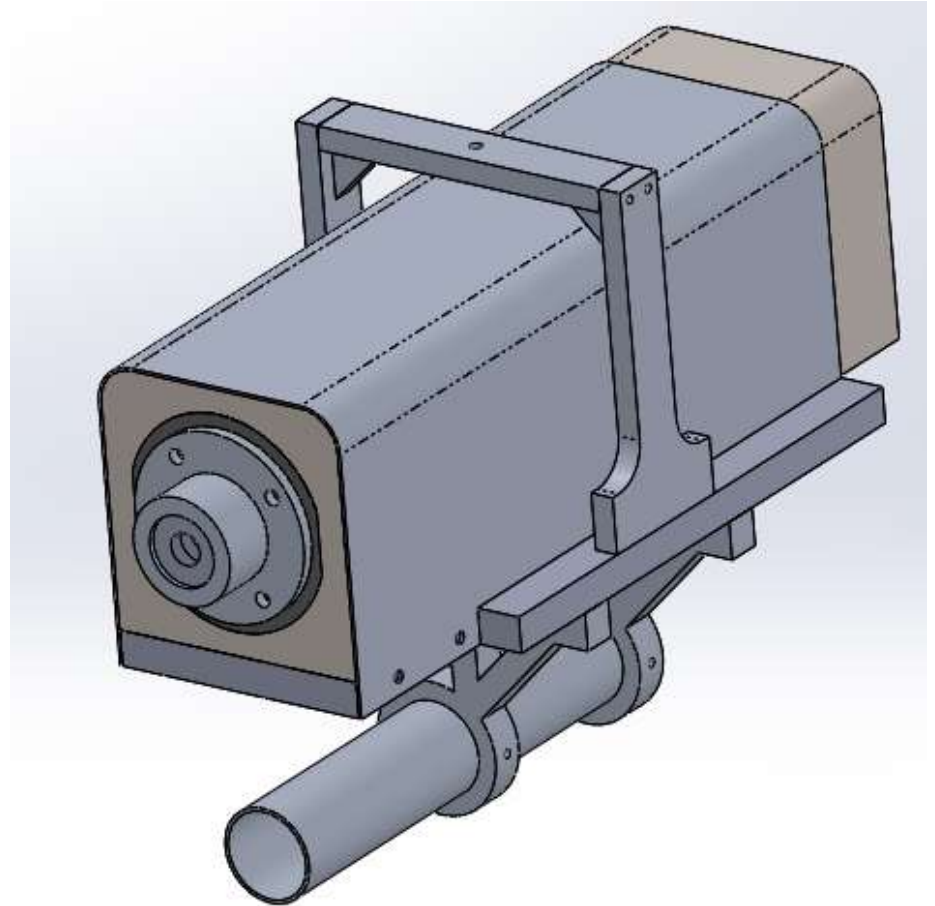


External Interfaces

- Frangibolt (FD04) for CoreSat interface
- Mount with mandrel for boom interface
- Interfaces aligned with camera CoM



* Image from TiNi Aerospace



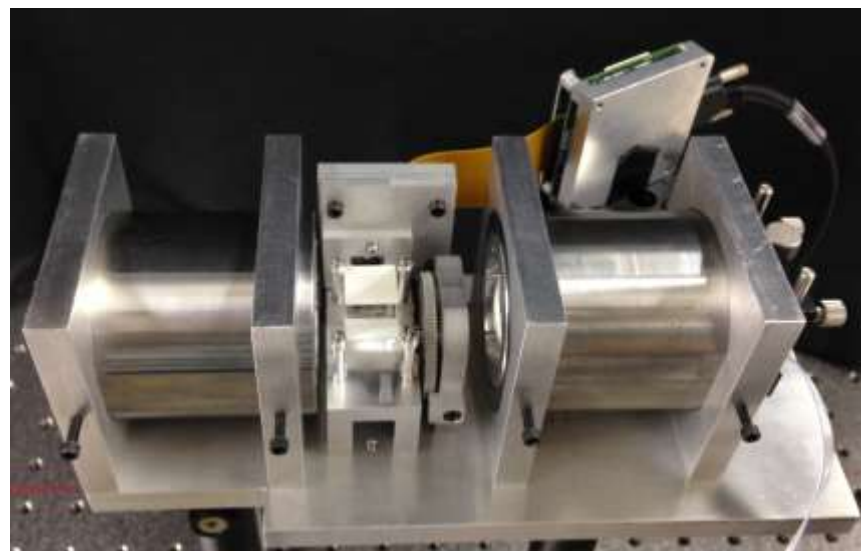
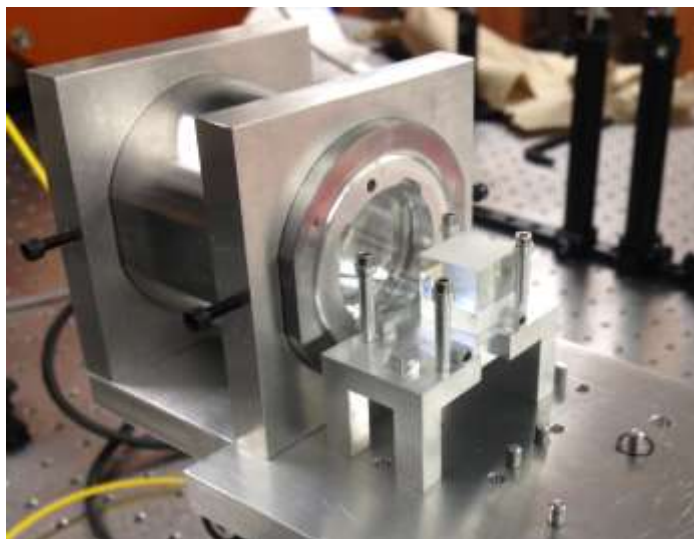
Test Plan

Component Level Testing

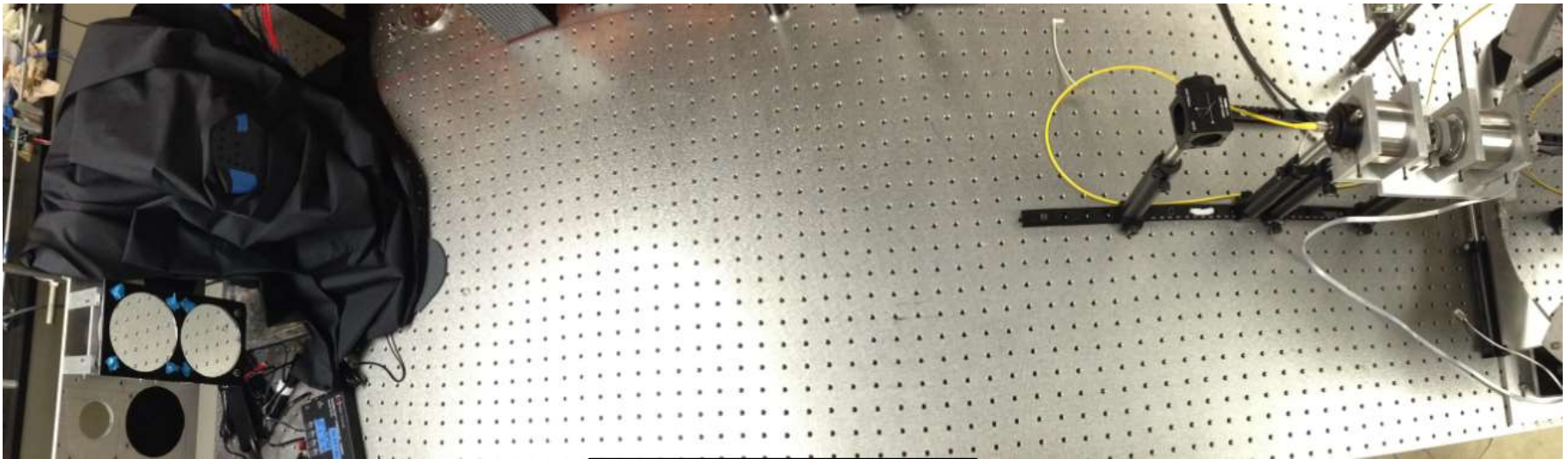
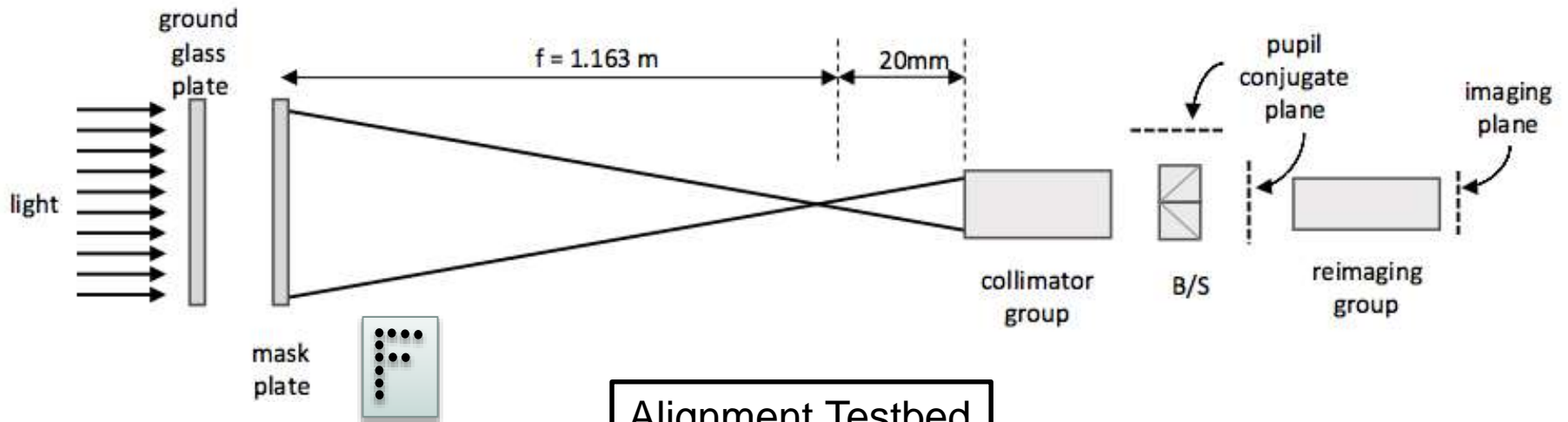
- ☐ Collimator Group
- ☐ Beam Splitter
- ☐ SHWS
- ☐ Mask Mechanism
- ☐ Reimaging Group
- ☐ Detector Mount

End to End Testing

- ☐ Verify Spot size
- ☐ Verify Spot shape
- ☐ Thermal Testing
- ☐ Shake Testing



Testbed Setup

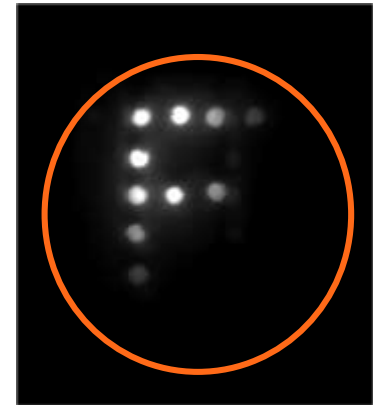
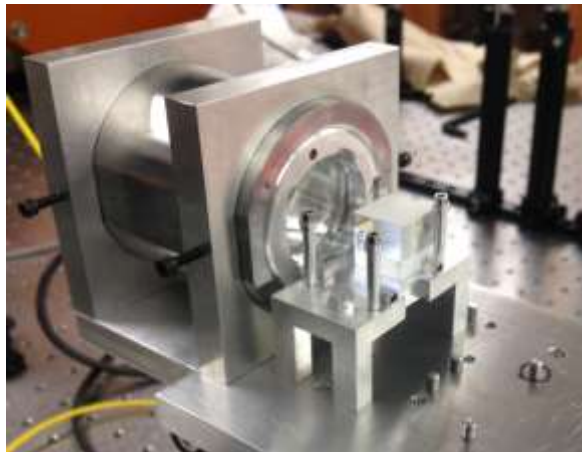


Pass/Fail Criteria

Component	Criteria
ALL	<ul style="list-style-type: none">• Light unobstructed & not scattered
Collimator Group	<ul style="list-style-type: none">• Light is collimated
Beam Splitter	<ul style="list-style-type: none">• Prism transmits & reflects along axis
SHWS	<ul style="list-style-type: none">• MLA is located at pupil conjugate• SHWS can process the wavefront• Measurements are repeatable
Mask	<ul style="list-style-type: none">• Pupil conjugate located at gear rear• Gears allow change in configuration
Reimaging Group	<ul style="list-style-type: none">• Focal point is at image detector surface
Imaging Detector	<ul style="list-style-type: none">• Image is on detector array

Pupil Conjugate Testing

- Assembly and alignment
- Collimated image
- Location of pupil conjugate and image size
- Main distortion is defocus



Raw data



Processed data superimposed
on actual image

SHWS Alignment

- Extract spot locations (x)
- Compare them to reference grid (o)
- Compute slope from the difference between the locations

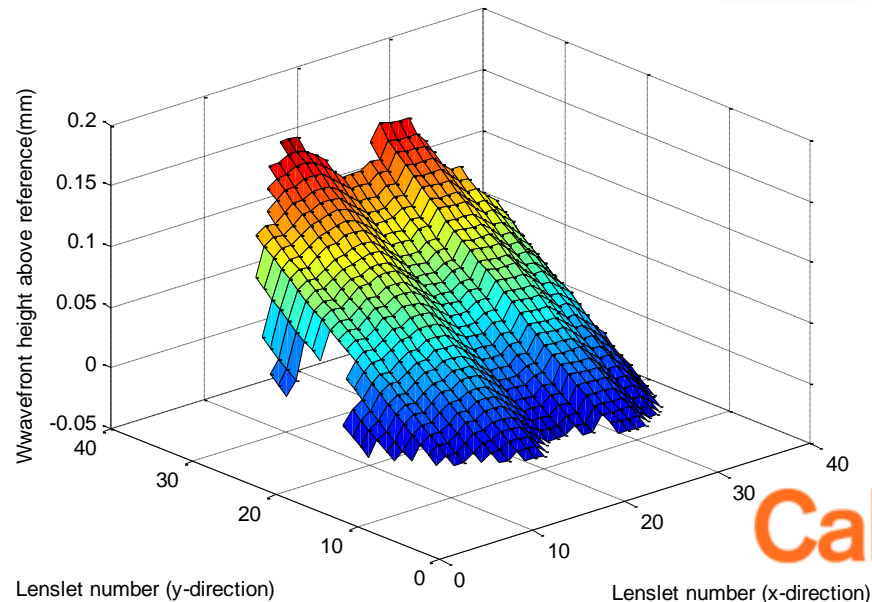
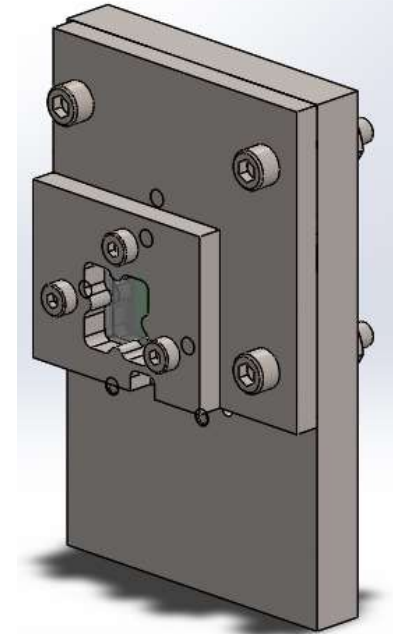
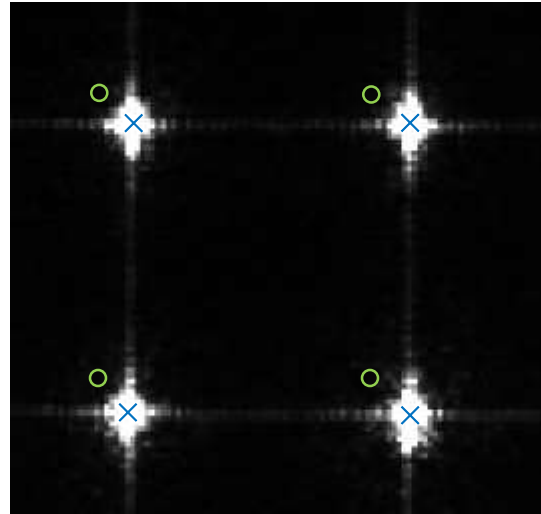
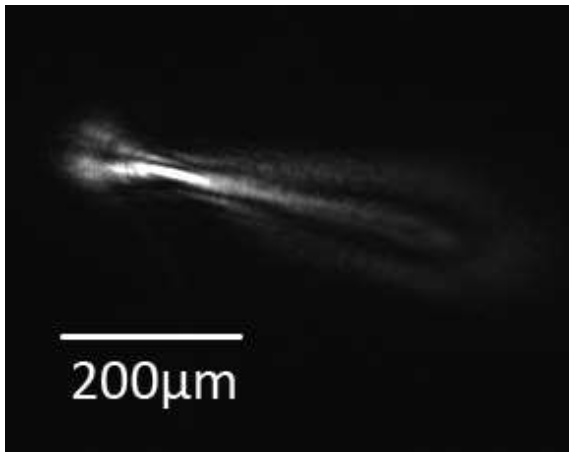
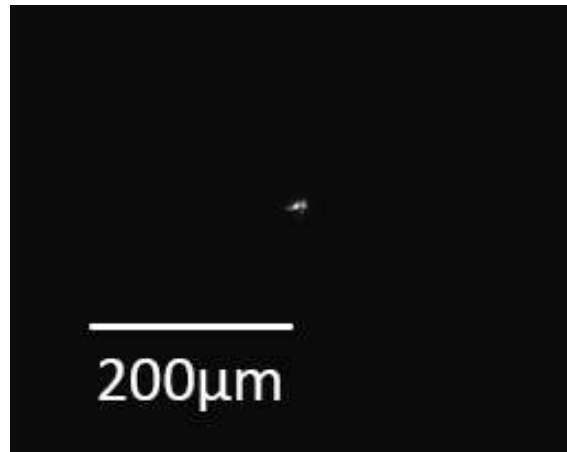


Image Detector Testing

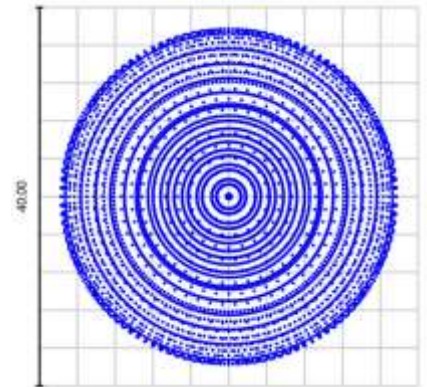
- Imaged with point source in test bed
- Deformations in resulting image:
 - Astigmatism due to misalignment in the full testbed
 - Coma due to off-axis spherical mirrors
- Placing point source at prime focus resulted in expected spot size ($36\text{ }\mu\text{m}$)



Full Testbed Set-Up



Point Source at Prime Focus



Predicted spot size = $36\text{ }\mu\text{m}$

Results

	Pass
	In-Progress
	Fail

Component	Criteria	Status
ALL	<ul style="list-style-type: none"> Light unobstructed & not scattered 	
Collimator Group	<ul style="list-style-type: none"> Light is collimated 	
Beam Splitter	<ul style="list-style-type: none"> Prism transmits & reflects along axis 	
SHWS	<ul style="list-style-type: none"> MLA is located at pupil conjugate SHWS can process the wavefront Measurements are repeatable 	
Mask	<ul style="list-style-type: none"> Pupil conjugate located at gear rear Gears allow change in configuration 	
Reimaging Group	<ul style="list-style-type: none"> Focal point is at image detector surface 	
Imaging Detector	<ul style="list-style-type: none"> Image is on detector array 	

Conclusion

Progress

- ✓ Re-designed existing CAD for manufacturability
- ✓ Fabricated & assembled camera prototype
- ✓ Developed a test plan for both prototype & flight
- ✓ Initiated component level testing

Future Work

- ☐ Complete prototype testing
- ☐ Integrate stepper motor
- ☐ Integrate electronics
- ☐ Integrate light shielding
- ☐ Finalize external interfaces
- ☐ Conduct environmental testing

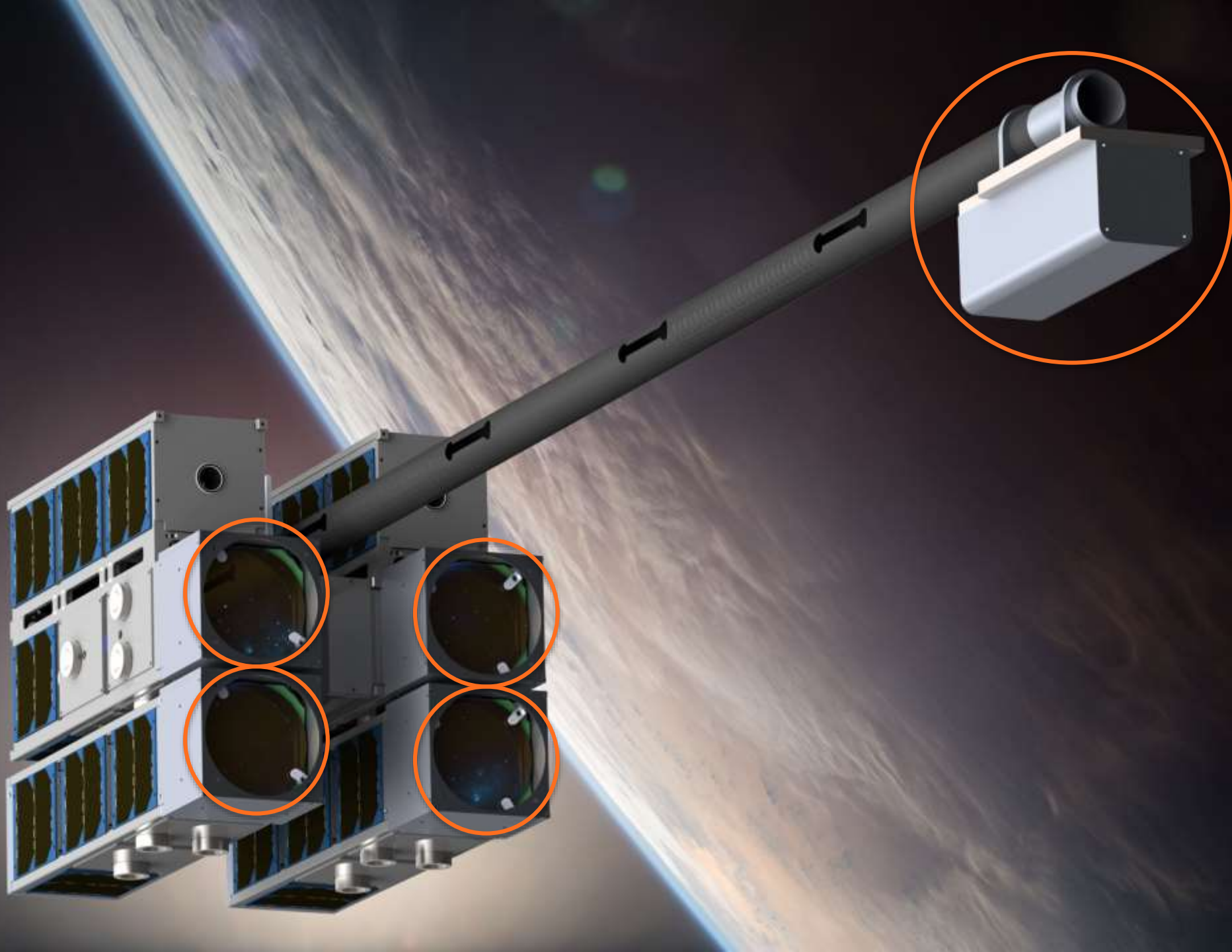
Questions?

Mirror Calibration Algorithms

Joseph Bowkett

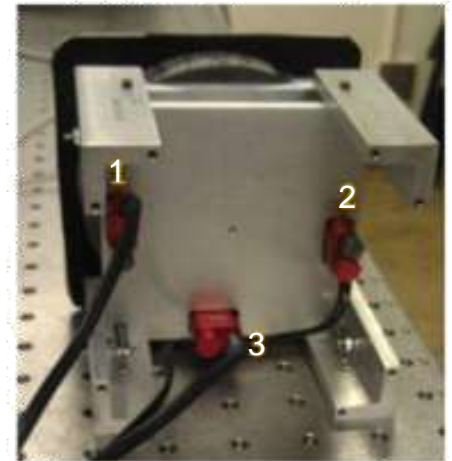
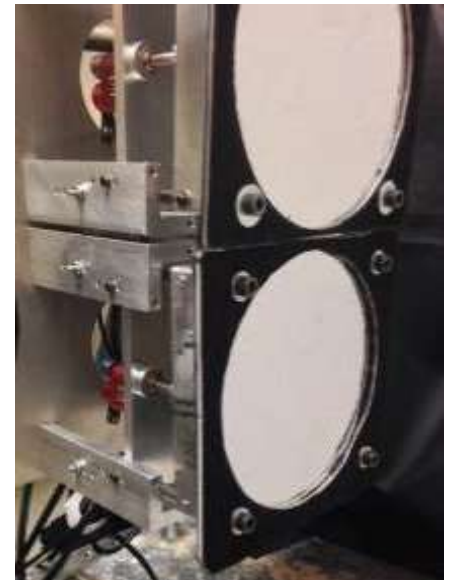
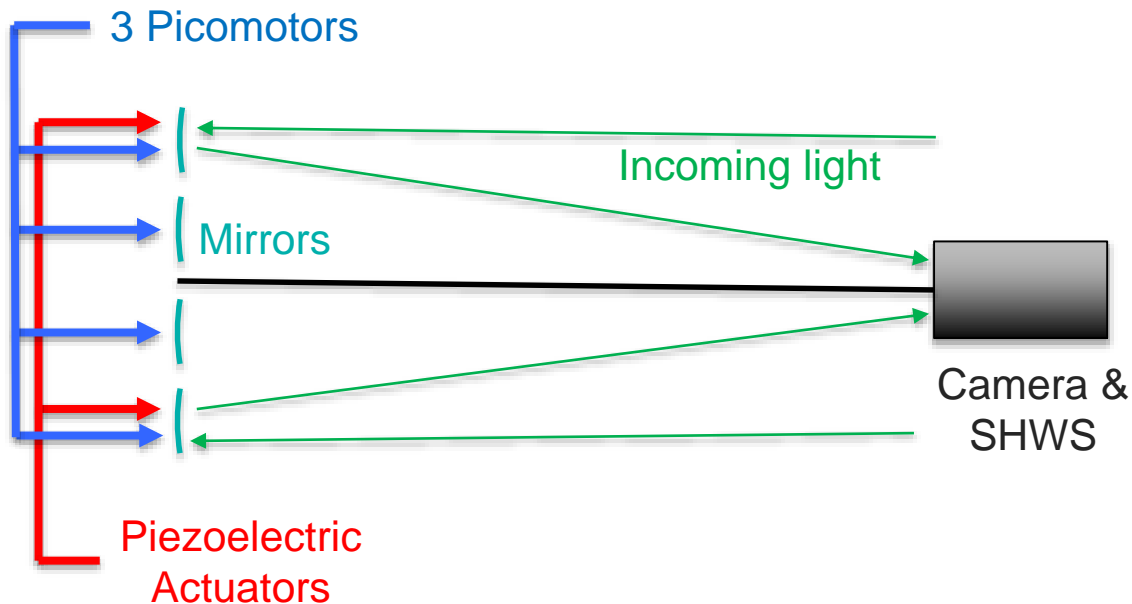
Greg Phlipot

Mentor: Melanie Delapierre,
Thibaud Talon



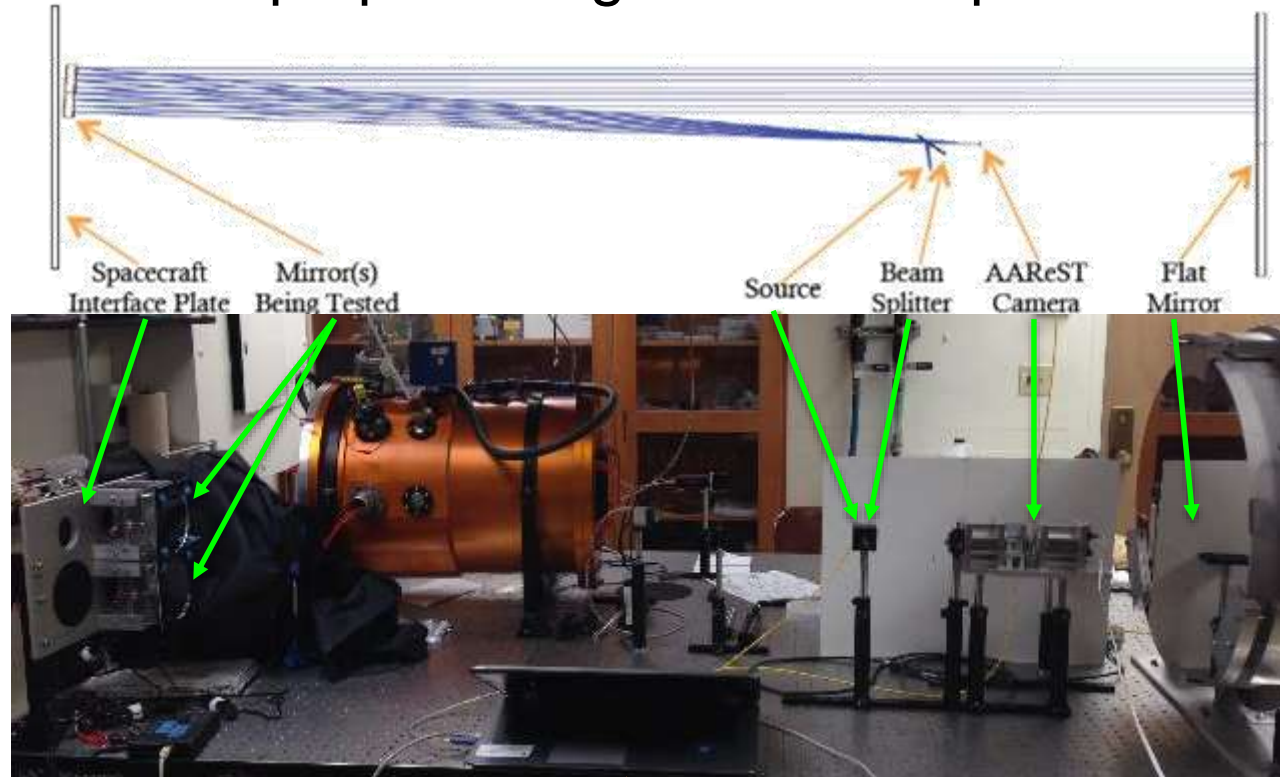
Overview

- Point, center, and focus four mirrors in reasonable time
- Wavefront error correction
- Implementation and experimental testing



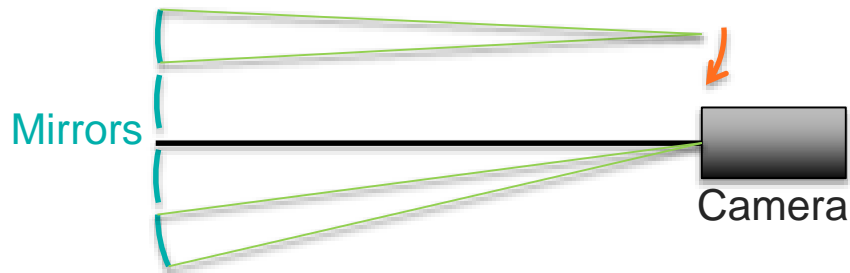
Telescope Testbed

- 2 rigid mirrors with three picomotors each
- Autocollimated light represents distant star
- Linux laptop with flight CPU compatible libraries

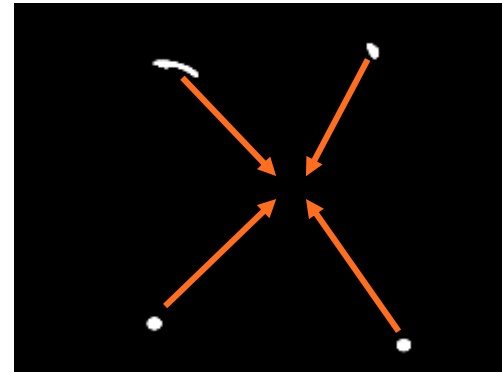


Algorithm sequence

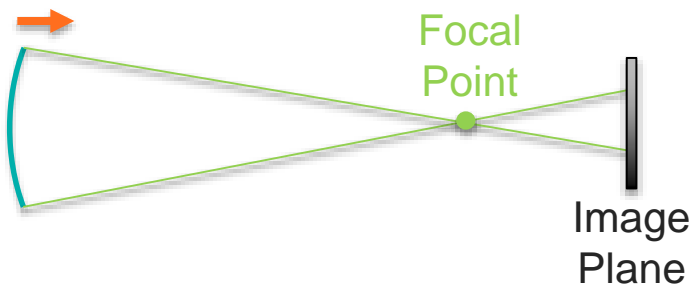
1. Blind search



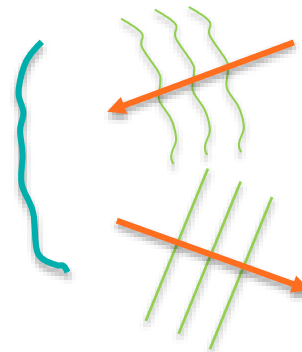
2. Centering



3. Focusing

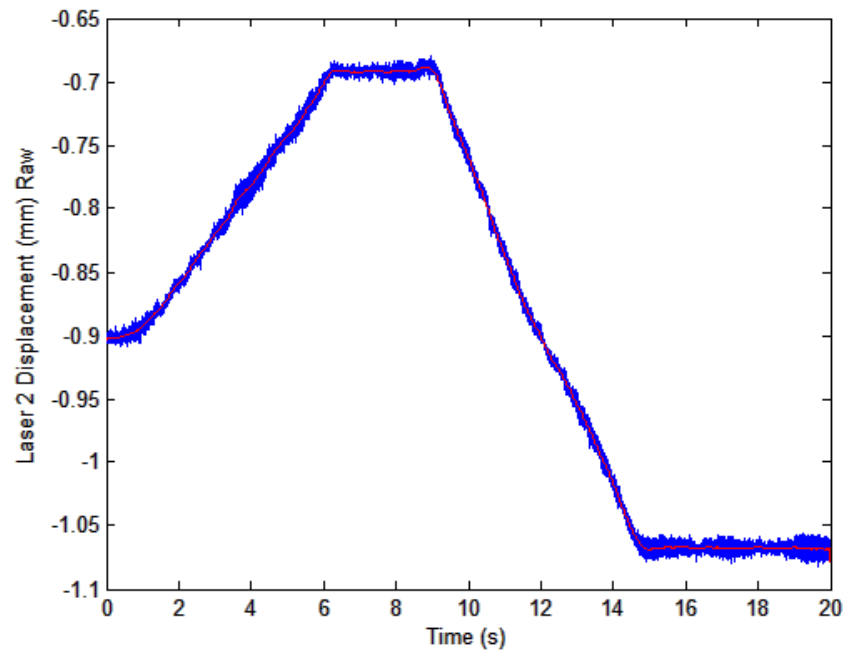


4. Shape correction



Picomotor Characterization

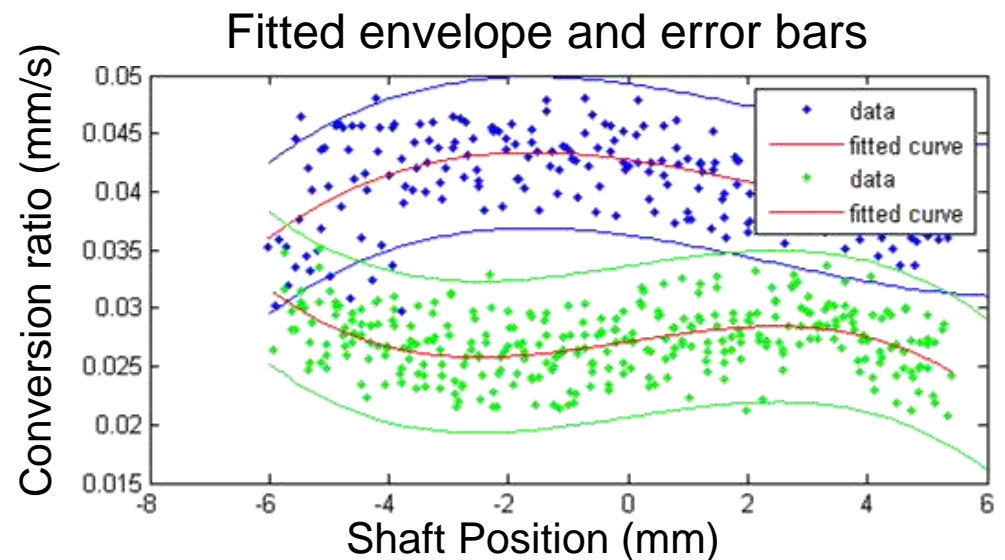
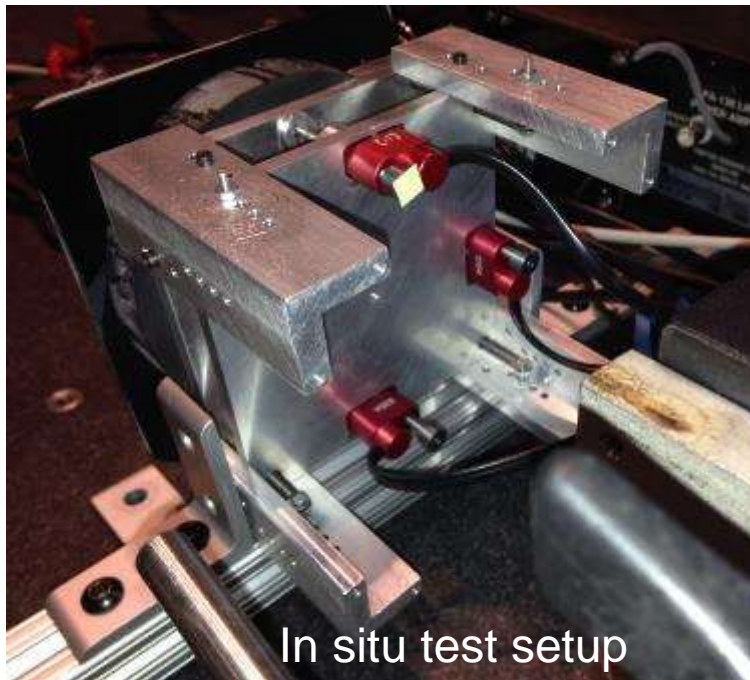
- Need consistent actuation for open loop control
- Forward and reverse directions different



Picomotor Characterization

- Non-linear axial spring force causes change along stroke
- Curve can be used but still has significant variance

$$\frac{\sigma_{std\ dev}}{\mu_{mean}} \approx 0.1$$

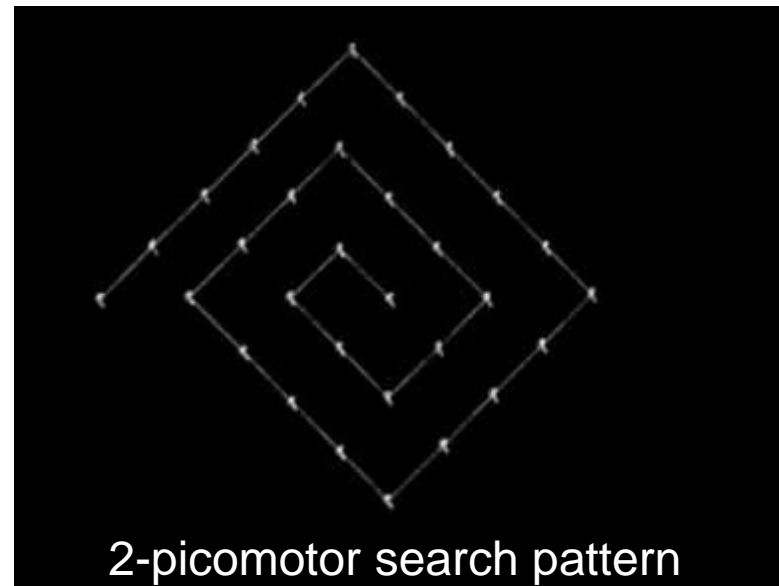


Blind Search

- Used to point mirrors toward image detector
- No sensor data, literally shooting in the dark
- Previously used 2 picomotors

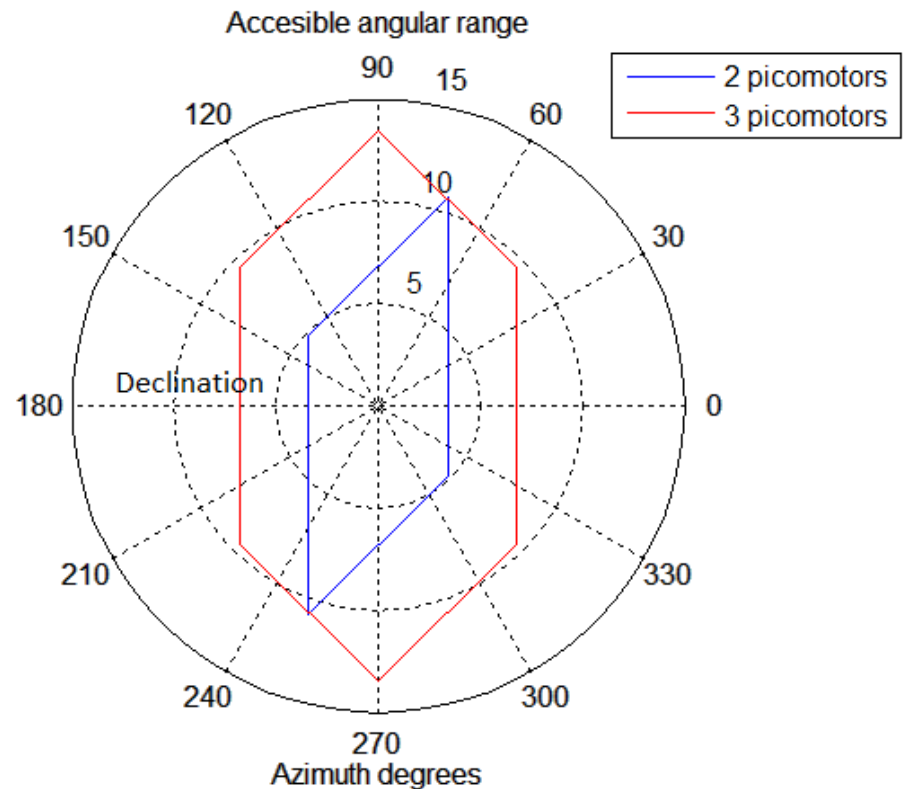
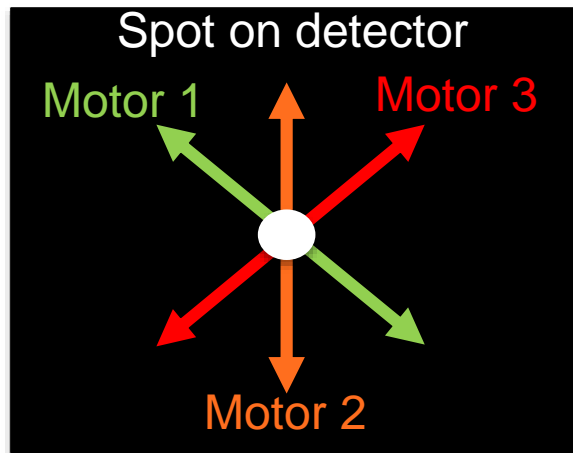
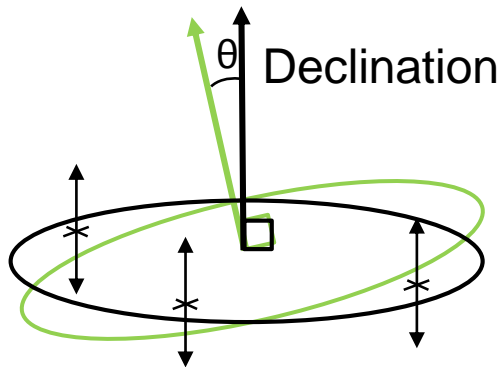
Our Tasks

- Extend to 3 picomotors
- Investigate repeatability



Blind Search

- Added a degree of freedom to search pattern

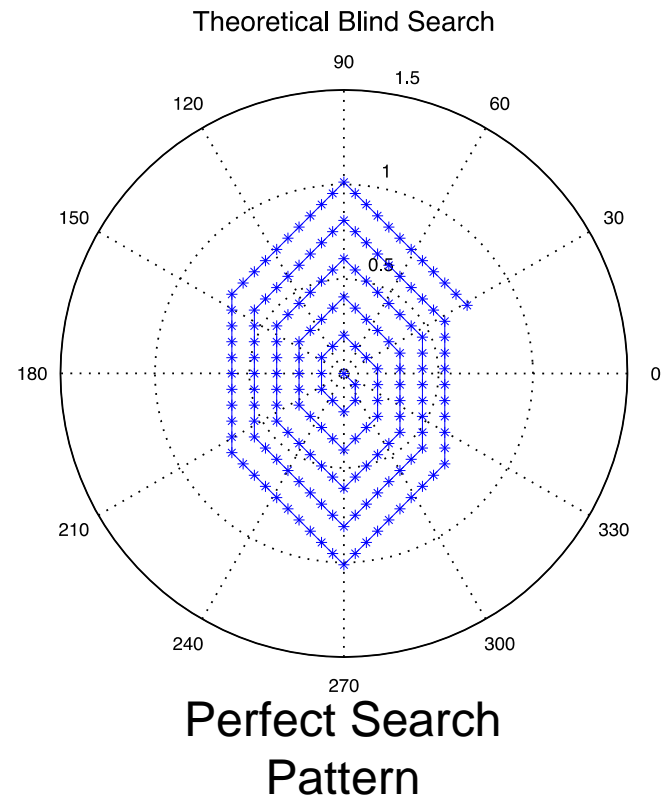


Blind Search

- Actuation variance can cause search to miss detector

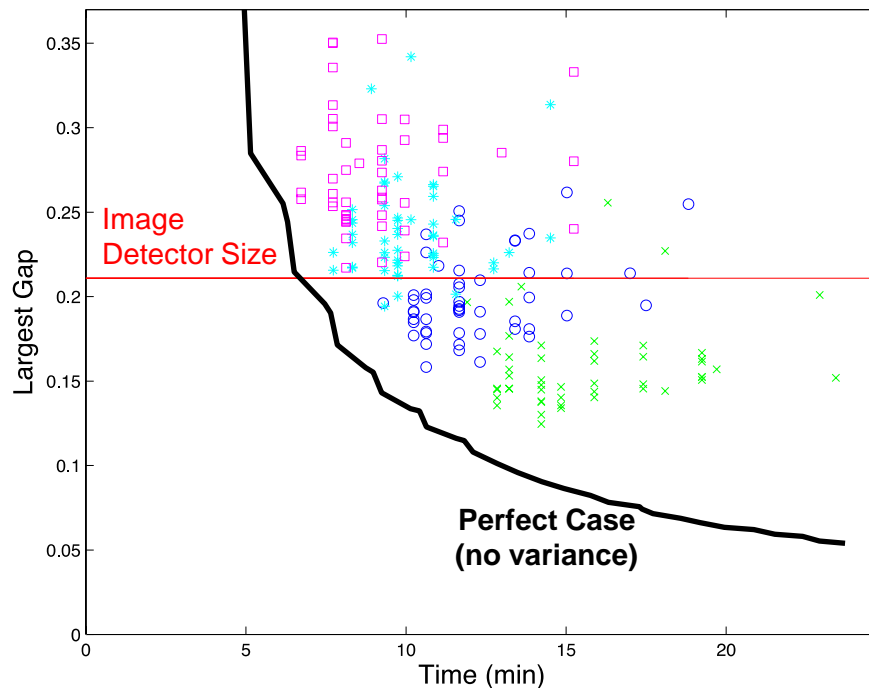


Reduced scale blind search

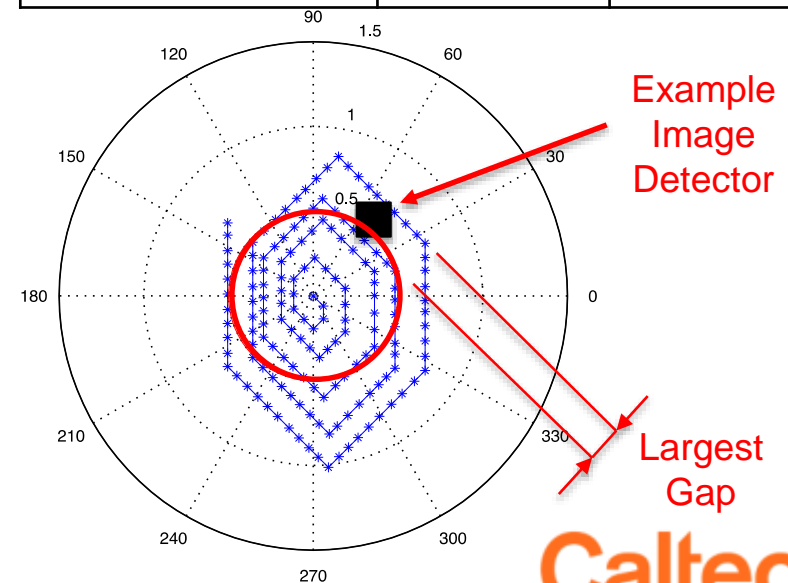


Blind Search

- Simulation shows success rate by step size for 0.5 degrees
- Needs to be considerably less than $\frac{1}{2}$ orbit (45 min)

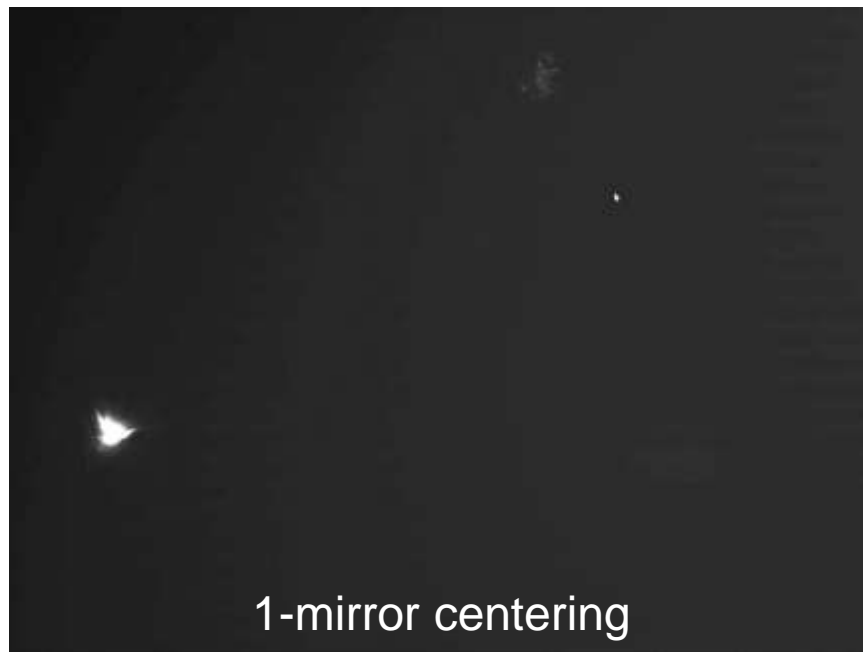


Step Size (mm/step)	Success %	Avg Time (min)
0.052	94%	15.9
0.069	74%	12.2
0.086	12%	10.0
0.104	0%	9.1



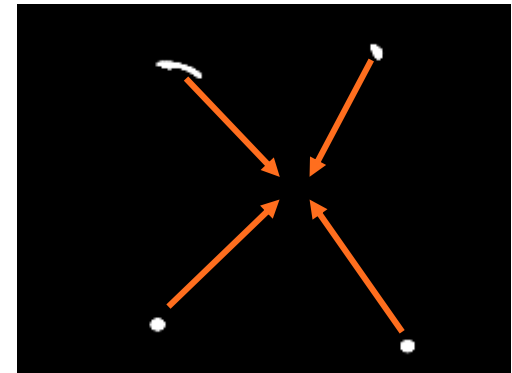
Centering

- Places spots corresponding to all mirrors in center of image detector
- Previously written for 1 spot

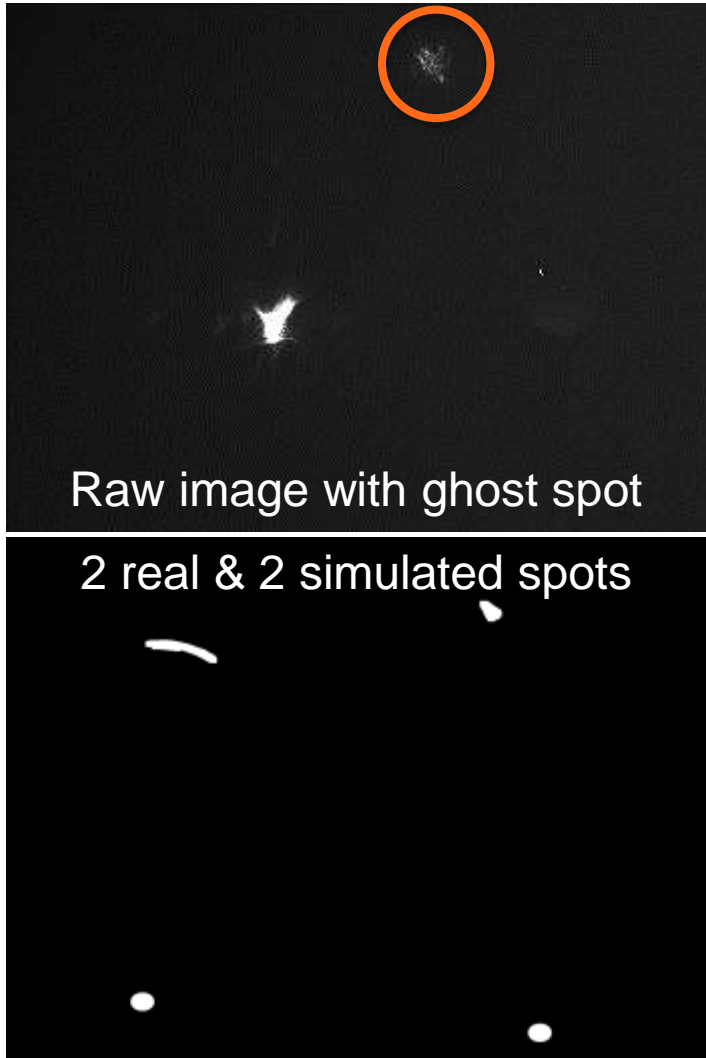


Our Tasks

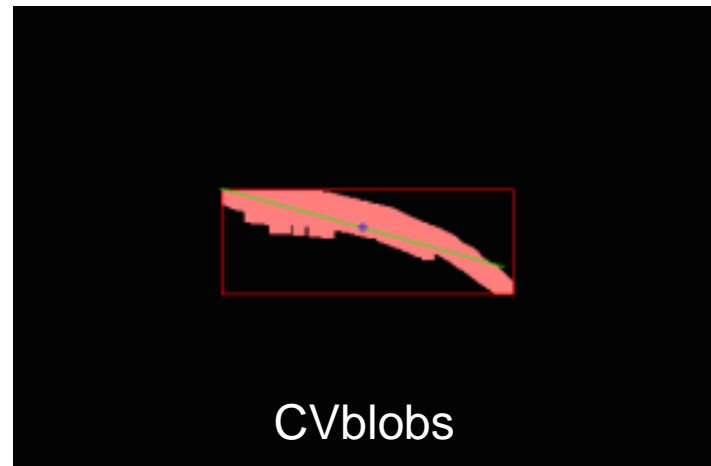
- Extend to multiple spots
- Improve robustness



Centering: Image Processing

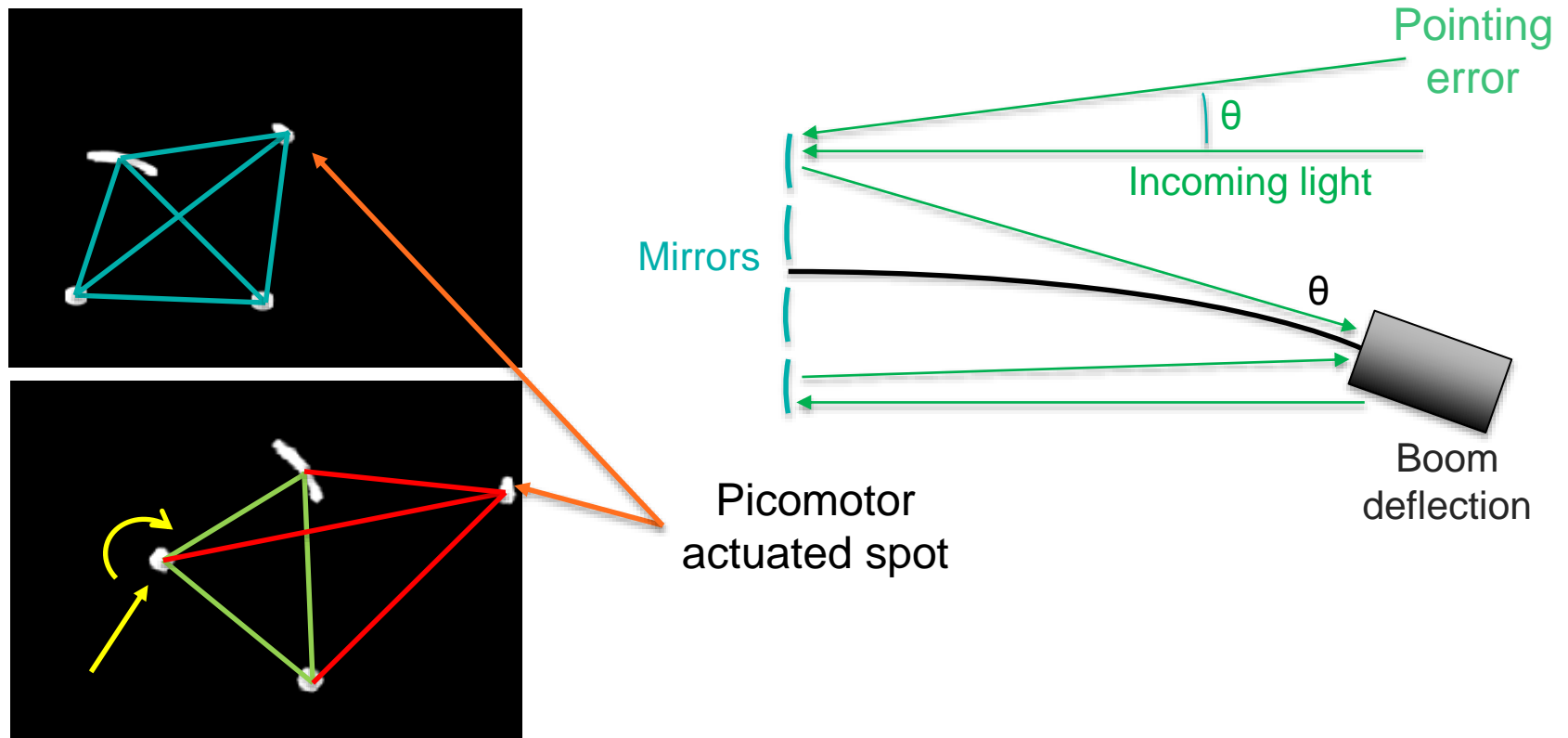


- Eliminate ghost images
- Simulate additional 2 spots
- Centroid and area detection

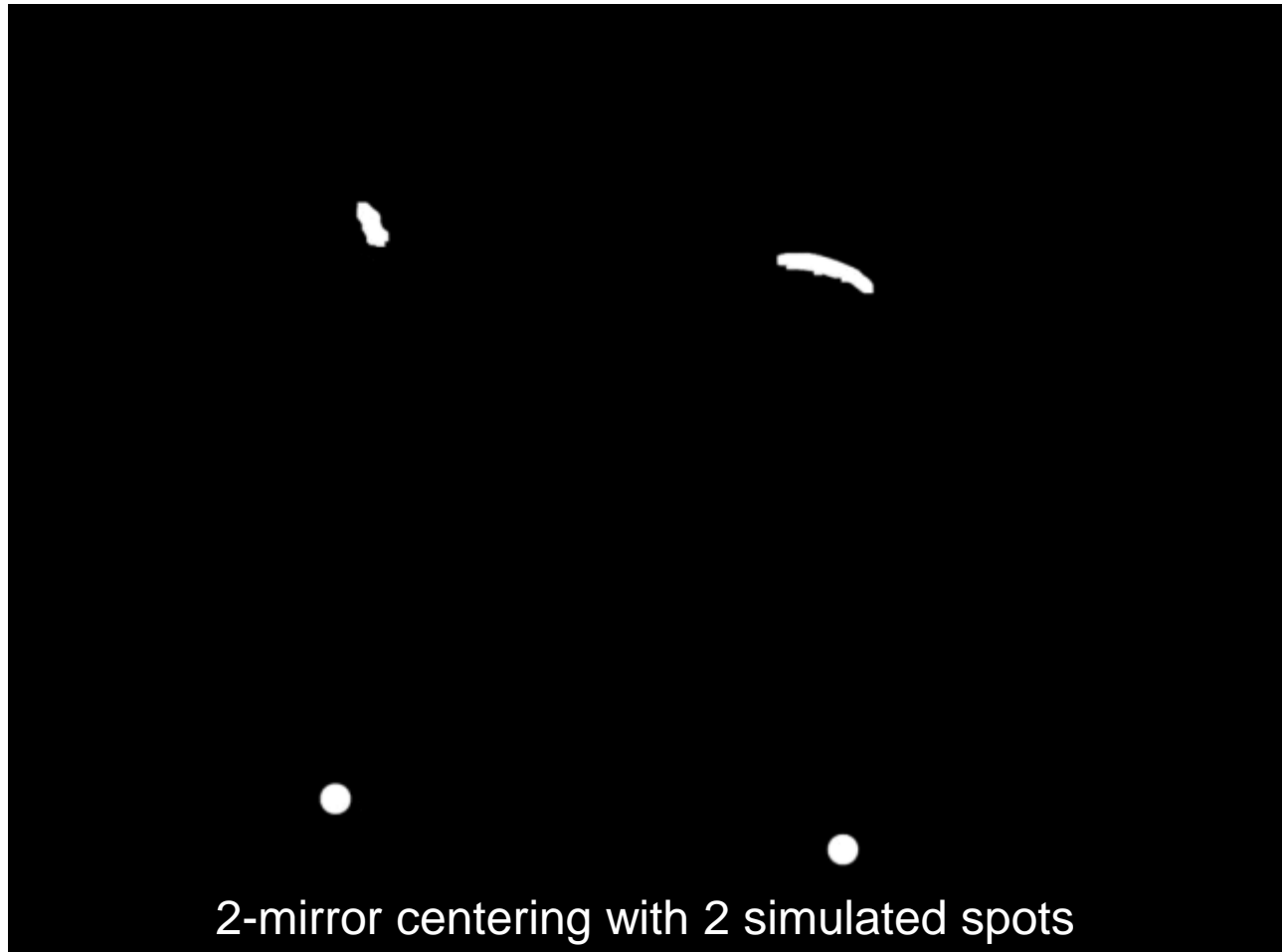


Centering: Rigid Body Motion

- Rigid body motion of all spots from transverse or torsional boom deflection & pointing error



Centering



Focusing

- Moves mirrors in piston to focus images
- Change in spot size undetectable

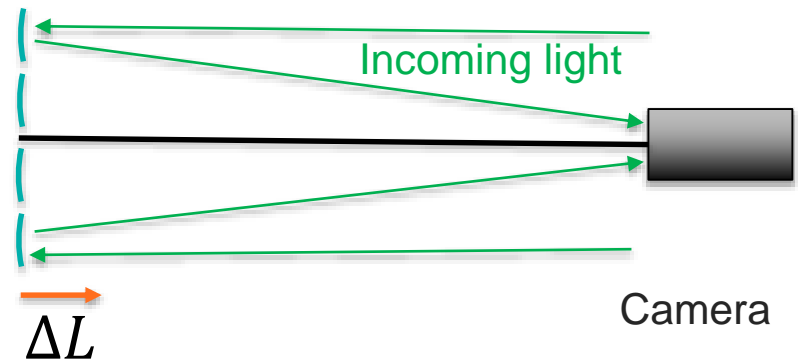
$$\Delta d = 1.22 \frac{\lambda \cdot \Delta L}{D}$$

d = spot size

λ = wavelength

L = focal length

D = mirror diameter

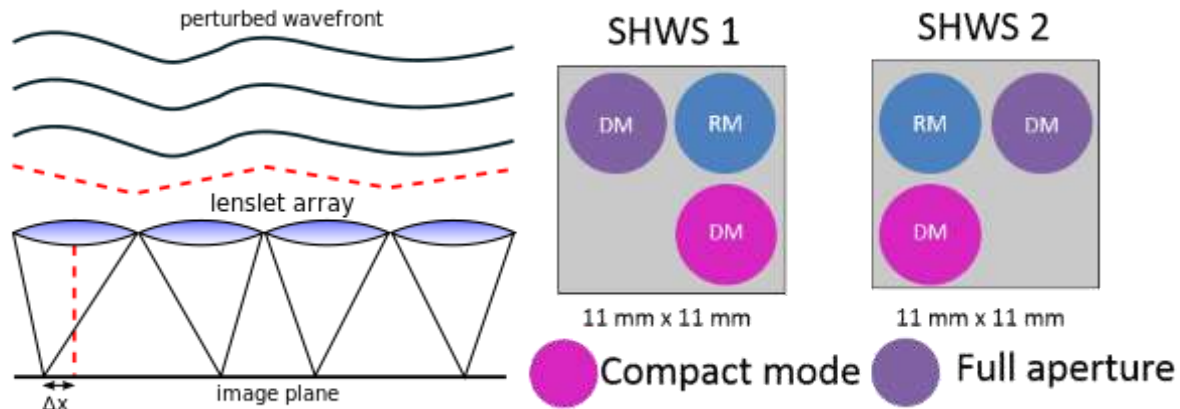
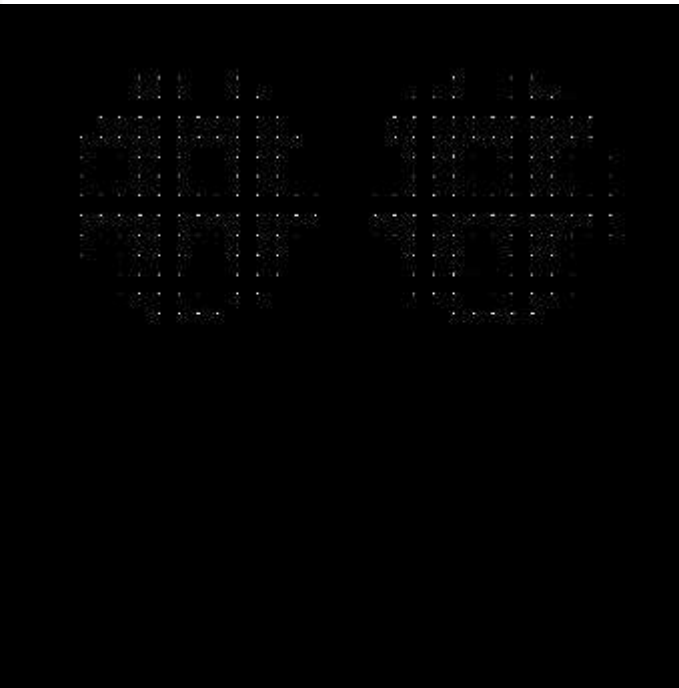


$$\Delta d \approx 60\text{nm}$$

$$\text{Pixel size} = 2.2\mu\text{m}$$

Shape Correction

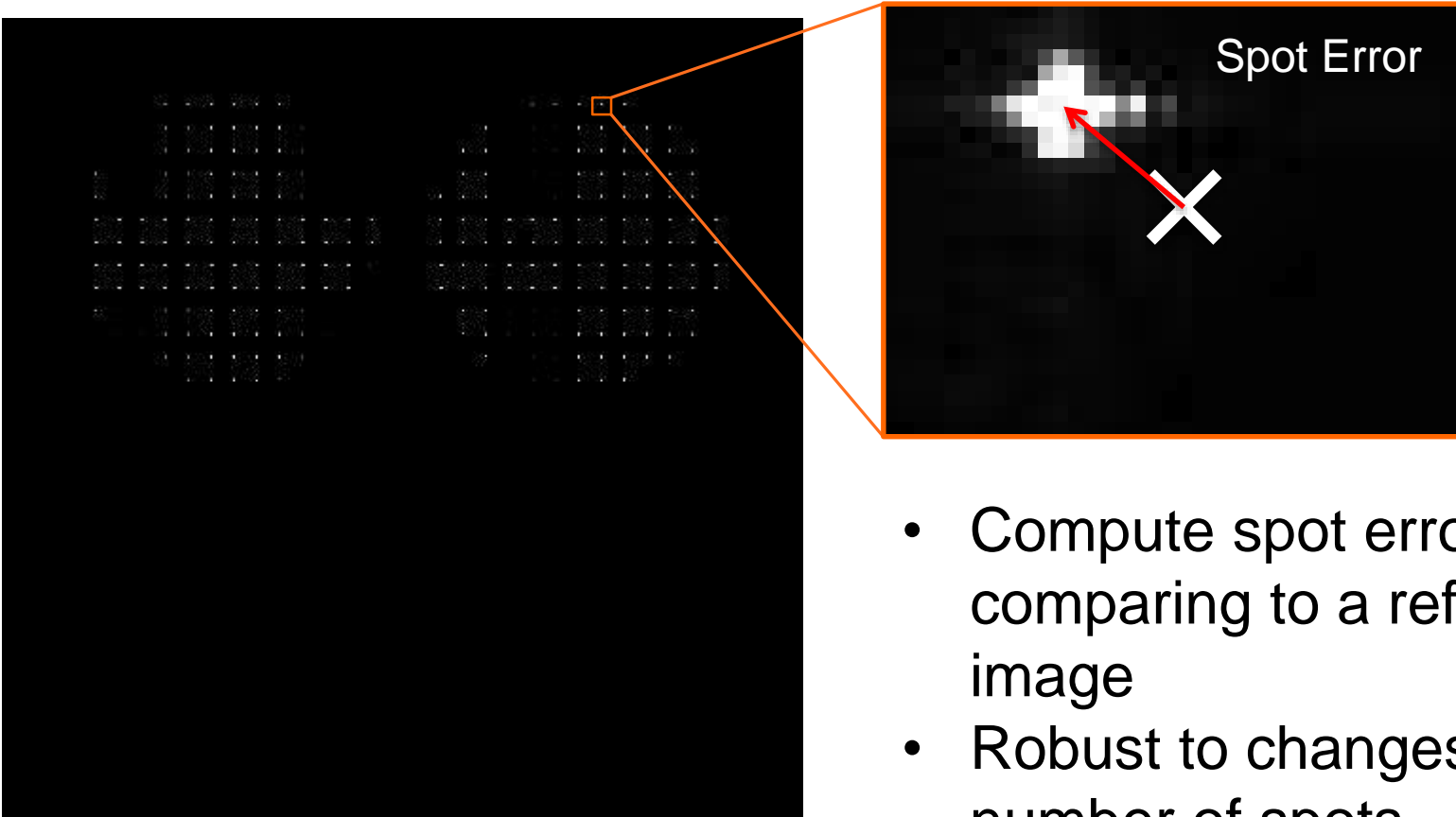
- Uses 41 piezoelectric actuators to correct shape of deformable mirrors



Our Tasks

- SHWS image processing
- Simulation of closed loop control

Shape Correction

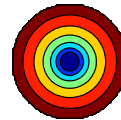


- Compute spot errors by comparing to a reference image
- Robust to changes in number of spots

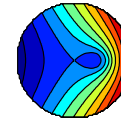
Shape Correction

- Constrained least squares minimization
- Simulated nonlinearity in actuators by adding in error

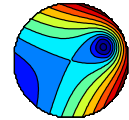
Influence Function 1



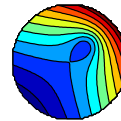
Influence Function 2



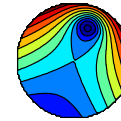
Influence Function 3



Influence Function 4



Influence Function 5



Influence Function 6



Precompiled

Create Jacobian Matrix from Influence Functions

Interpolate Jacobian at Reference Spot Locations

Separate Deformed Image into Mirror Regions

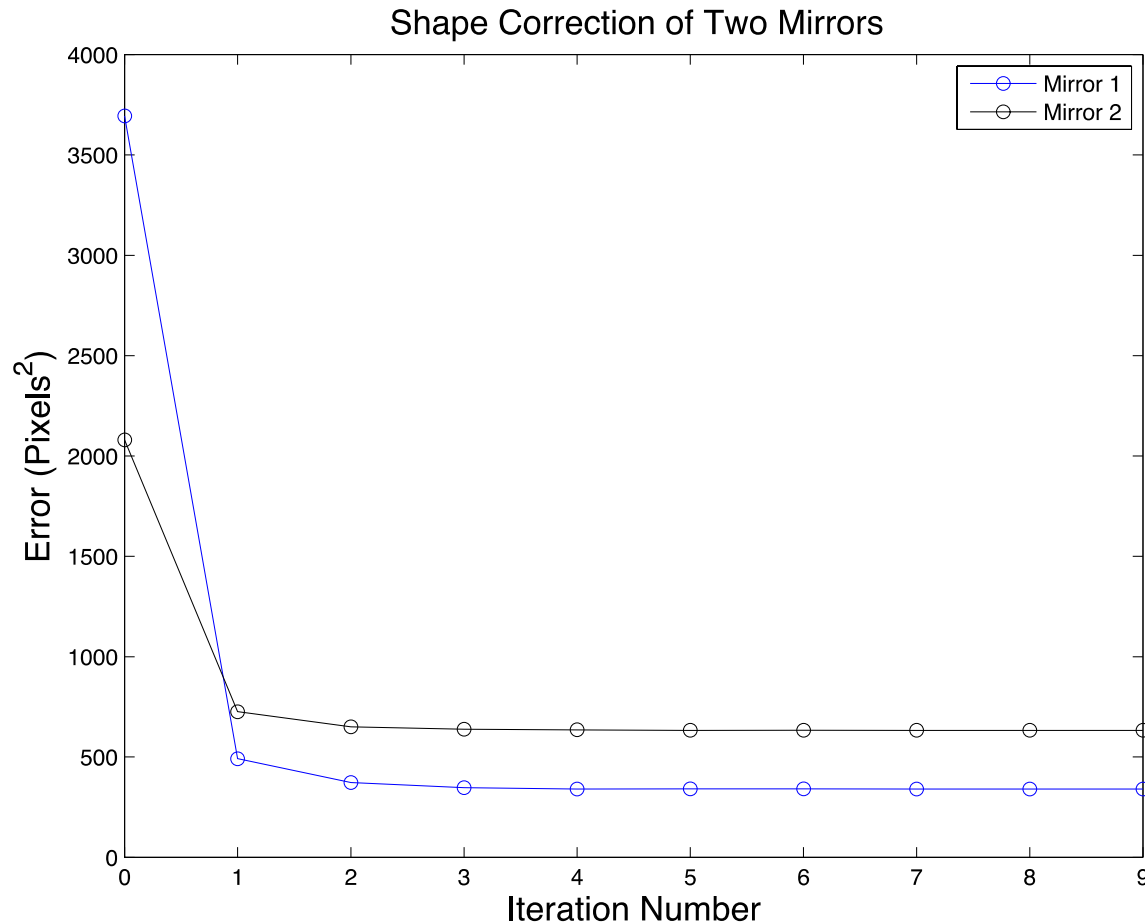
At runtime

Calculate Spot Errors

Minimize $|J^*u - \delta|$
 $V_{\min} < u < V_{\max}$

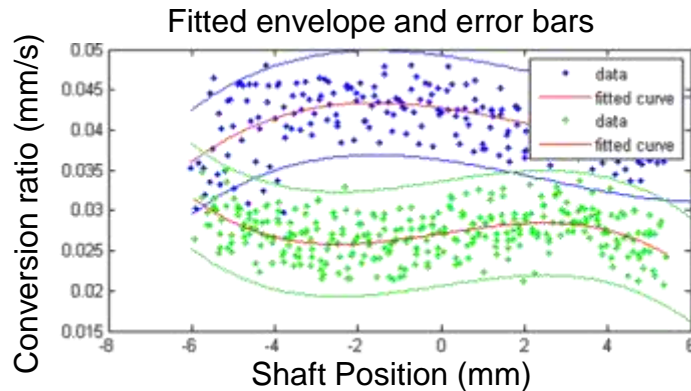
Introduce Error

Shape Correction

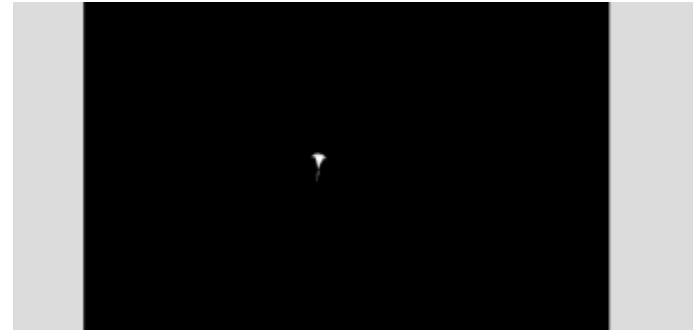


Summary

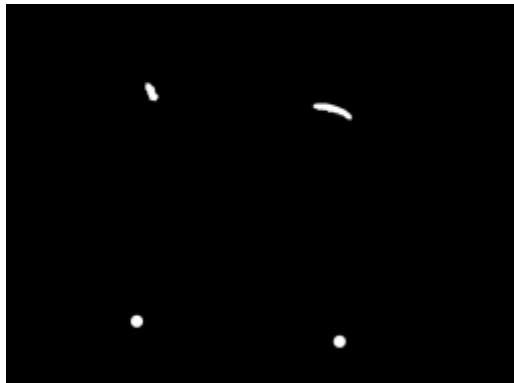
Characterized Picomotors



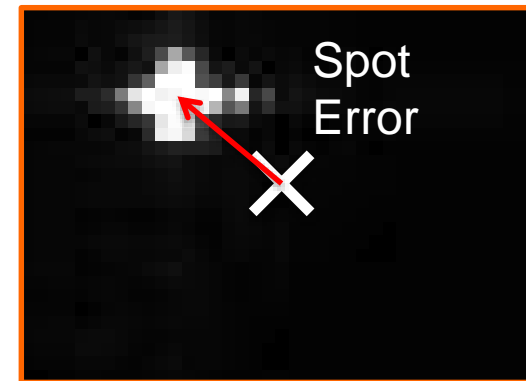
Improved Blind Search



Extended Centering Capabilities



Simulated Deformable Mirrors



Future Work

- Test rigid body algorithm on full complement of mirrors
- Test deformable mirror algorithm on telescope testbed
- Adapt focusing to use SHWS data
- Test algorithms on the flight CPU

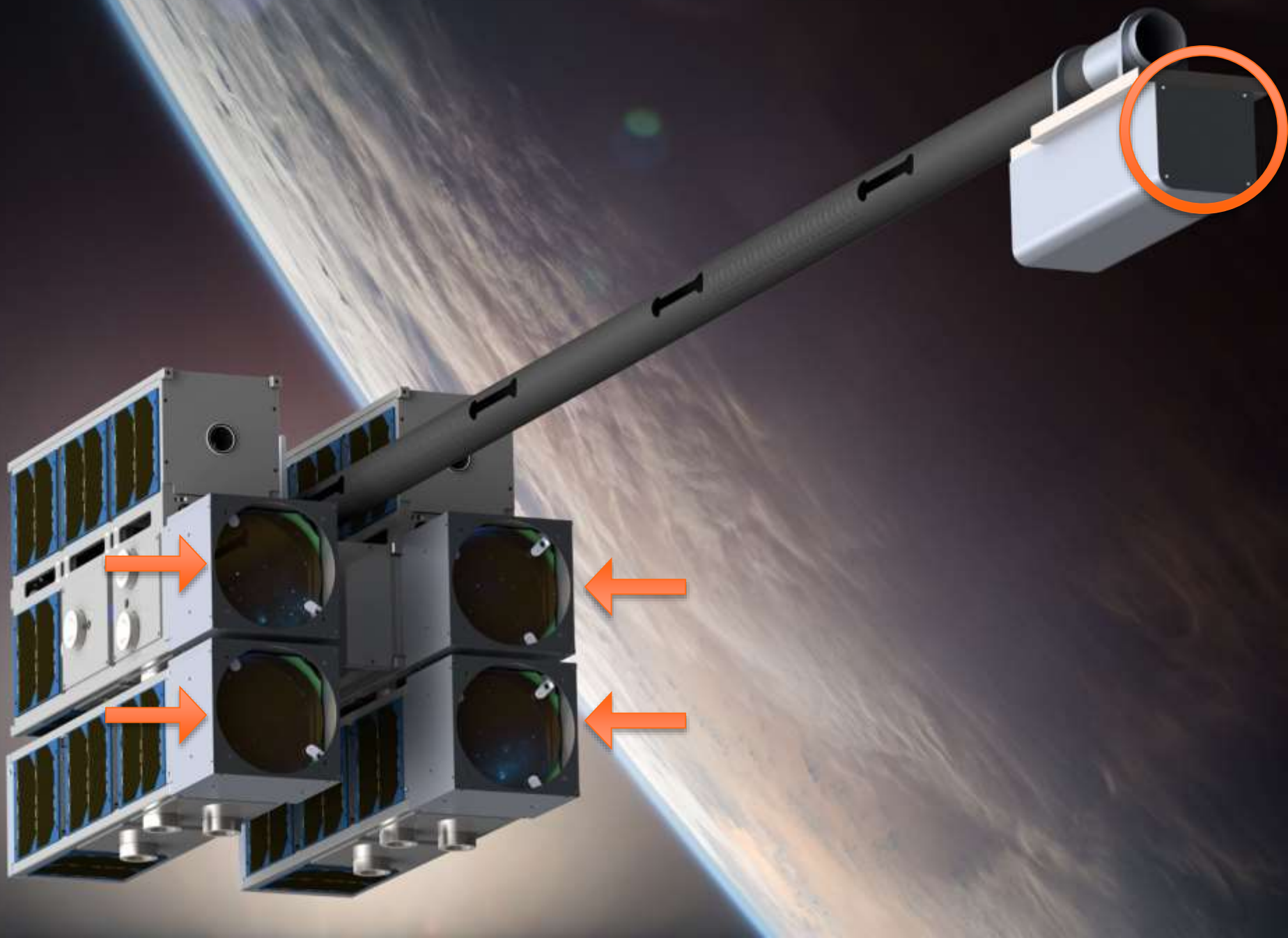
Questions?

O is for OBSW

Onboard Software

Finn Carlsvi
Chiraag Nataraj

Mentor: Yuchen Wei
Adviser: Dan Scharf



Purpose of On-Board Software



- Controls hardware
- Enables autonomy
- Relays science and engineering data
- Fault detection and recovery

Overall Group Task

- Analyze mission requirements
- Define an overall software architecture
- Implement design

Achievements

- Performed a detailed mission analysis
- Designed the OBSW framework
- Implemented the OBSW on flight hardware

Detailed Mission Analysis

Mission Analysis
System Architecture
Design Implementation

- Gathered information from other teams
- Mission Requirements Document (MRD)
 - Based on ConOps and team meetings
 - Used James Webb Space Telescope MRD as template
- Software Requirements Specification (SRS)
 - Based on MRD
 - Used IEEE 830 standard
 - Used as foundation for system design

- Software Requirements Specification
 - Functional requirements
 - Non-functional requirements
 - Interface definitions and communication standards
 - Provides traceability
 - Provides testability

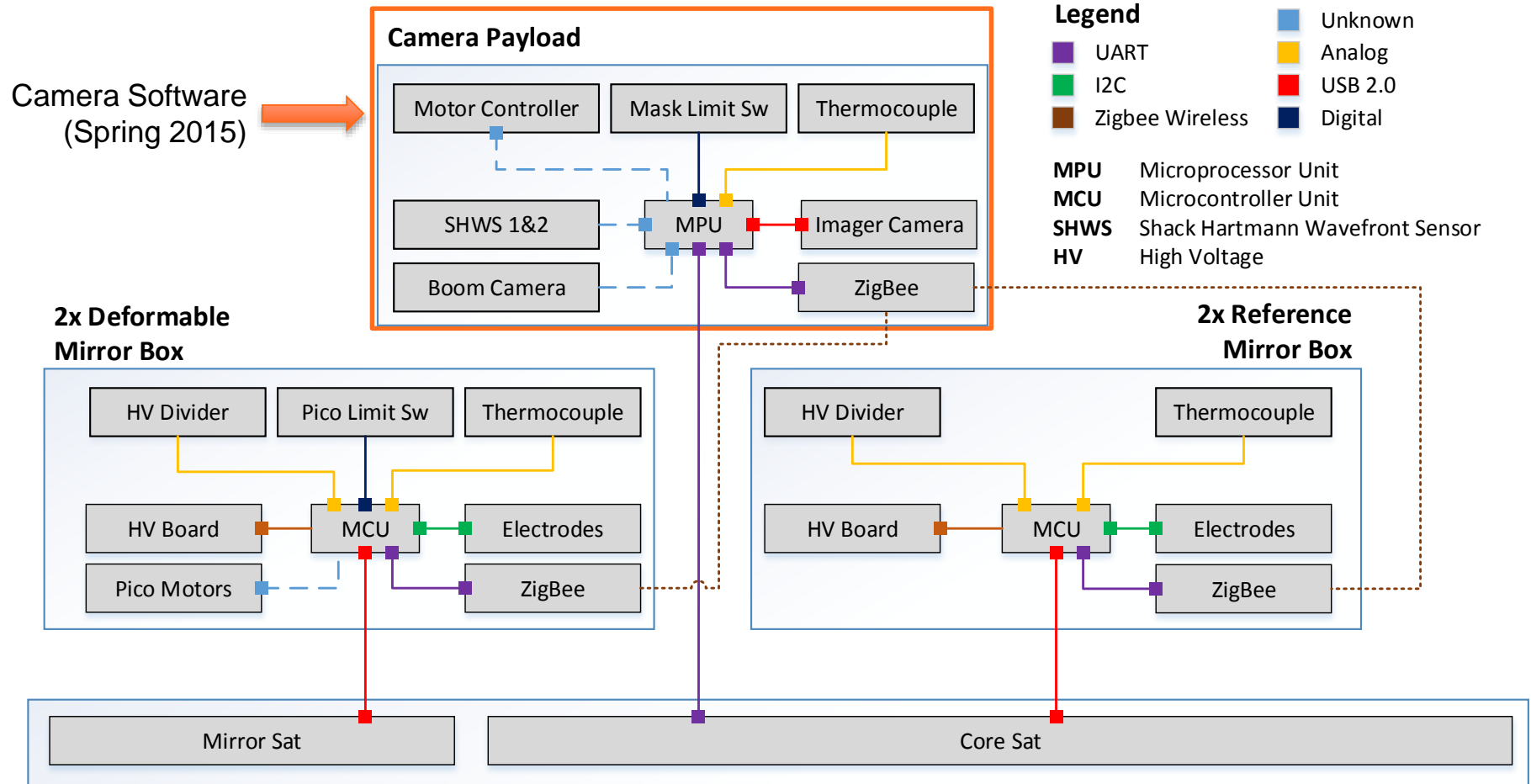
System Architecture

Mission Analysis
System Architecture
Design Implementation

- Hardware Design
 - Peripherals and Interfaces
- Operating System
 - Scheduling and Hardware Abstraction
- Software Architecture
 - Control and Logic

Payload Hardware

Mission Analysis
System Architecture
Design Implementation



Camera Computer

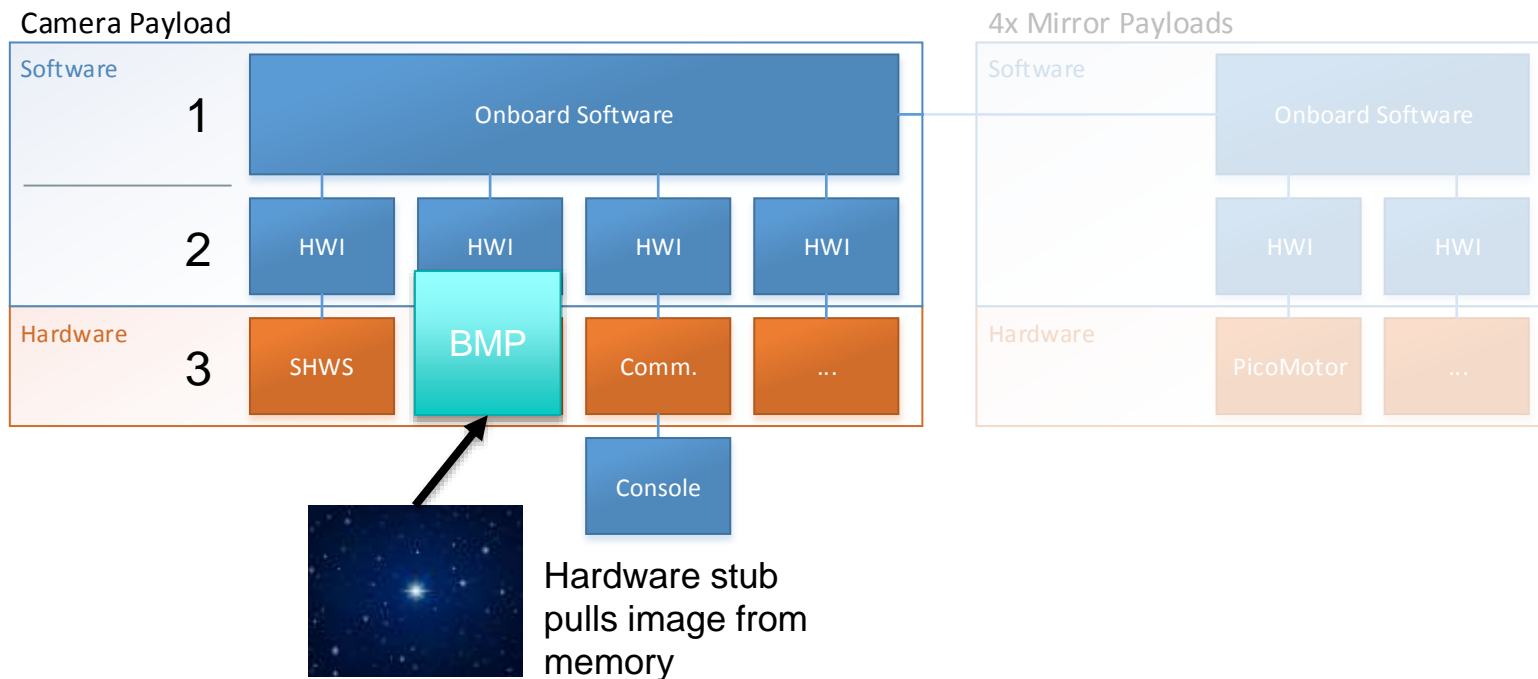
- Flight computer selected
- Linux AT91 Kernel
 - Issue: Non mainstream kernel
- Challenge: Preemptive scheduling
 - Threads must execute on time
 - Scheduling is currently not defined
 - A patch must be modified



Hardware Abstraction

Mission Analysis
System Architecture
Design Implementation

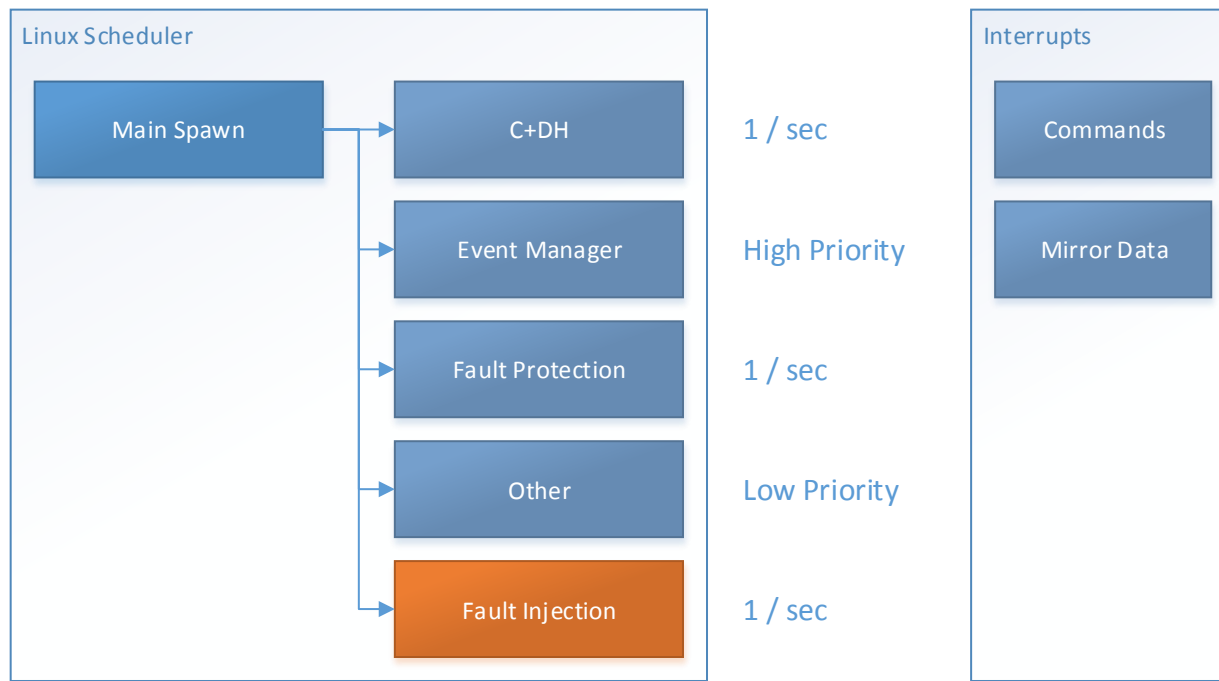
– 3 layer design



Software Architecture

Mission Analysis
System Architecture
Design Implementation

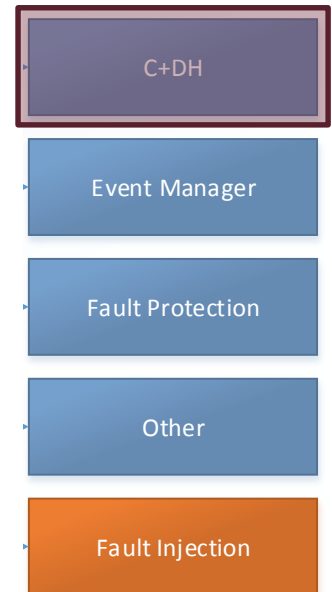
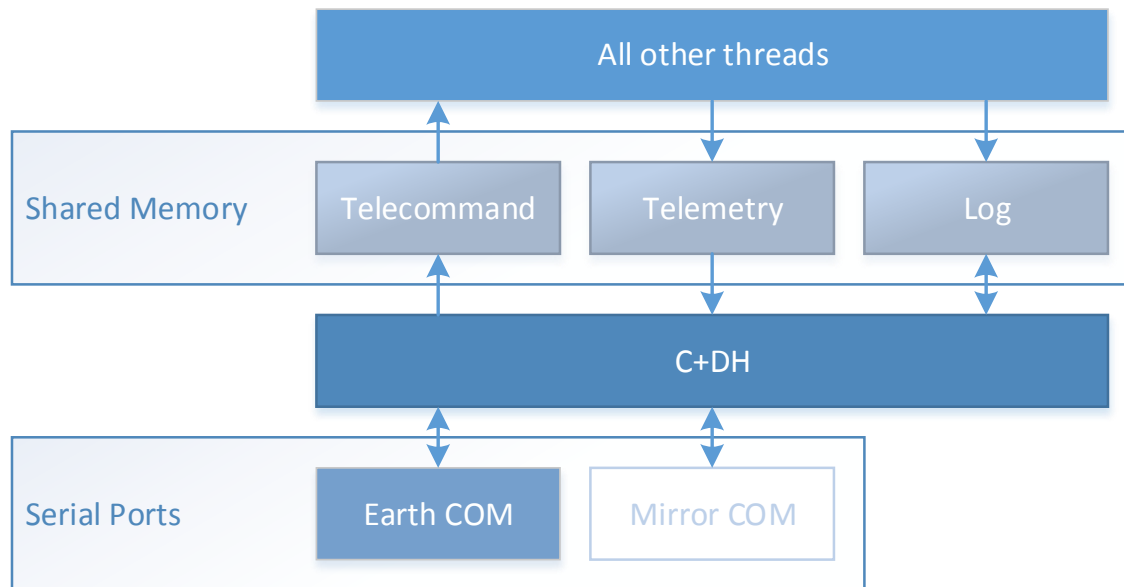
- Has been implemented in C
 - Demo on Flight Computer will follow



Command and Data Handling

Mission Analysis
System Architecture
Design Implementation

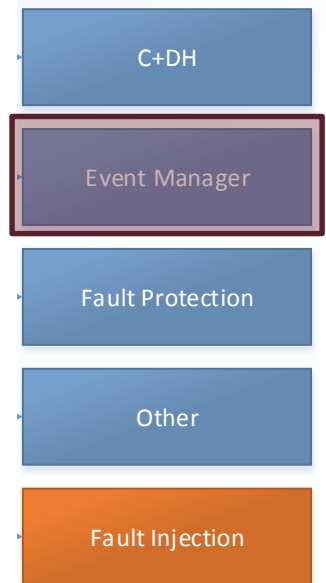
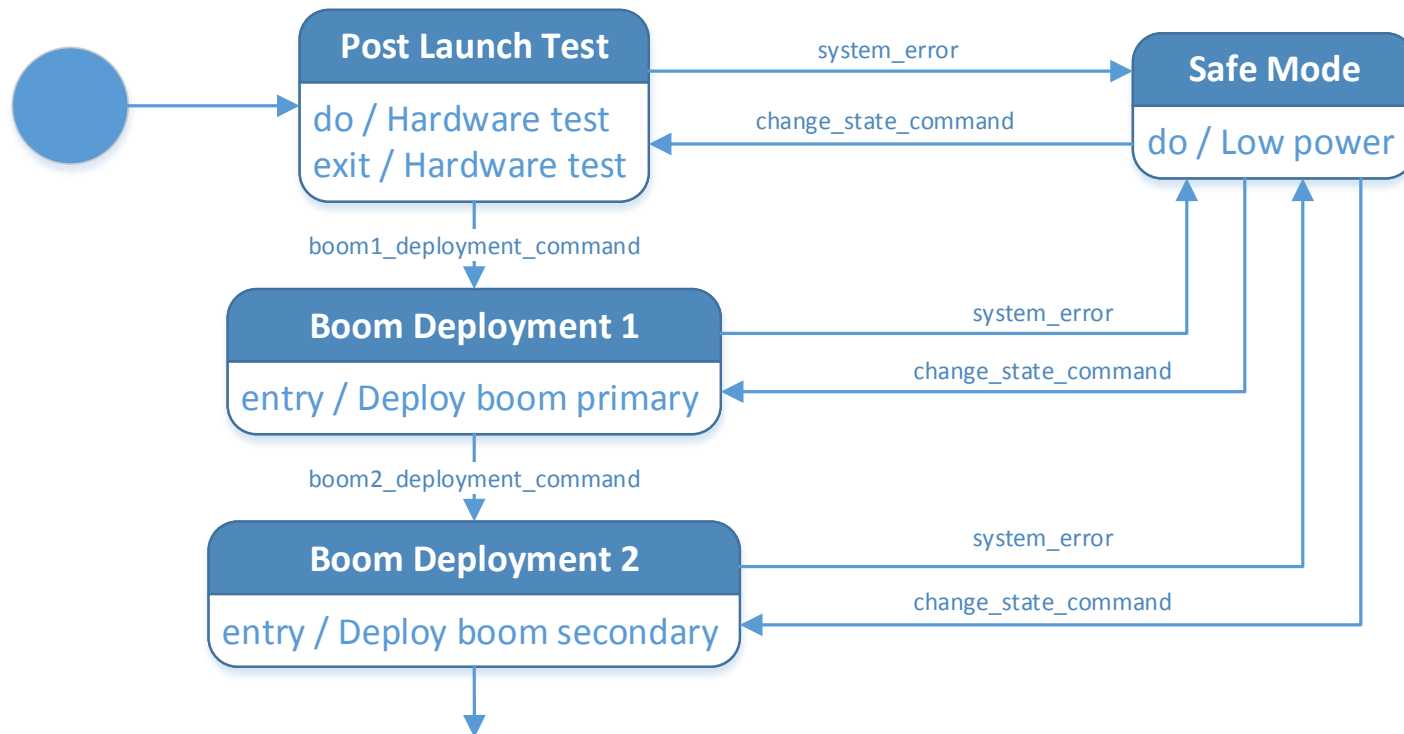
- Handles all external communication



Event Manager

Mission Analysis
System Architecture
Design Implementation

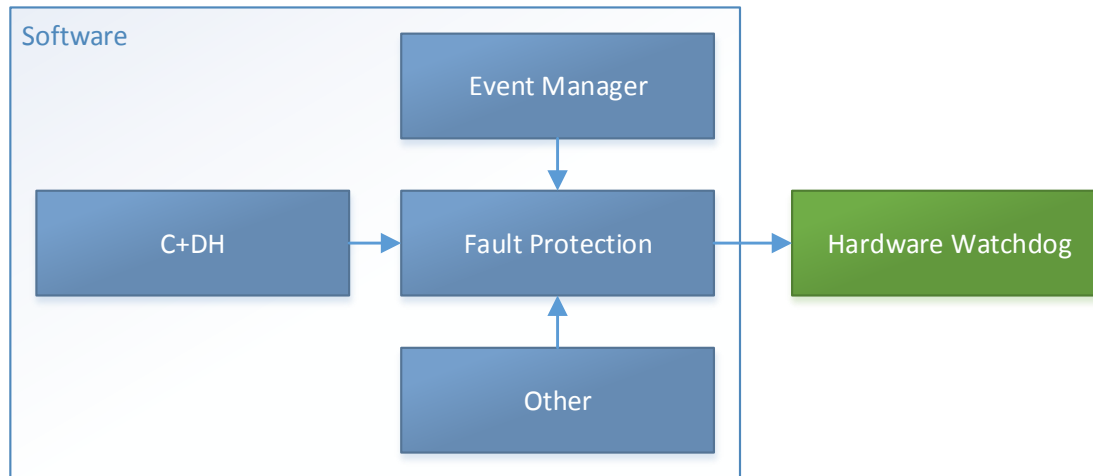
- Executes functions based on
 - Satellite state
 - Events and telecommands



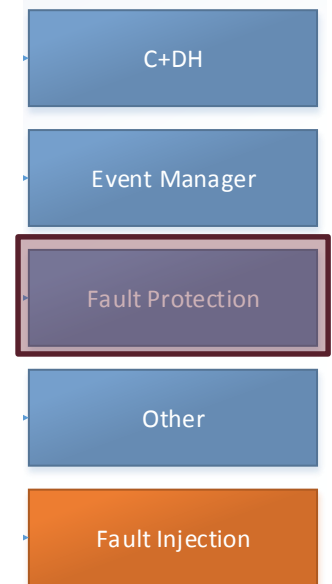
Fault Protection

Mission Analysis
System Architecture
Design Implementation

- Acts as software watchdog

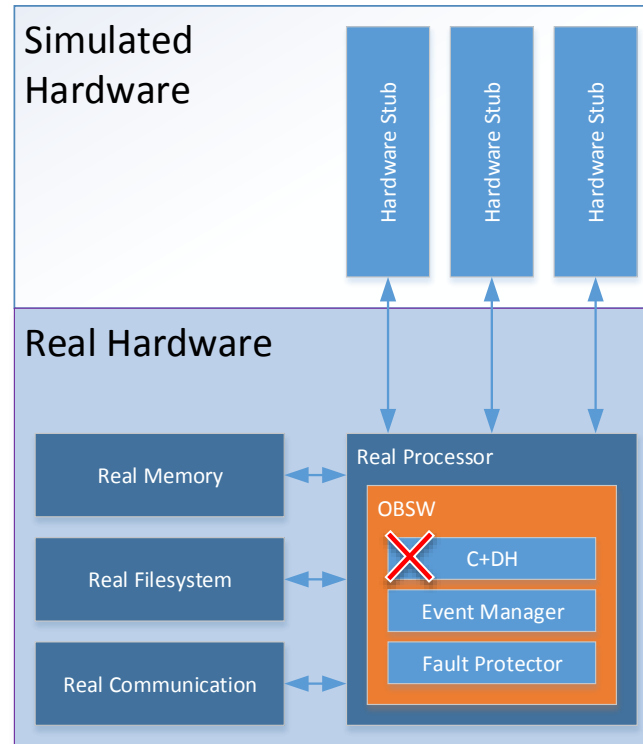
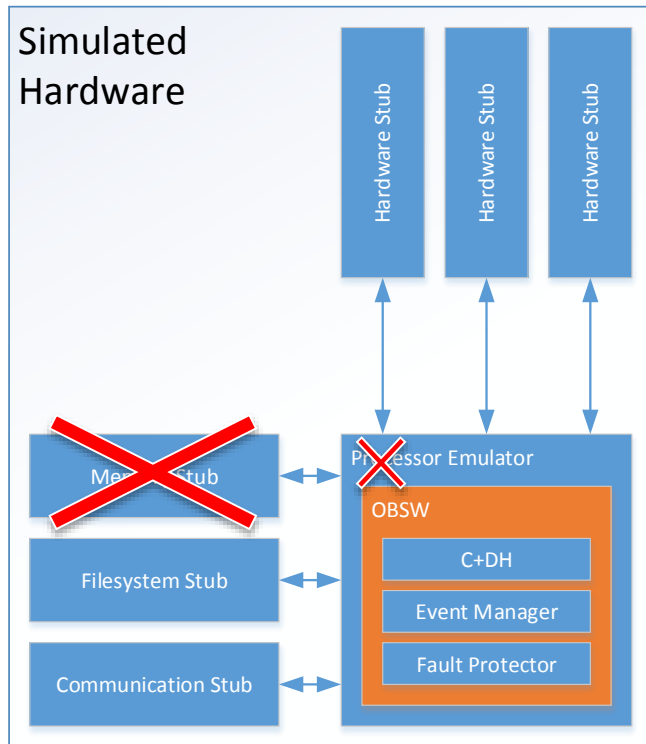


- Monitors engineering data
 - Temperature, Power, ...



Fault Injection

Mission Analysis
System Architecture
Design Implementation

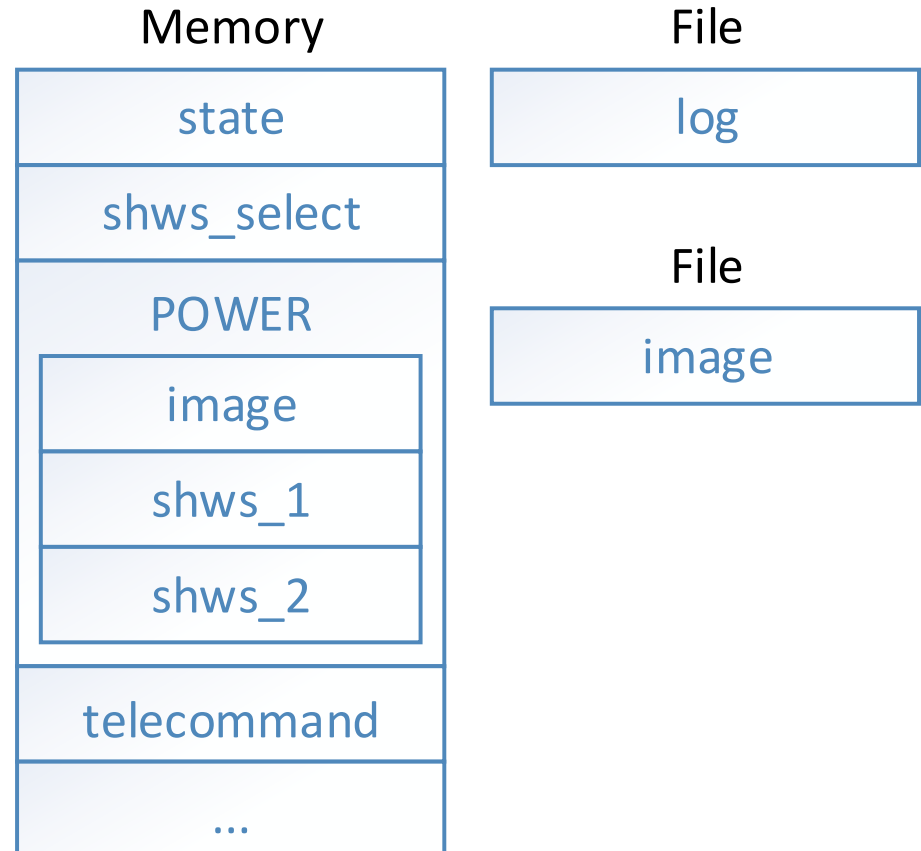


Design Implementation

- Memory
 - Run Time and Long Term
- Communication
 - Uplink and Downlink
- Demo
 - Image Acquisition
 - (Fault Injection)

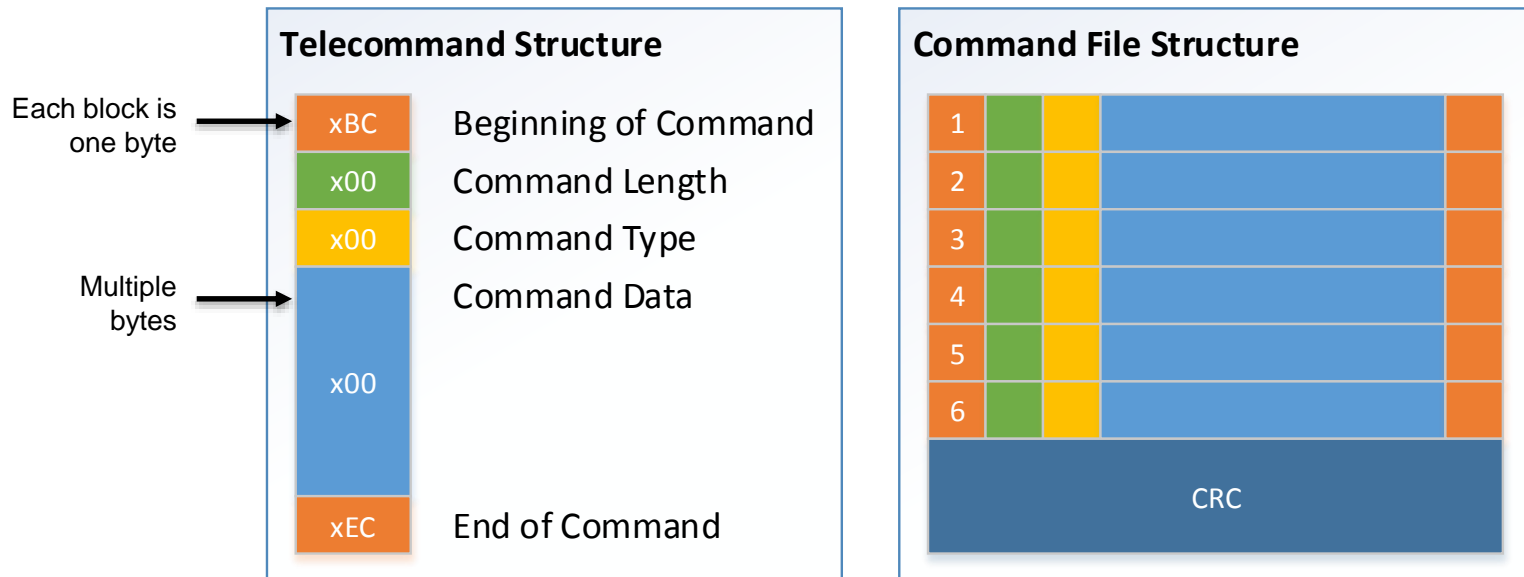
Memory

- Run Time
 - C Struct
 - Easy for memory dump
- Long Term
 - ASCII Files



Uplink Communication

- **Telecommands**
 - Commands sent as list with CRC

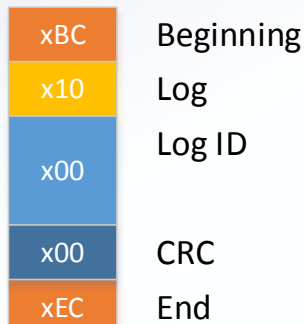


Downlink Communication

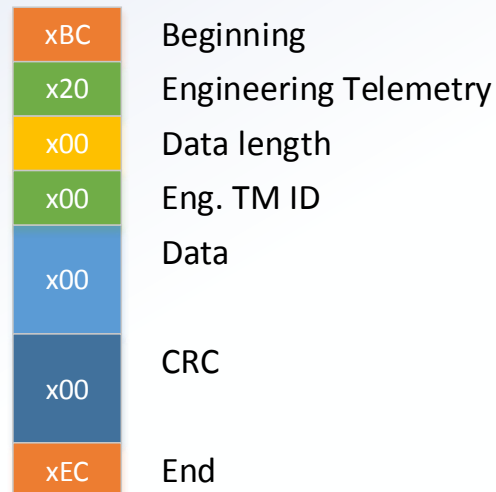
Mission Analysis
System Architecture
Design Implementation

- Event Reports
- Telemetry (Science and Engineering)

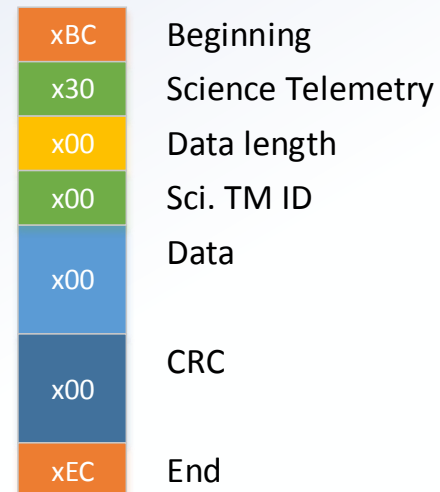
Event Report Package



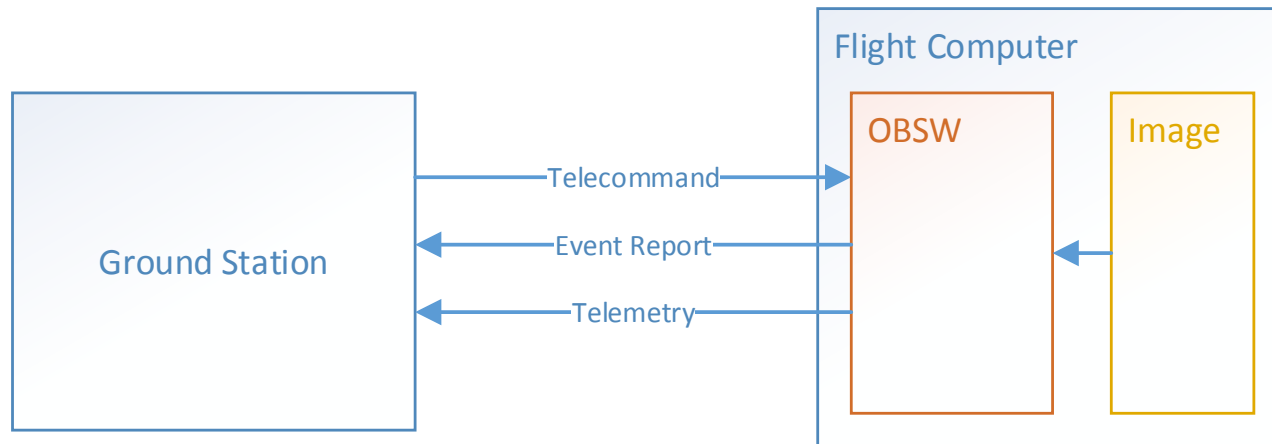
Engineering Telemetry Package



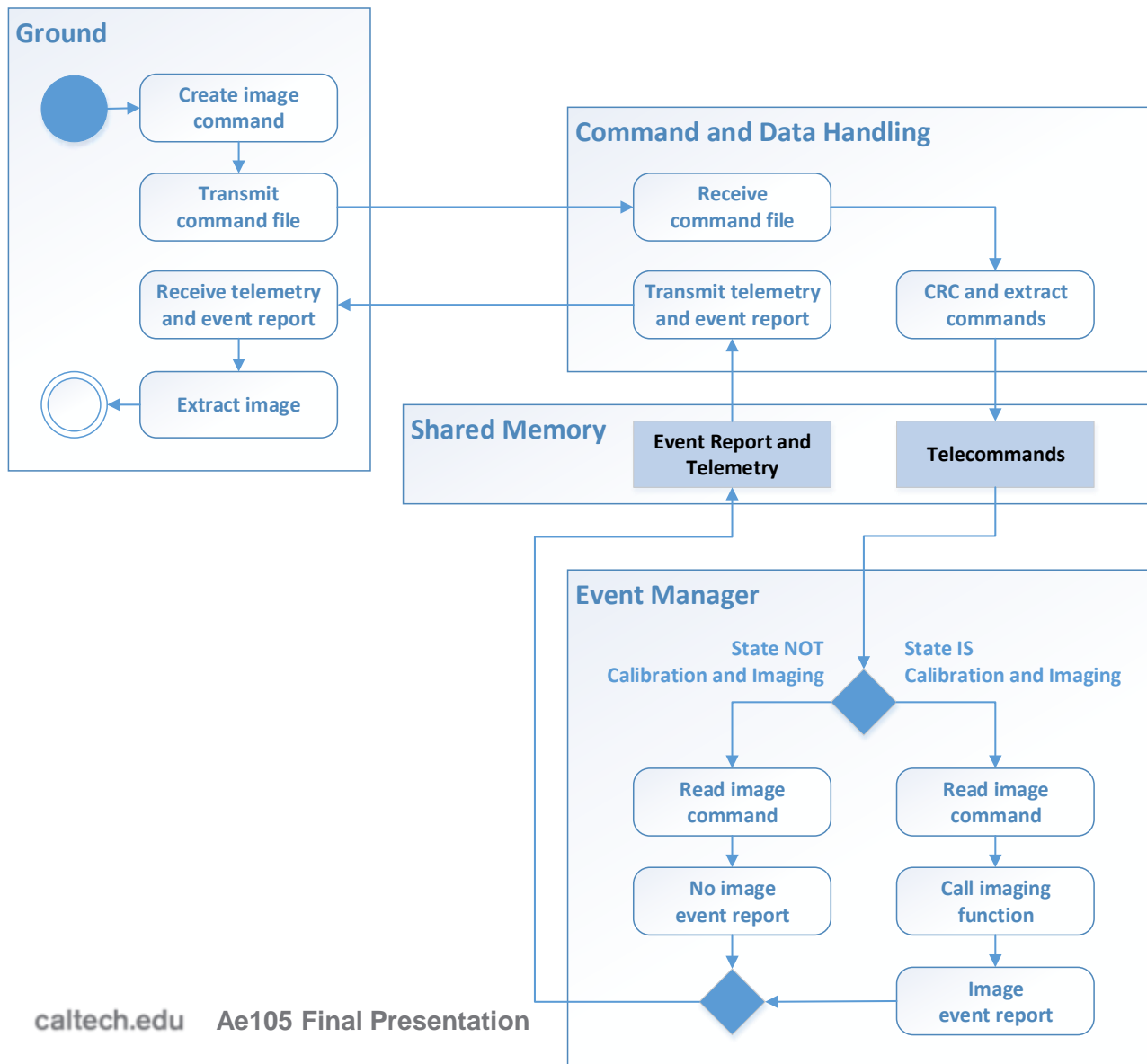
Science Telemetry Package



Demo Image Acquisition



Demo Image Acquisition



OBSW - Future Work

- Improve & extend the functions of telescope software
 - Improve the existing function modules
 - Complete interface layer with camera hardware (SHWS, image detector)
 - Add TC/TM with reference & deformable mirror boxes
- OBSW design for mirror CPU
 - Communication with telescope CPU
 - Operation and failure handling for mirror boxes
- Continue work on software requirements specification
 - Need to specify the TC/TM format with Surrey
- System integration test
 - Unit test for OBSW modules
 - Hardware in the loop test