

Model-Based Rigorous Uncertainty Quantification in Complex Systems

M. Ortiz

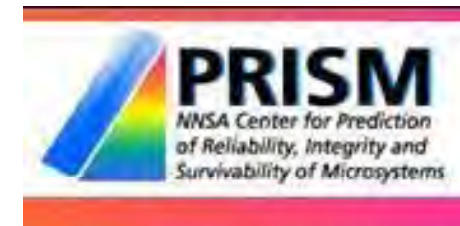
California Institute of Technology

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(CMNE 2011)

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Coimbra, Portugal, June 17, 2011

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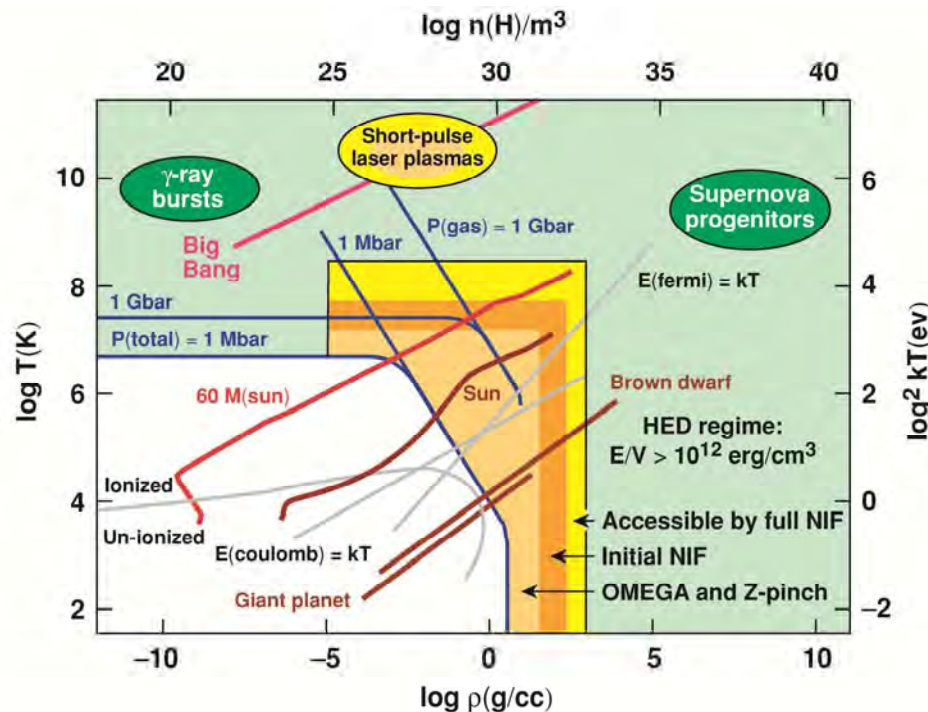


Hypervelocity impact as an example of a complex system

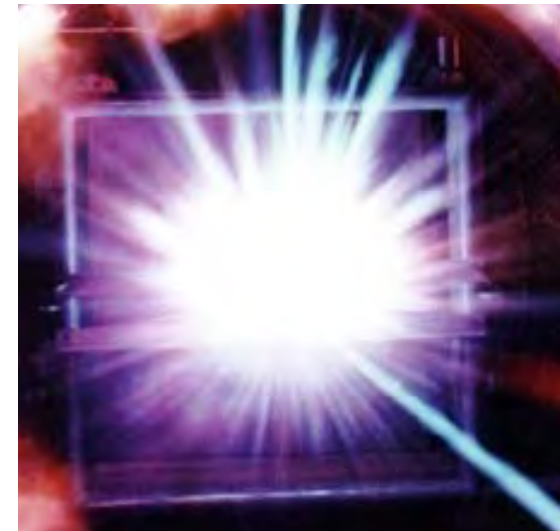
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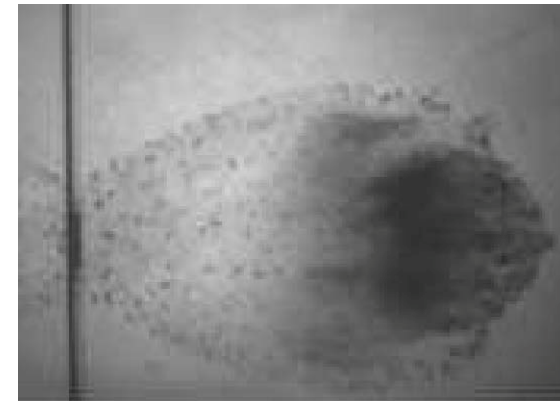
Challenge: Predict *hypervelocity impact* phenomena (10Km/s) with **quantified margins and uncertainties**



Hypervelocity impact test bumper shield
(Ernst-Mach Institut, Freiburg Germany)



NASA Ames Research Center
Energy flash from hypervelocity test
at 7.9 Km/s

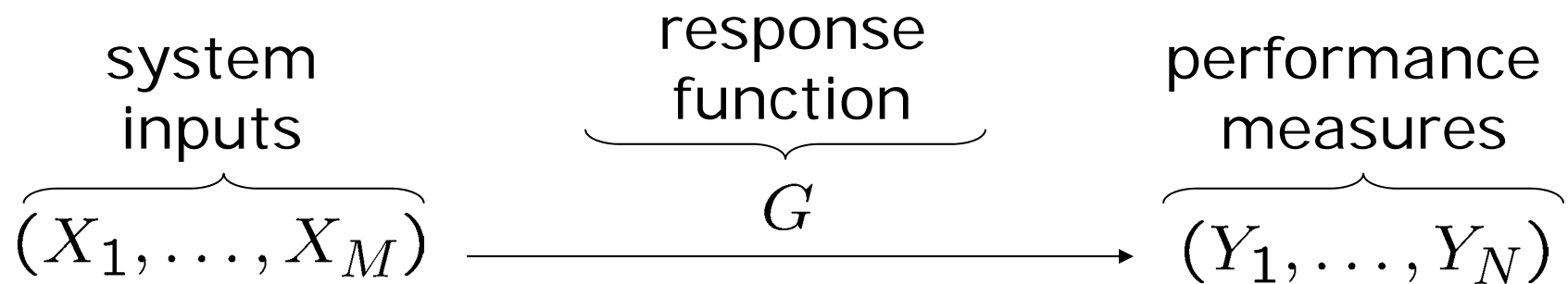


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Quantification of margins and uncertainties (QMU)

- Aim: *Predict mean performance and **uncertainty** in the behavior of complex physical/engineered systems*
- Example: Short-term weather prediction,
 - Old: Prediction that tomorrow will rain in Coimbra...
 - New: **Guarantee** same with 99% confidence...
- **QMU** is important for achieving confidence in high-consequence decisions, designs
- **Paradigm shift** in experimental science, modeling and simulation, scientific computing (**predictive science**):
 - Deterministic → Non-deterministic systems
 - Mean performance → Mean performance + uncertainties
 - Tight integration of experiments, theory and simulation
 - Robust design: Design systems to minimize uncertainty
 - Resource allocation: Eliminate main uncertainty sources

Certification view of QMU



- Random variables
- Known or unknown pdfs
- Controllable, uncontrollable, unknown-unknowns

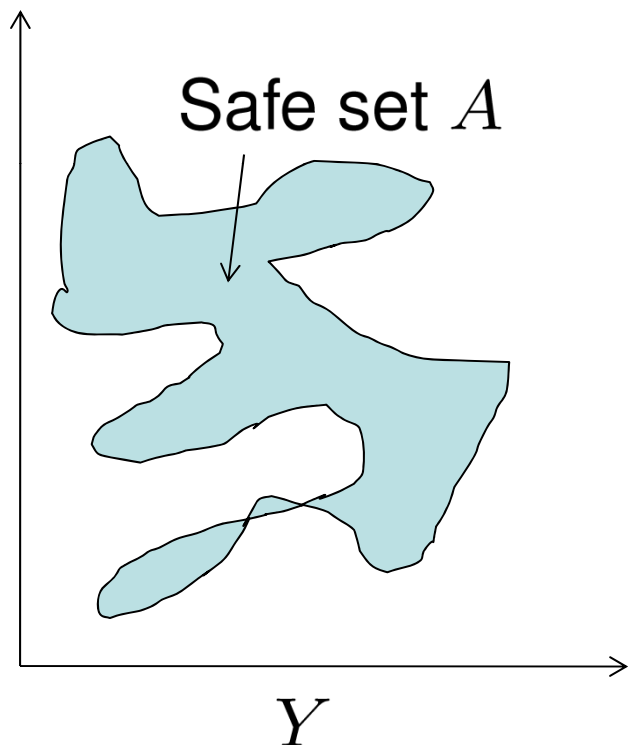


System as black box

- Observables
- Subject to performance specs
- Random due to randomness of inputs or of system

Certification view of QMU

- Certification = Rigorous guarantee that complex system will perform safely and according to specifications



- Certification criterion: Probability of failure must be below tolerance,

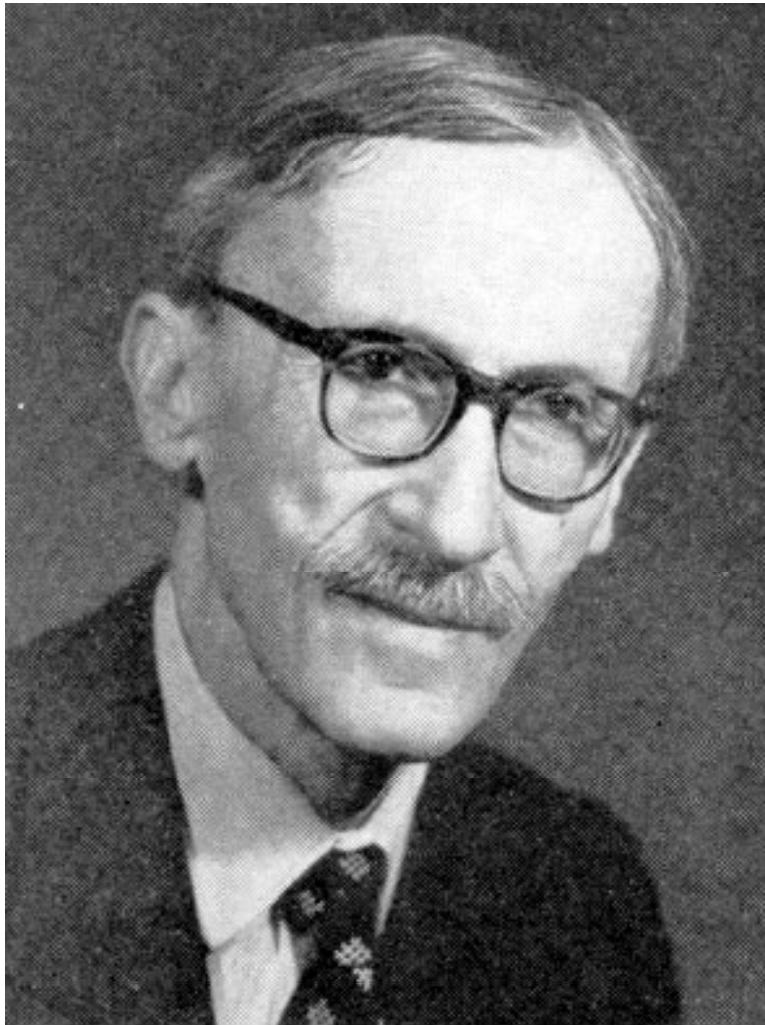
$$\mathbb{P}[Y \in A^c] \leq \epsilon$$

- Alternative (conservative) certification criterion: Rigorous *upper bound* of probability of failure must be below tolerance,

$$\mathbb{P}[Y \in A^c] \leq \text{upper bound} \leq \epsilon$$

- Challenge: Rigorous, measurable/computable upper bounds on the probability of failure of systems

Concentration of measure (CoM)



Paul Pierre Levy (1886-1971)

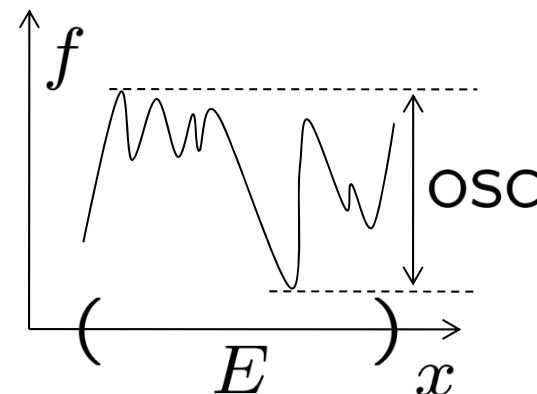
- CoM phenomenon (Levy, 1951): Functions over high-dimensional spaces with small local oscillations in each variable are almost constant
- CoM gives rise to a class of probability-of-failure inequalities that can be used for rigorous certification of complex systems



The *diameter* of a function

- Oscillation of a function of one variable:

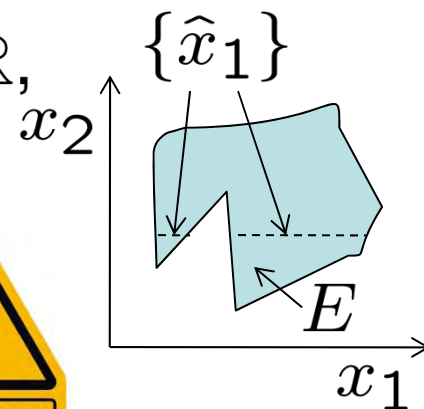
$$\begin{aligned}\text{osc}(f, E) &= \sup_{x \in E} f(x) - \inf_{x \in E} f(x) \\ &= \sup_{x, x' \in E} |f(x) - f(x')|\end{aligned}$$



- Function subdiameters: $f : E \subset \mathbb{R}^N \rightarrow \mathbb{R}$,

$$D_i(f, E) = \sup_{\hat{x}_i \in \mathbb{R}^{N-1}} \text{osc}(f, E \cap \{\hat{x}_i\}),$$

$$\hat{x}_i = \{x_1, \dots, x_{i-1}, x_{i+1}, \dots, x_N\}$$



- Function diameter:

$$D(f, E) = \sqrt{\sum_{i=1}^N D_i^2(f, E)}$$

**evaluation requires
global optimization!**



ON THE METHOD OF BOUNDED DIFFERENCES

Colin McDiarmid

(1.2) Lemma: Let X_1, \dots, X_n be independent random variables, with X_k taking values in a set A_k for each k . Suppose that the (measurable) function $f: \prod A_k \rightarrow \mathbb{R}$ satisfies

$$(1.3) \quad |f(\underline{x}) - f(\underline{x}')| \leq c_k$$

whenever the vectors \underline{x} and \underline{x}' differ only in the k th co-ordinate. Let Y be the random variable $f[X_1, \dots, X_n]$. Then for any $t > 0$,

$$P(|Y - E(Y)| \geq t) \leq 2\exp\left[-2t^2 / \sum c_k^2\right].$$

McDiarmid, C. (1989) "On the method of bounded differences". In J. Simmons (ed.), *Surveys in Combinatorics: London Math. Soc. Lecture Note Series 141*. Cambridge University Press.

McDiarmid's inequality

Theorem [McDiarmid] *Suppose that:*

- i) $\{x_1, \dots, x_N\}$ are independent random variables,*
- ii) $f : E \subset \mathbb{R}^N \rightarrow \mathbb{R}$ is integrable.*

Then, for every $r \geq 0$

$$\mathbb{P}[|f - \mathbb{E}[f]| \geq r] \leq \exp\left(-2 \frac{r^2}{D^2(f, E)}\right),$$

where $D(f, E)$ is the diameter of f over E .

- Bound does not require distribution of inputs
- Bound depends on two numbers only:
Function **mean** and function **diameter!**



Corollary *A conservative certification criterion is:*

$$\underbrace{\mathbb{P}[G \leq a]}_{\text{Probability of failure}} \leq \underbrace{\exp \left(-2 \frac{(\mathbb{E}[G] - a)_+^2}{D_G^2} \right)}_{\text{Upper bound}} \underbrace{\leq \epsilon}_{\text{Failure tolerance}},$$

Probability of failure Upper bound Failure tolerance

- Equivalent statement (confidence factor CF):

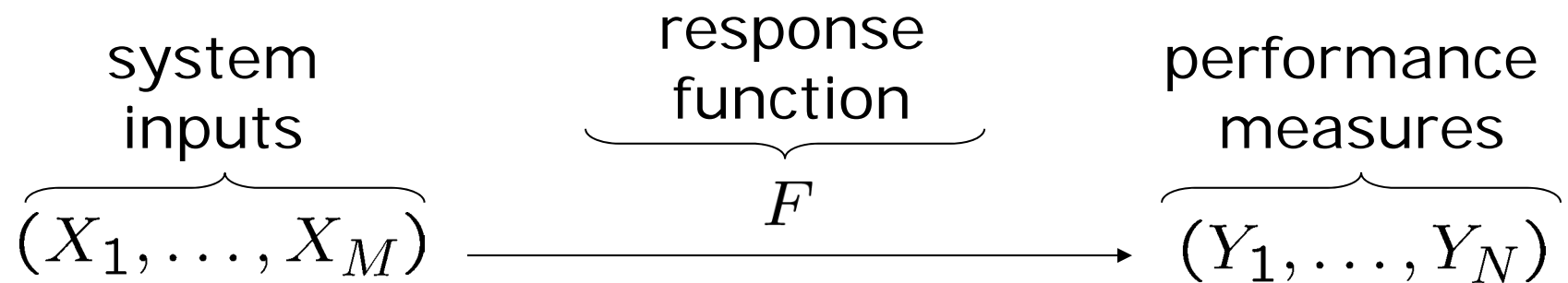
$$\text{CF} \equiv \frac{M}{U} \equiv \frac{(\mathbb{E}[G] - a)_+}{D_G} \geq \sqrt{\log \sqrt{\frac{1}{\epsilon}}} \Rightarrow \text{certification!}$$

- Rigorous definition of margin (M)
- Rigorous definition of uncertainty (U)

McDiarmid's inequality and QMU

- CoM Uncertainty Quantification (UQ) 'does the job':
 - Rigorous upper bounds on PoFs for complex systems
 - Rigorous definitions of 'uncertainty' and 'margin'
 - Does not require knowledge of input parameters pdfs
 - Reduces UQ to determination of:
 - Mean performance $E[G]$
 - System diameter D_G
- But determination of response diameter is a global optimization problem over parameter space: Solution requires exceedingly many function evaluations
- Strictly experimental implementation is often impractical
- Alternative: ***Model-Based Uncertainty Quantification!***

Model-Based QMU



- Random variables
- Known or unknown pdfs
- Controllable, uncontrollable, unknown-unknowns



- Observables
- Subject to performance specs
- Random due to randomness of inputs or of system

System model

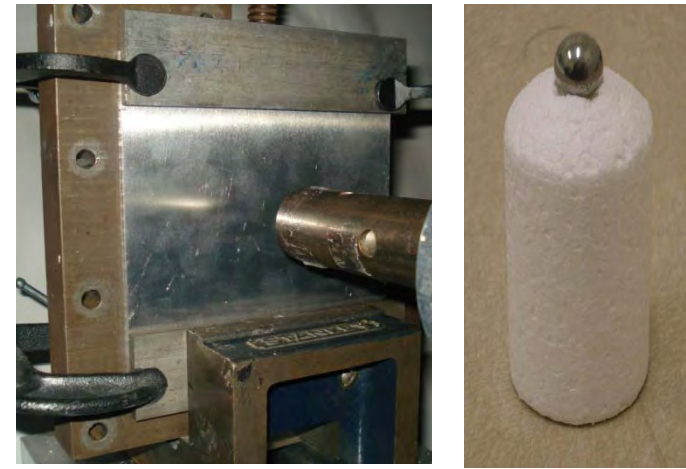
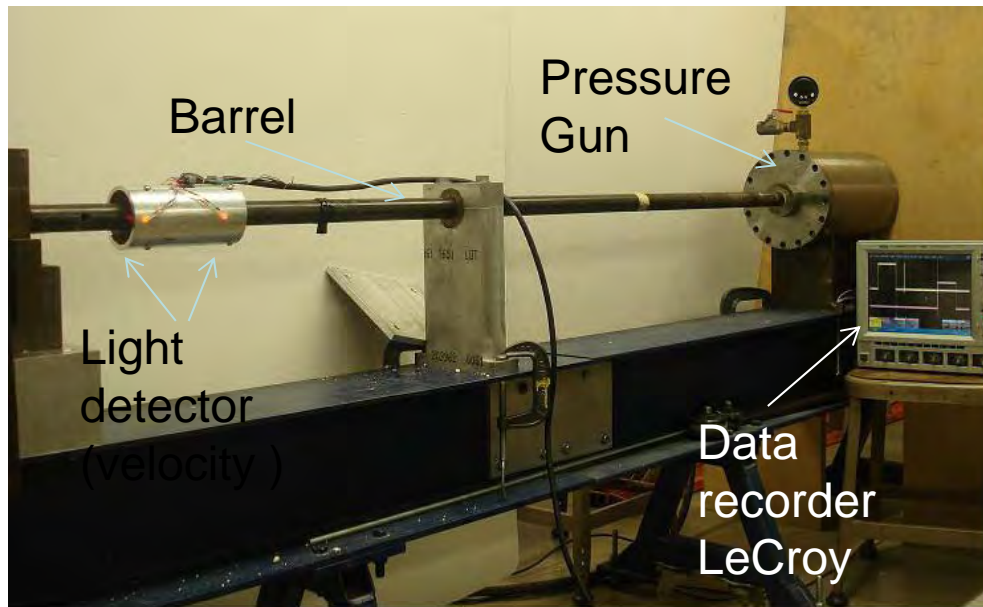
Model-based QMU – Perfect model

System model



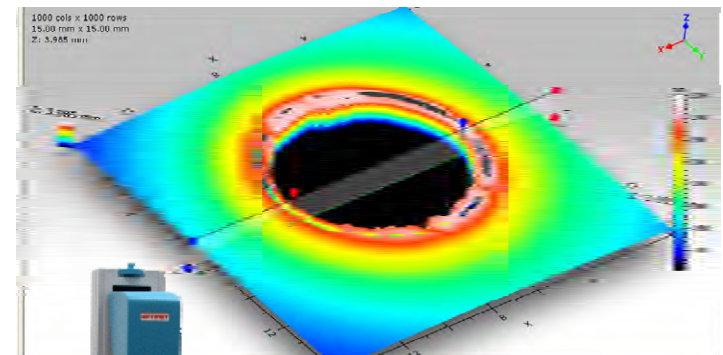
- Assume ***deterministic system*** (no scatter)
- Assume ***model is perfect*** ($F=G$)
- Assume that *mean performance* and *system diameter* can be ***computed exactly***
- Then UQ can be carried out entirely in cyber-space, ***no experiments are required!***

Case Study – Steel/Al ballistics



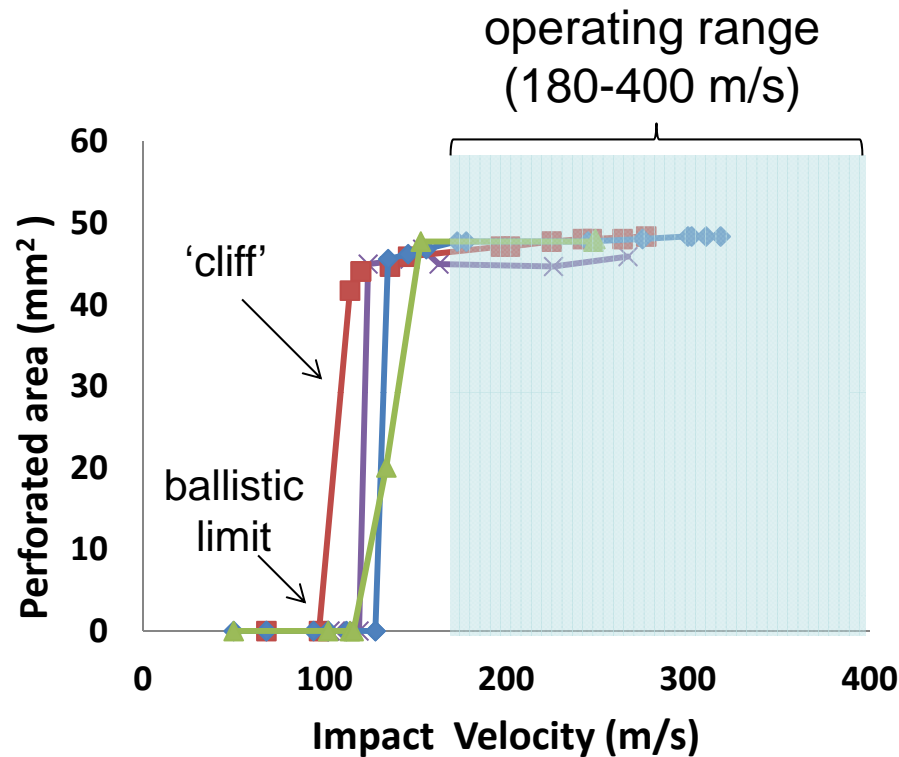
Target and projectile

- Target/projectile materials:
 - Target: Al 6061-T6 plates (6"x 6")
 - Projectile: S2 Tool steel balls (5/16")
- Model input parameters (X):
 - Plate thickness (0.032"-0.063")
 - Impact velocity (200-400 m/s)

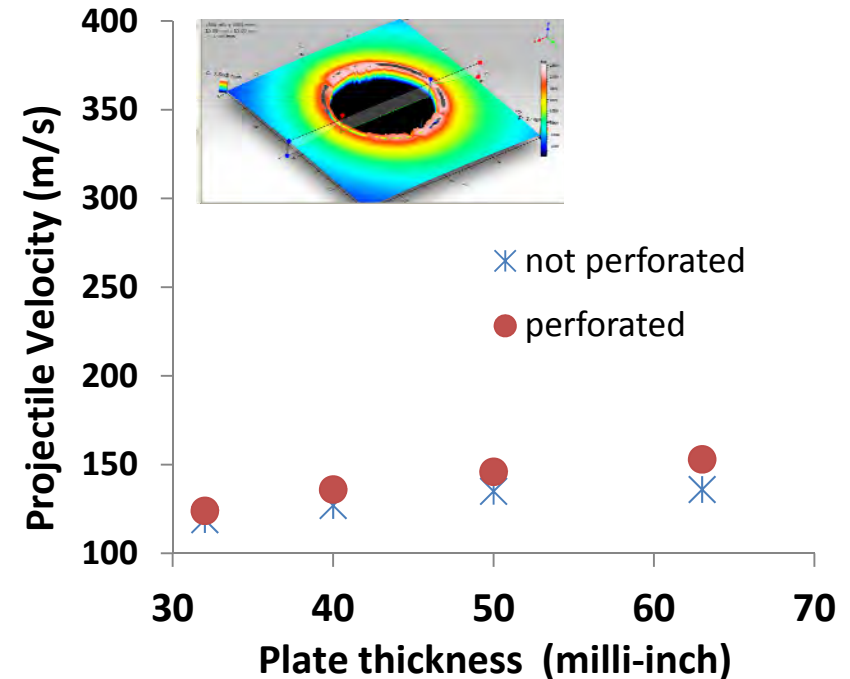


Optimet
MiniConoscan
3000

Case Study – Steel/Al ballistics



Perforation area vs. impact velocity
(note small data scatter!)



Perforation/non-perforation
boundary

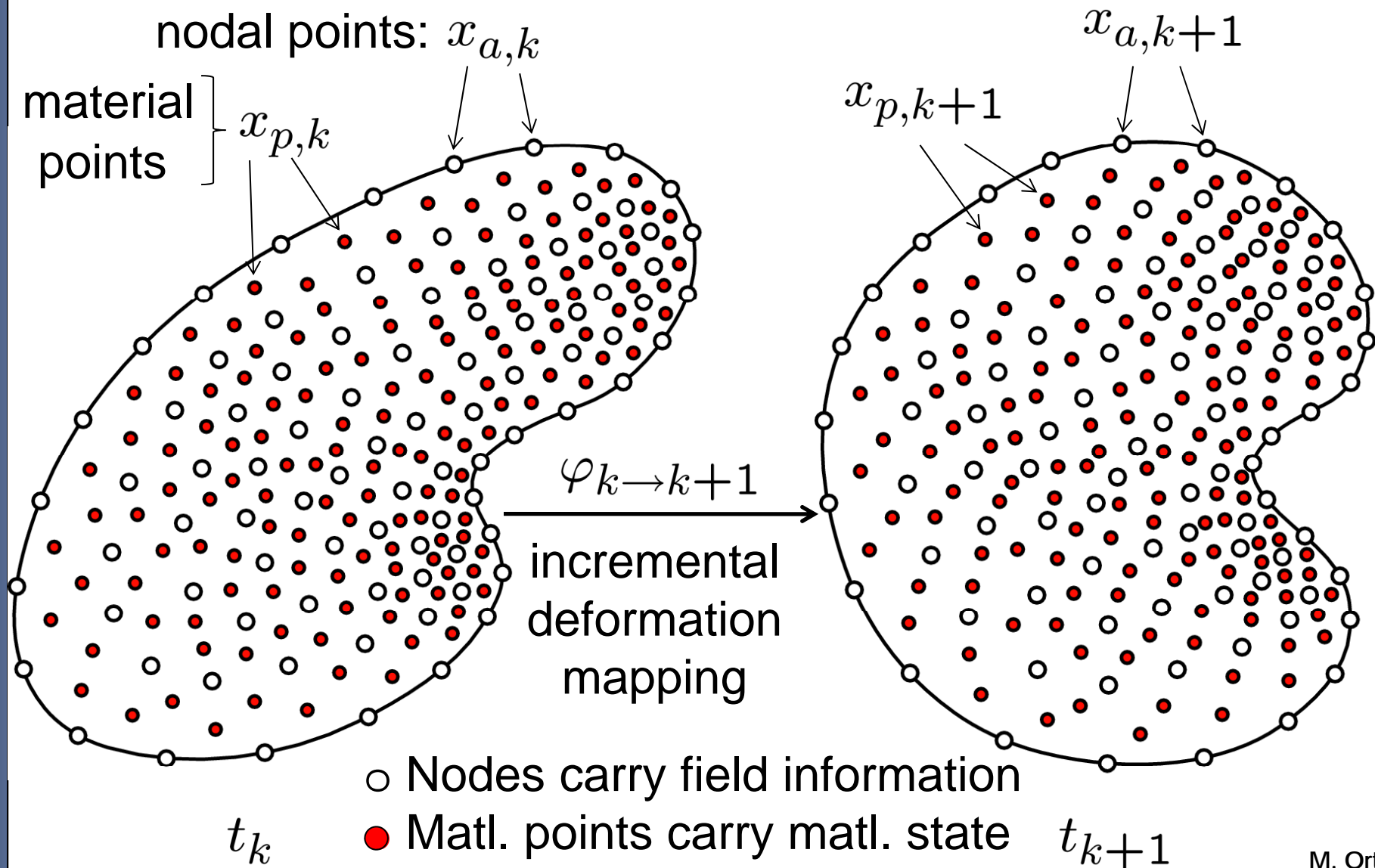
- System output (Y): ***Perforation area!***
- Certification criterion: $Y > 0$ (lethality)

Optimal-Transportation Meshfree (OTM) model of terminal ballistics

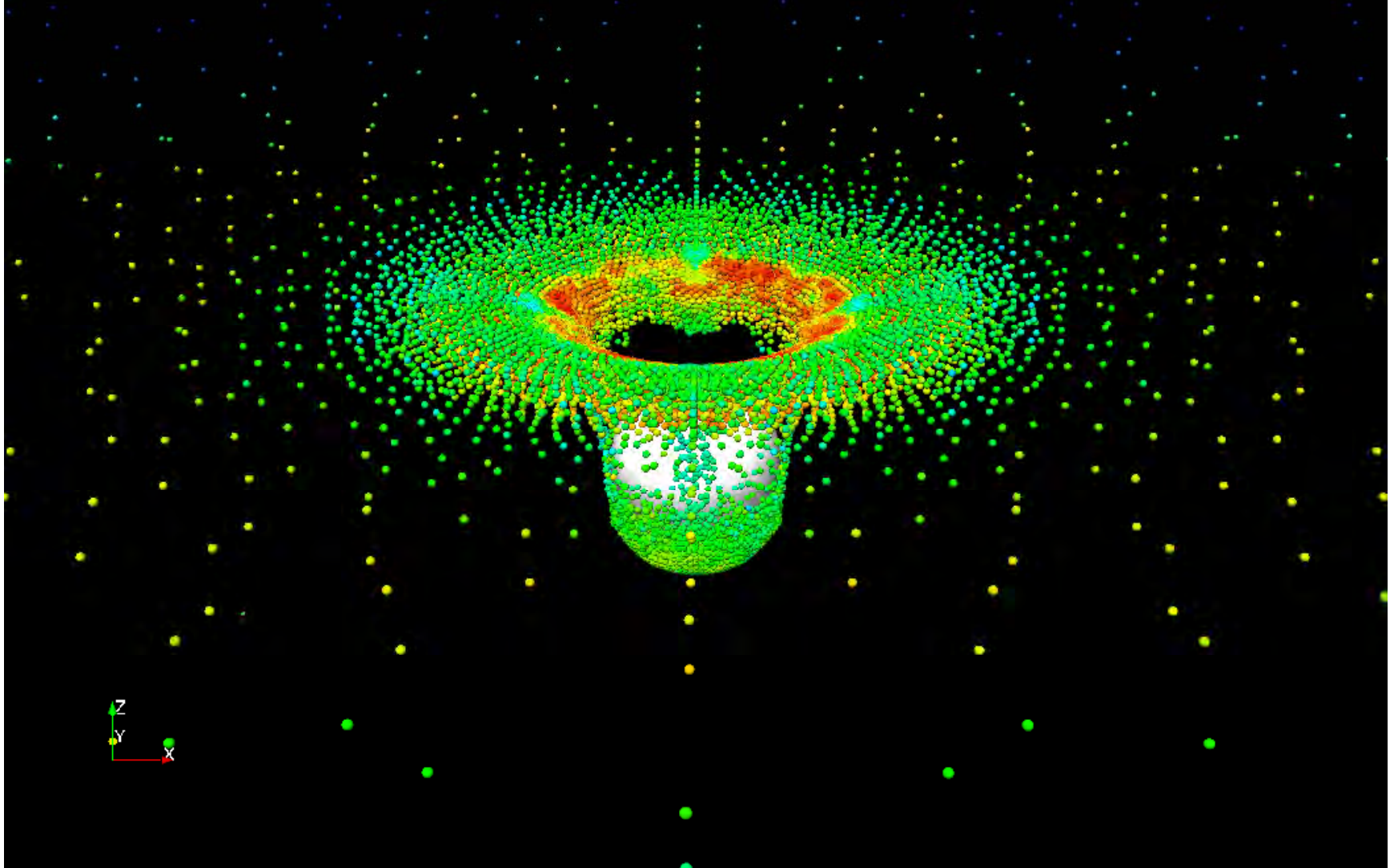
- Optimal transportation theory is a useful tool for generating geometrically-exact discrete Lagrangians for flow problems
- Inertial part of discrete Lagrangian measures distance between consecutive mass densities (in sense of Wasserstein)
- Discrete Hamilton principle of stationary action: Variational time integration scheme:
 - Symplectic, time reversible, exact conservation
 - Variational convergence (Γ -convergence, B. Schmidt)
- Extension to inelasticity: Variational constitutive updates

Li, B., Habbal, F. and Ortiz, M., *IJNME*, **83** (2010) 1541-1579

OTM – Spatial discretization



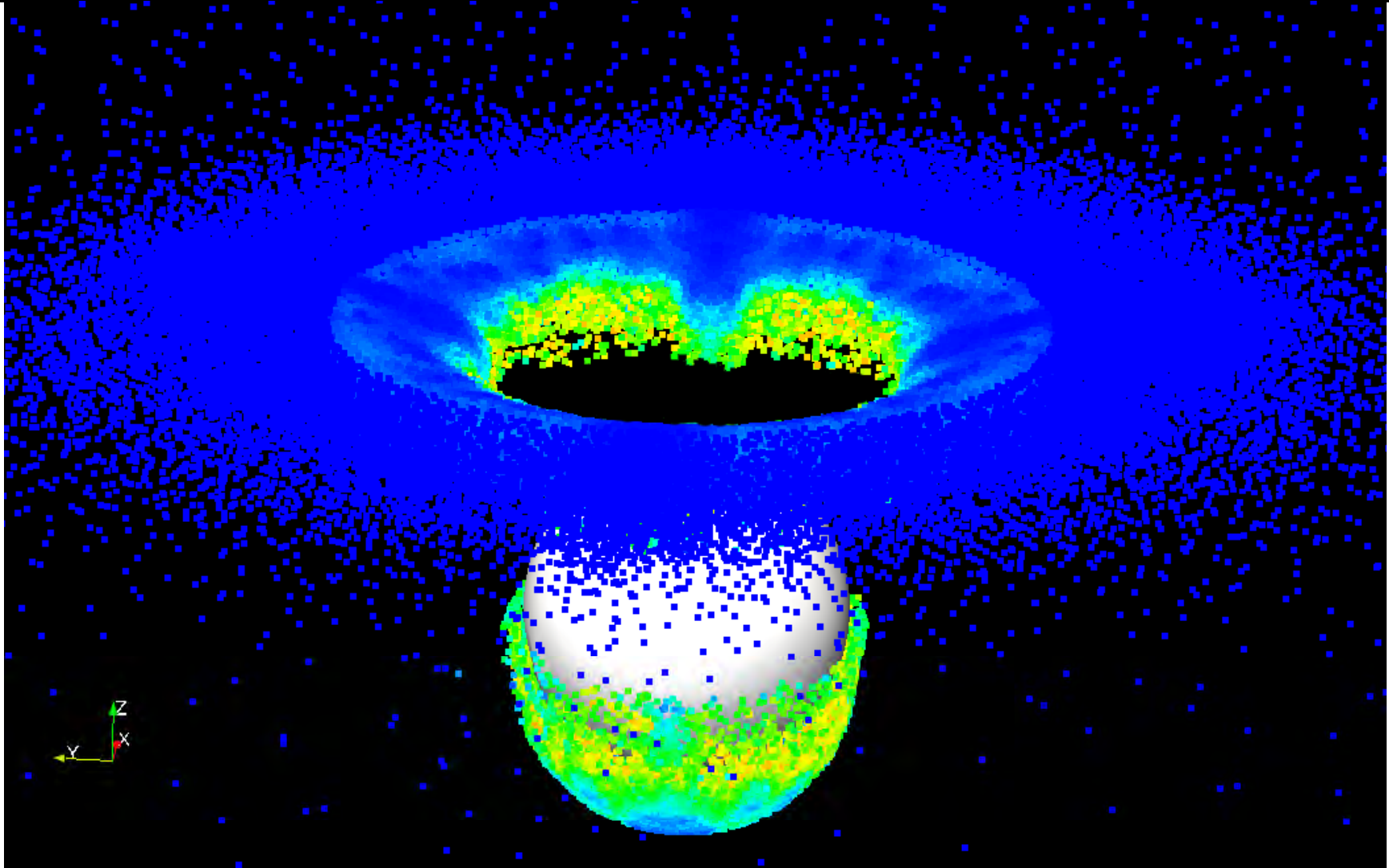
OTM — Nodal point set



Steel projectile/aluminum plate: Nodal set

OTM — Material point set

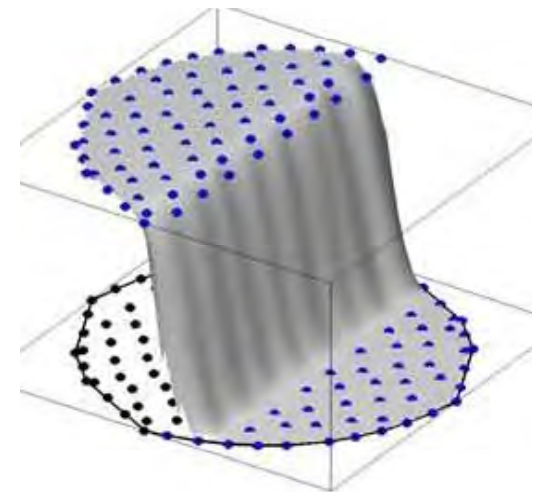
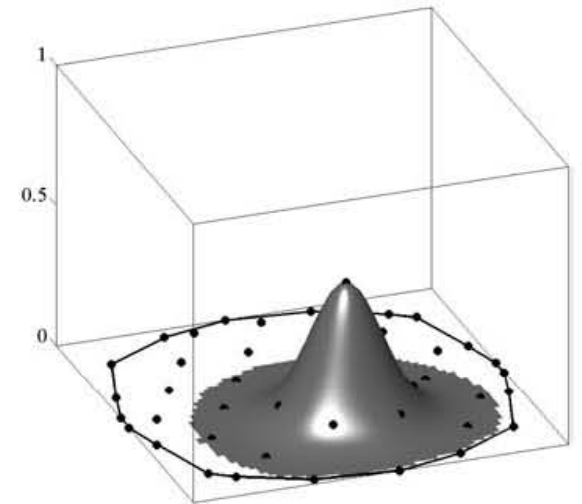
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Steel projectile/aluminum plate: Material point set

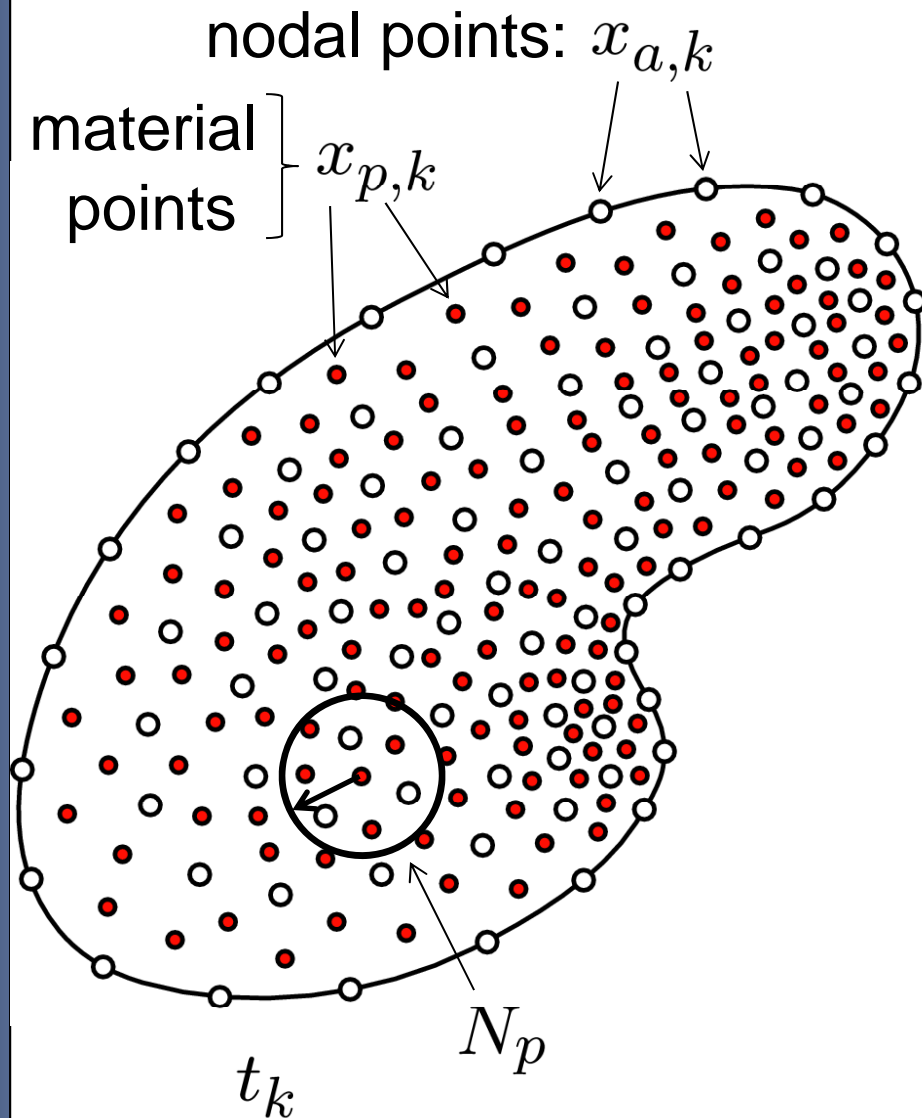
OTM — Max-ent interpolation

- Max-ent interpolation is smooth, meshfree
- Finite-element interpolation is recovered as a limit
- Rapid decay, short range
- Monotonicity, maximum principle
- Good mass lumping properties
- Kronecker-delta property at the boundary:
 - Displacement boundary conditions
 - Compatibility with finite elements



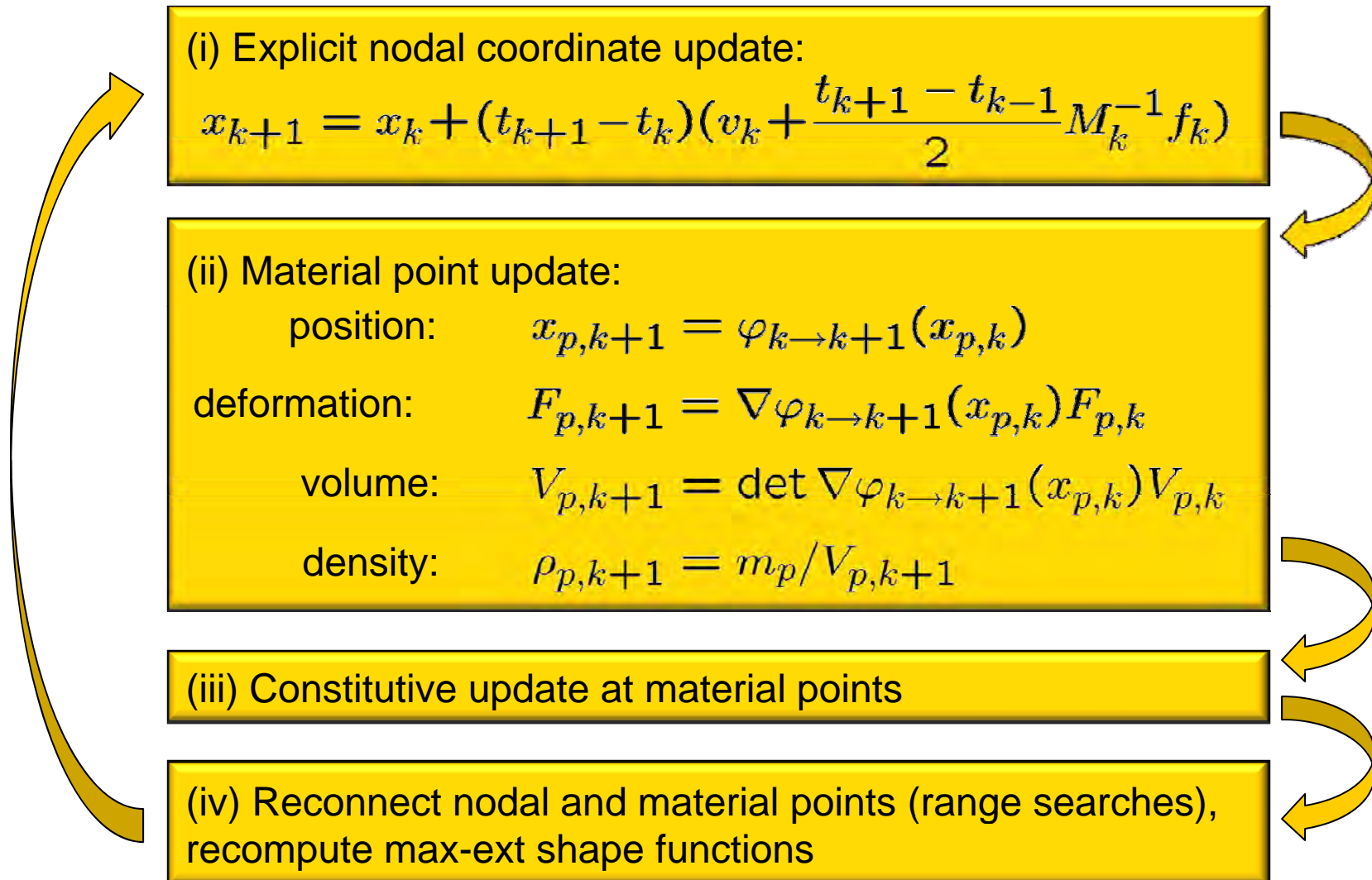
Arroyo, M. and Ortiz, M., *IJNME*, **65** (2006) 2167-2202

OTM – Spatial discretization

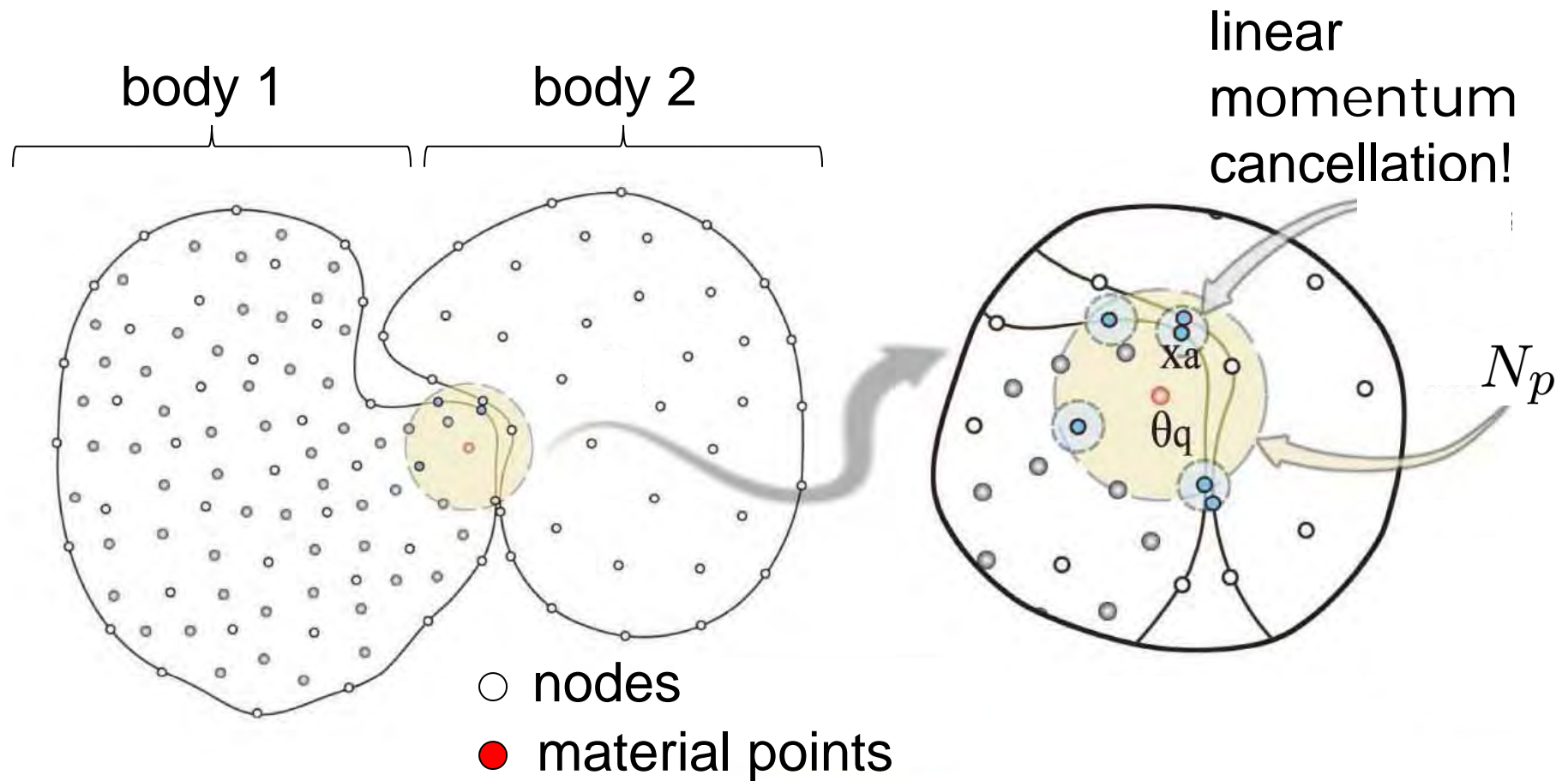


- Max-ent interpolation at material point p determined by nodes in its local environment N_p
- Local environments determined 'on-the-fly' by range searches
- Local environments evolve continuously during flow (dynamic reconnection)
- Dynamic reconnection requires no remapping of history variables!

OTM — Flow chart

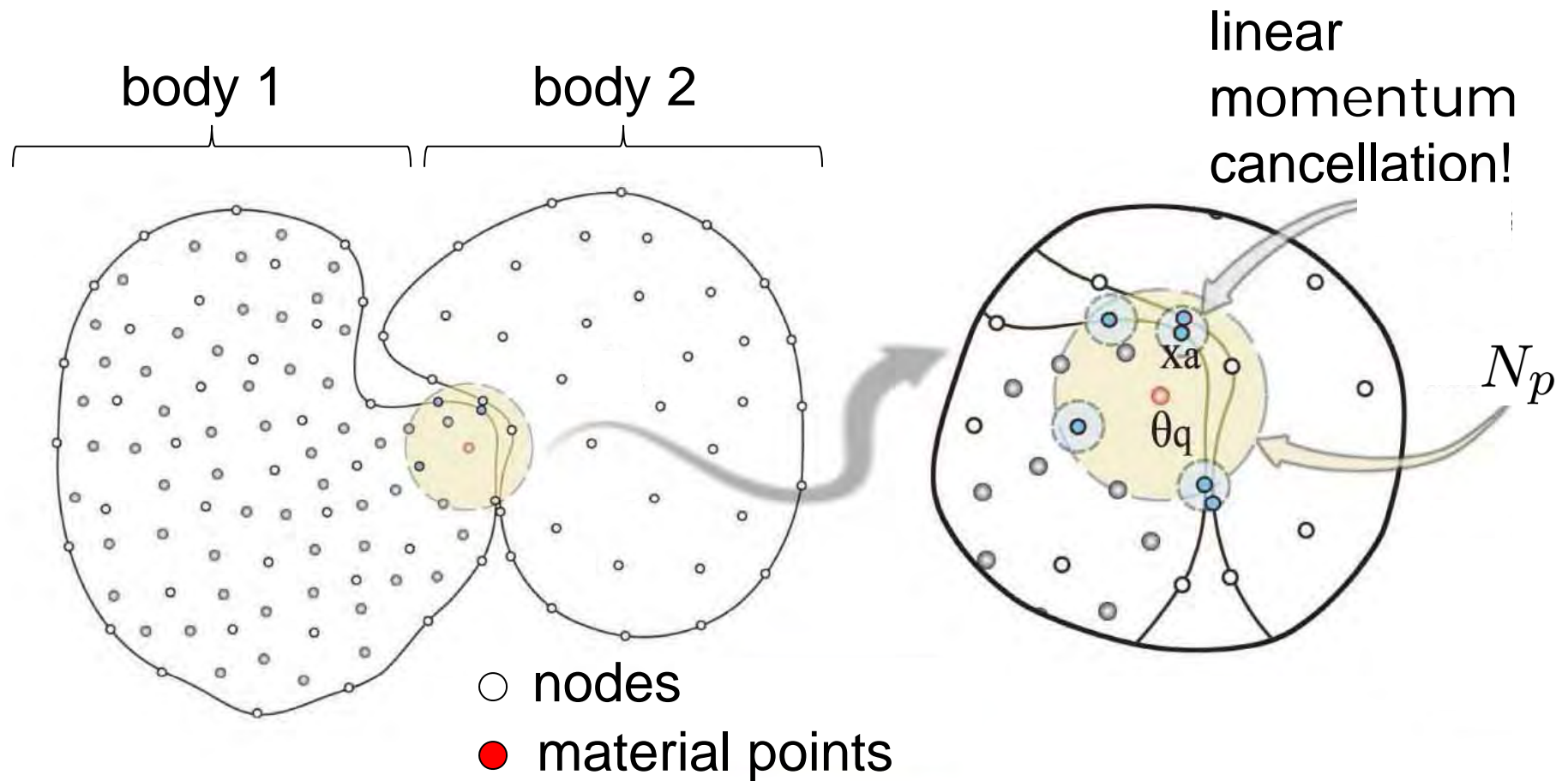


OTM – Seizing contact



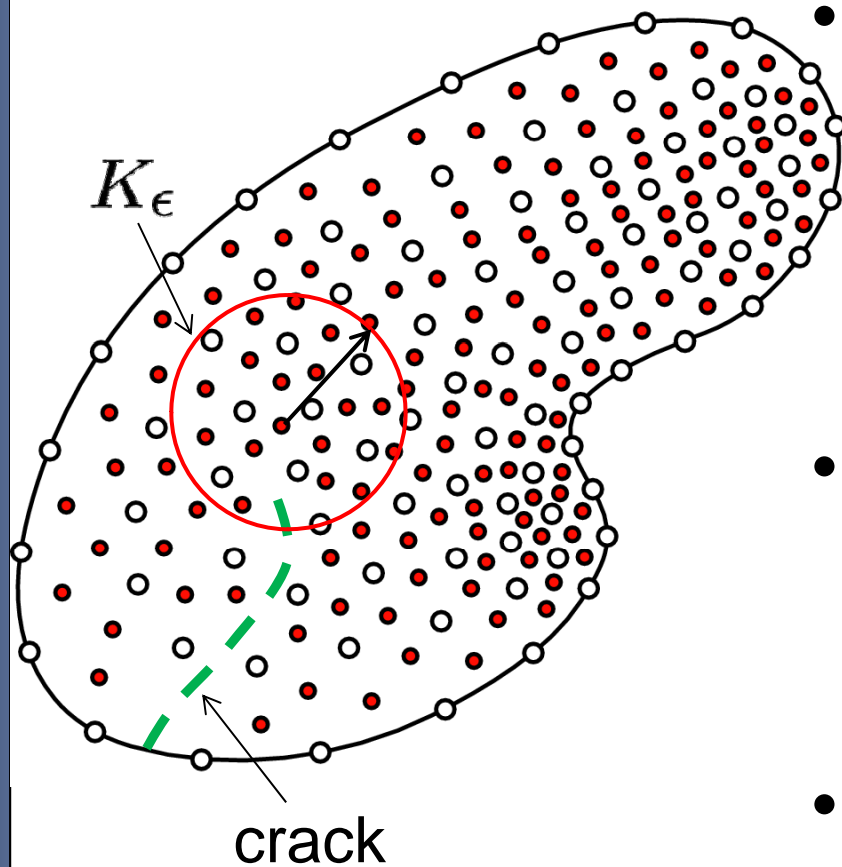
Seizing contact (infinite friction)
is obtained for free in OTM!
(as in other material point methods)

OTM – Seizing contact



Seizing contact (infinite friction)
is obtained for free in OTM!
(as in other material point methods)

OTM - Fracture & fragmentation



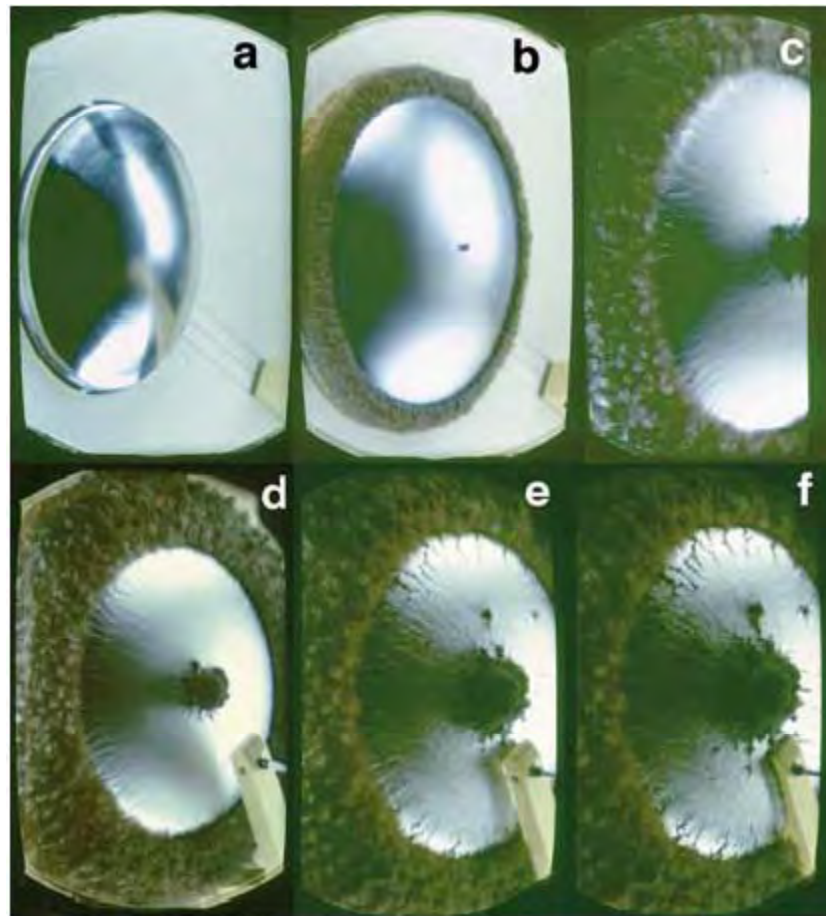
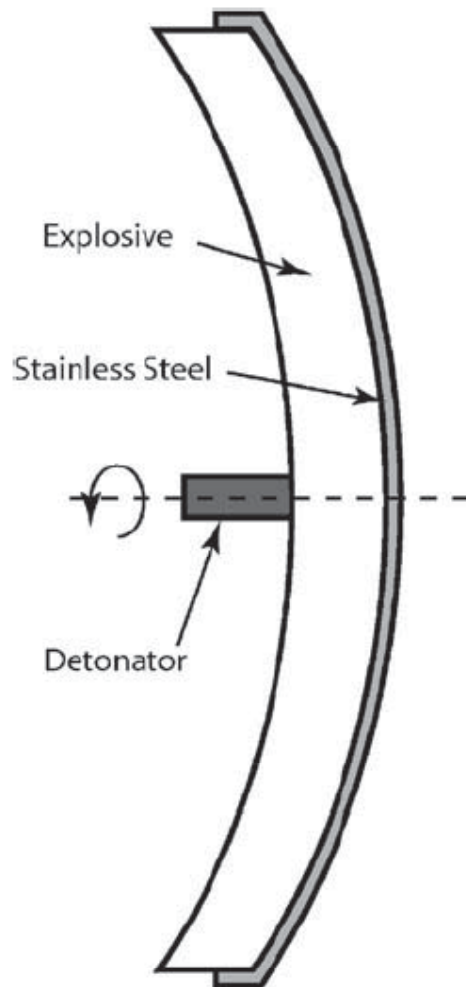
- Proof of convergence of variational element erosion to Griffith fracture:
 - Schmidt, B., Fraternali, F. and Ortiz, M., SIAM J. Multiscale Model. Simul., 7(3) (2009) 1237-1366.
- OTM implementation: Variational erosion of material points (by ϵ -neighborhood construction),

$$G_\epsilon \geq G_c$$

- Alternatively: Material point failure + comminution:
 - Pandolfi, A., Conti, S. and Ortiz, M., JMPS, **54** (2006) 1972-2003

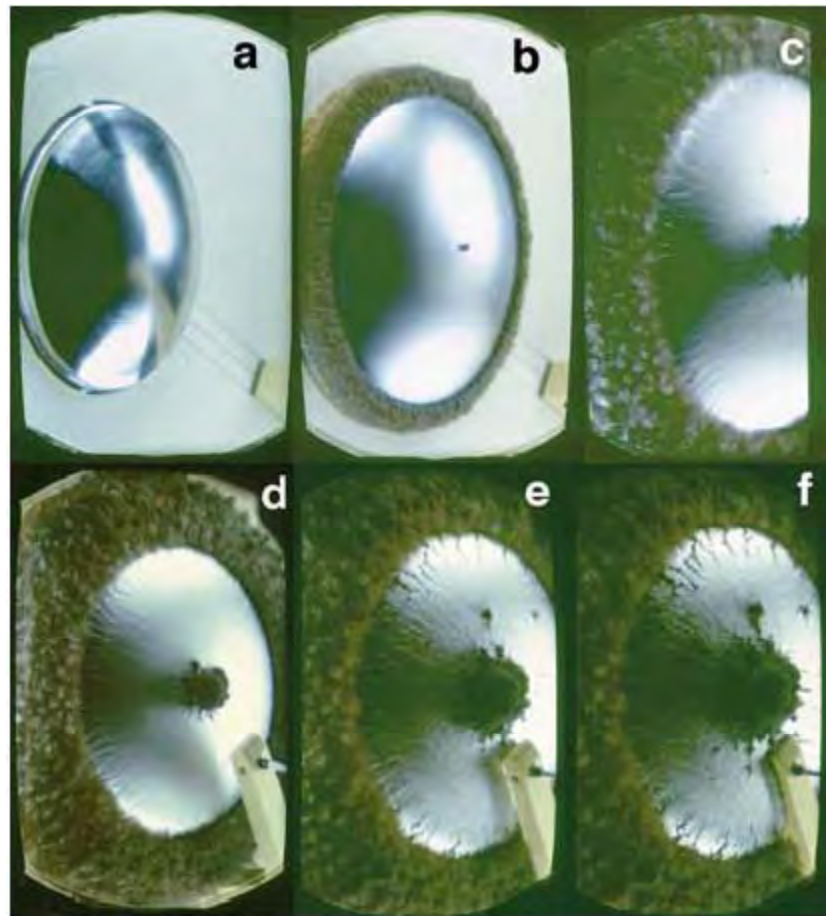
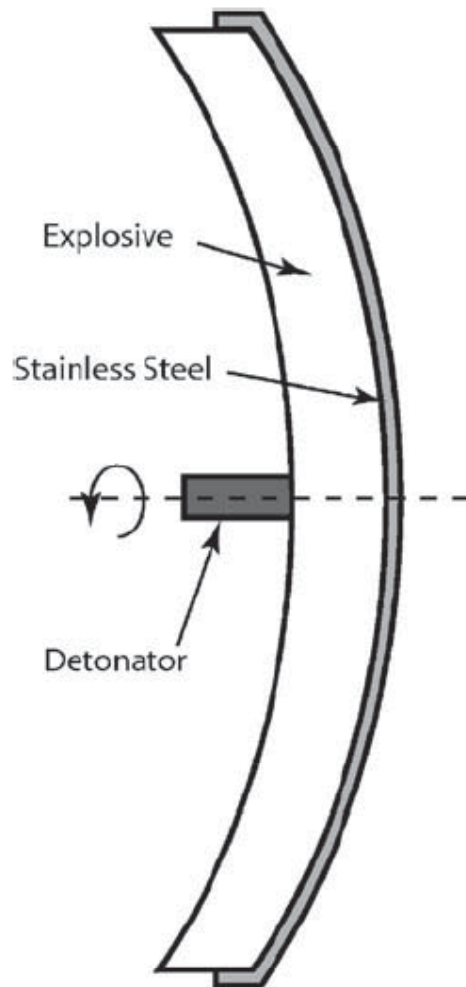
$$G_\epsilon \sim \frac{h^2}{|K_\epsilon|} \int_{K_\epsilon} W(\nabla u) dx$$

OTM - Fracture & fragmentation



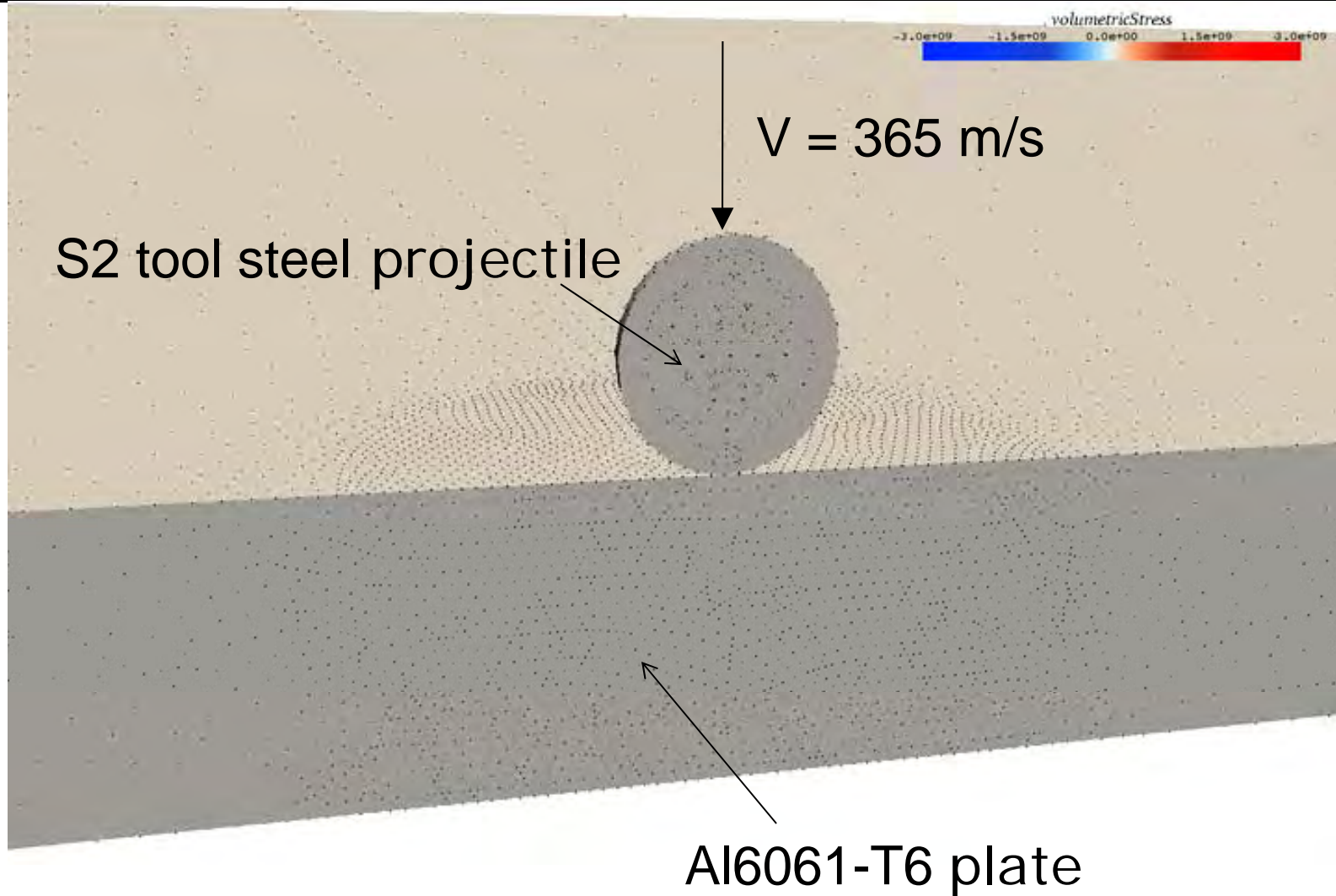
[Campbell *et al.*, 2007]

OTM - Fracture & fragmentation

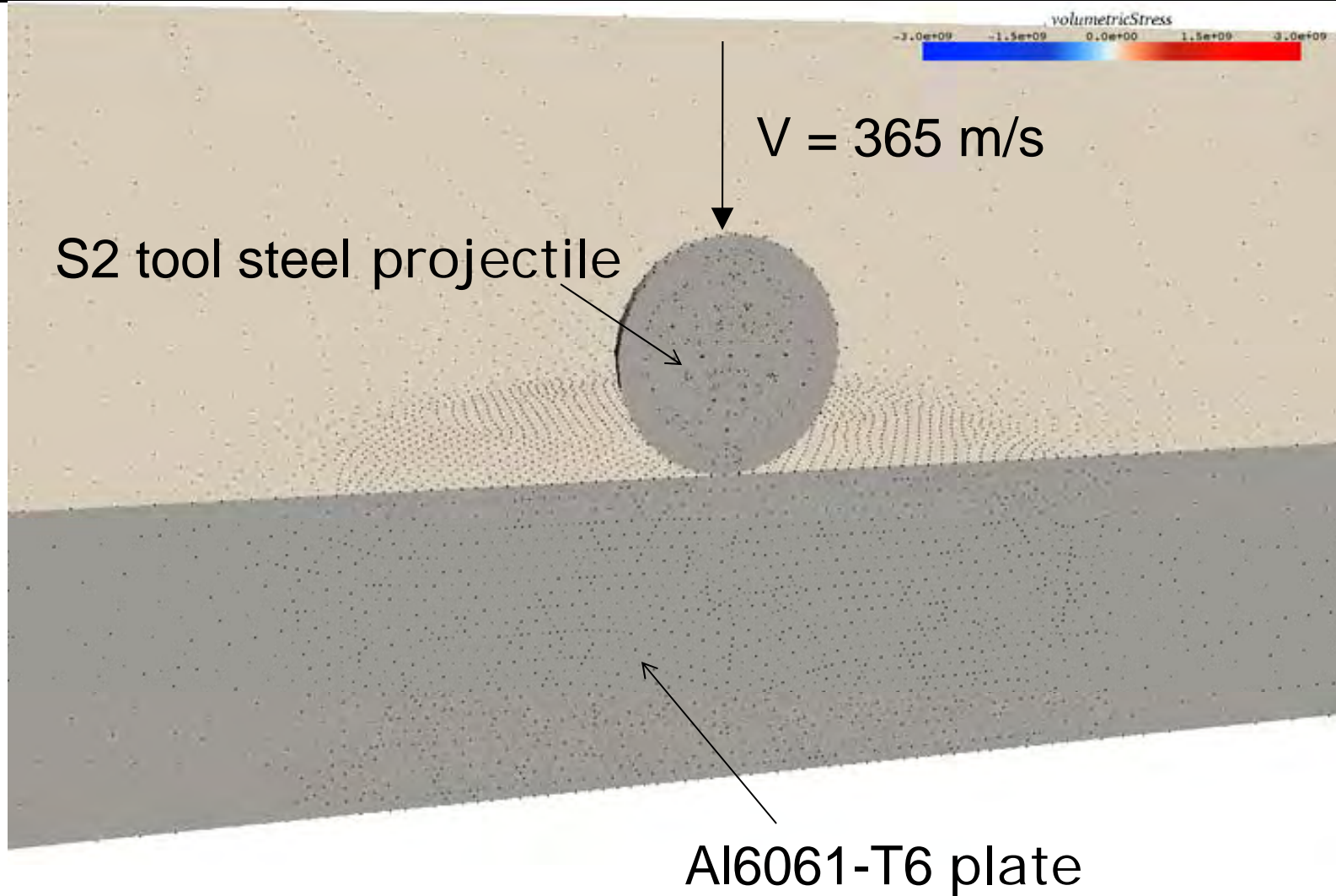


[Campbell *et al.*, 2007]

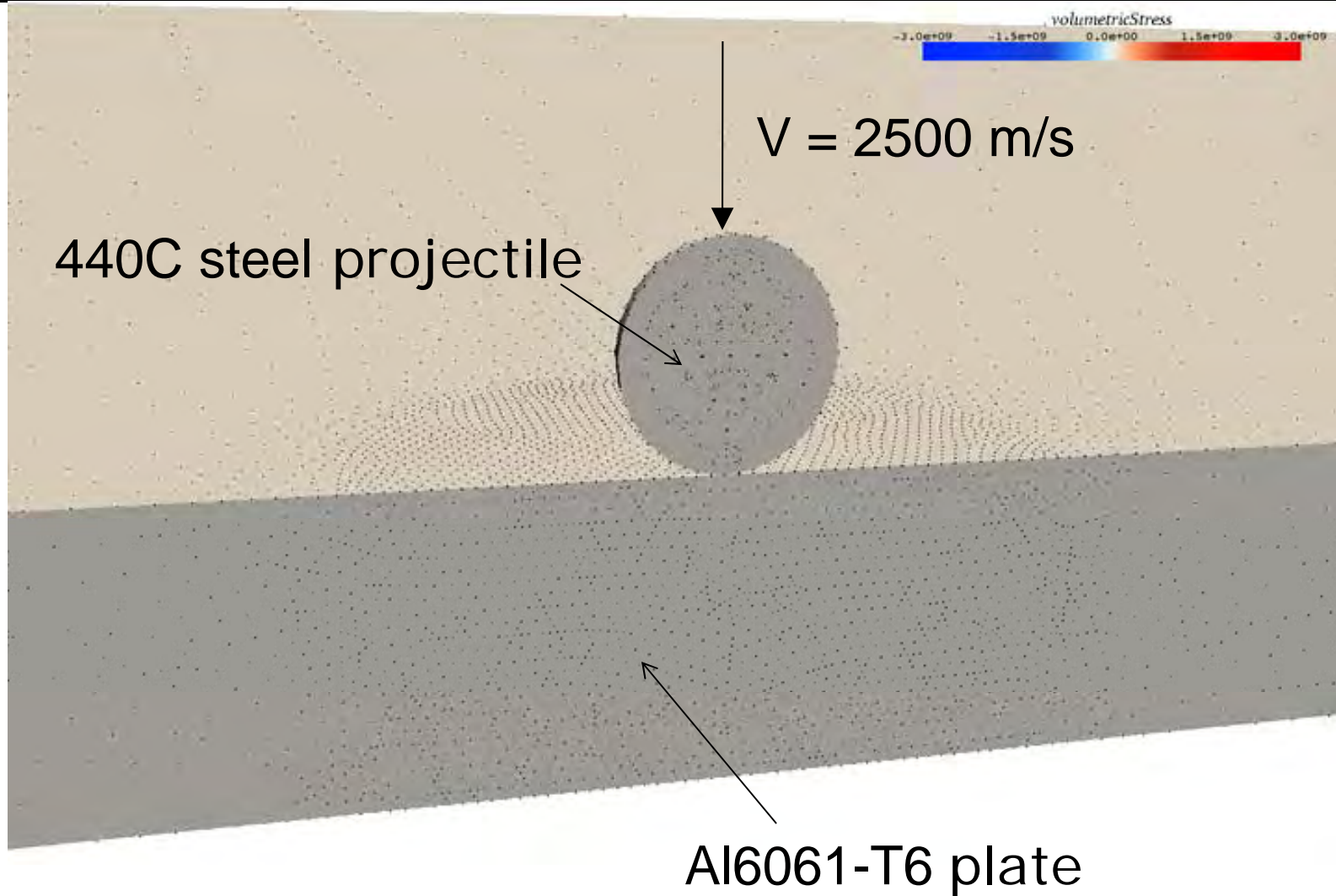
OTM — Terminal ballistics



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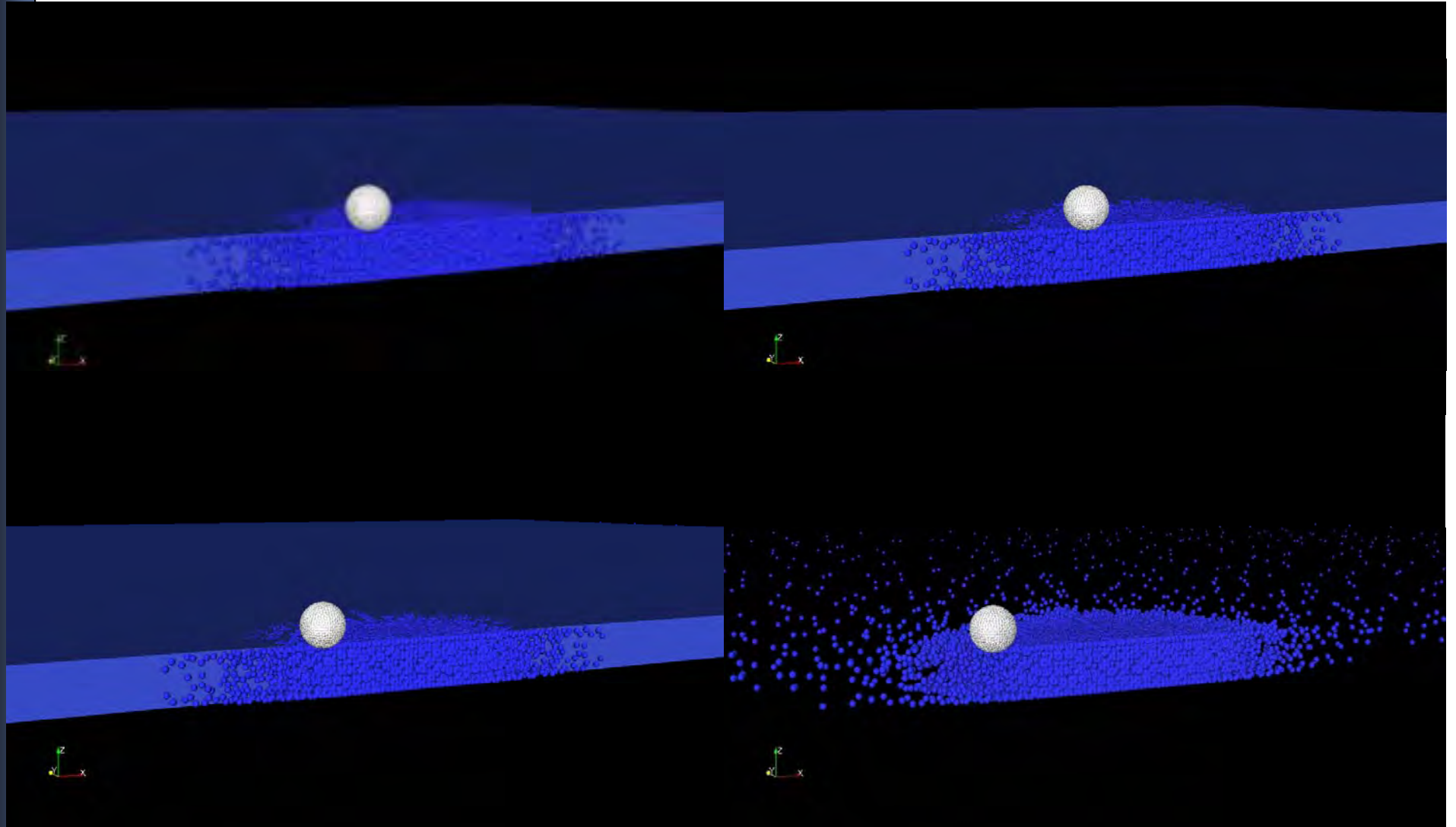


OTM — Terminal ballistics



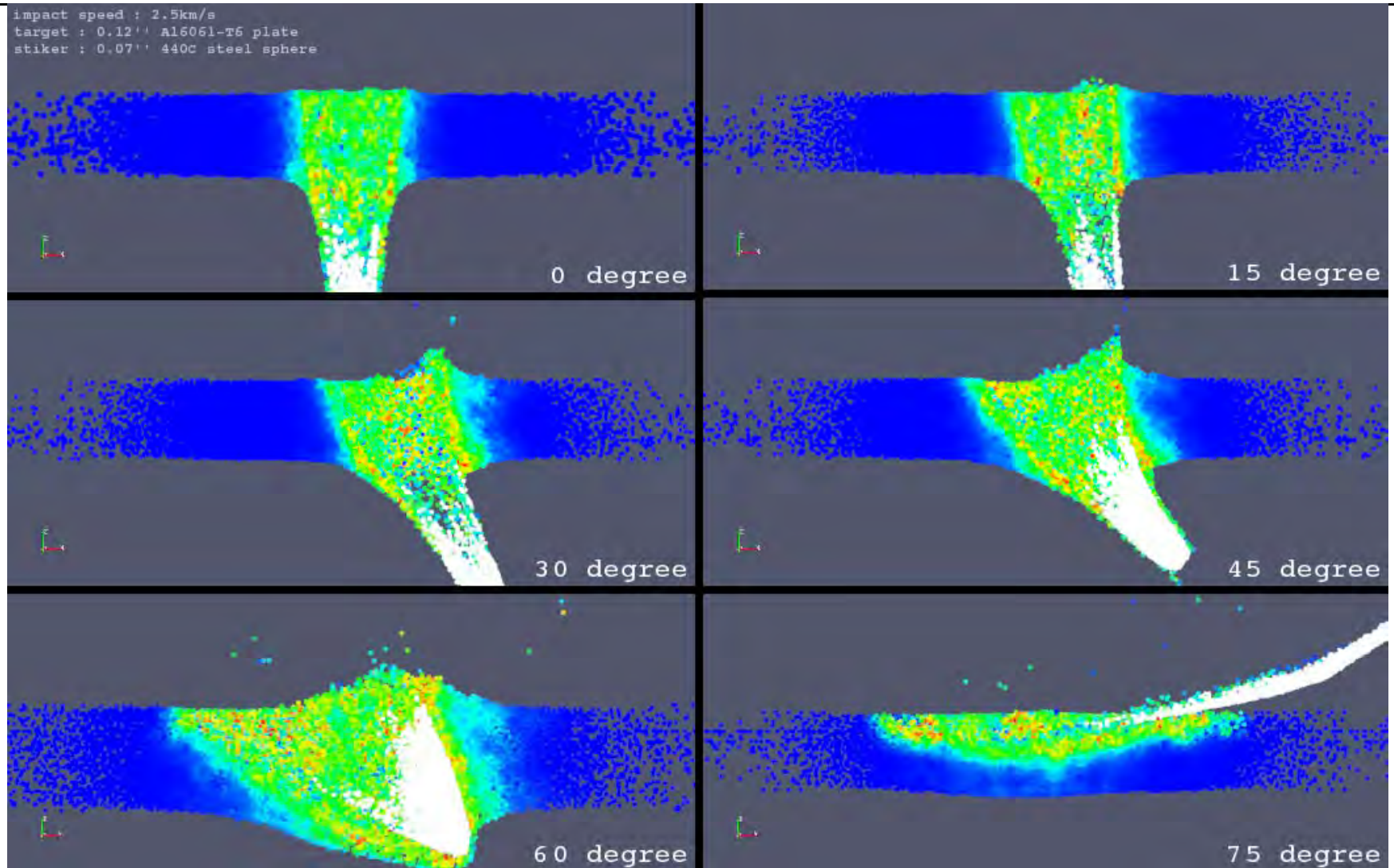
OTM — Terminal ballistics

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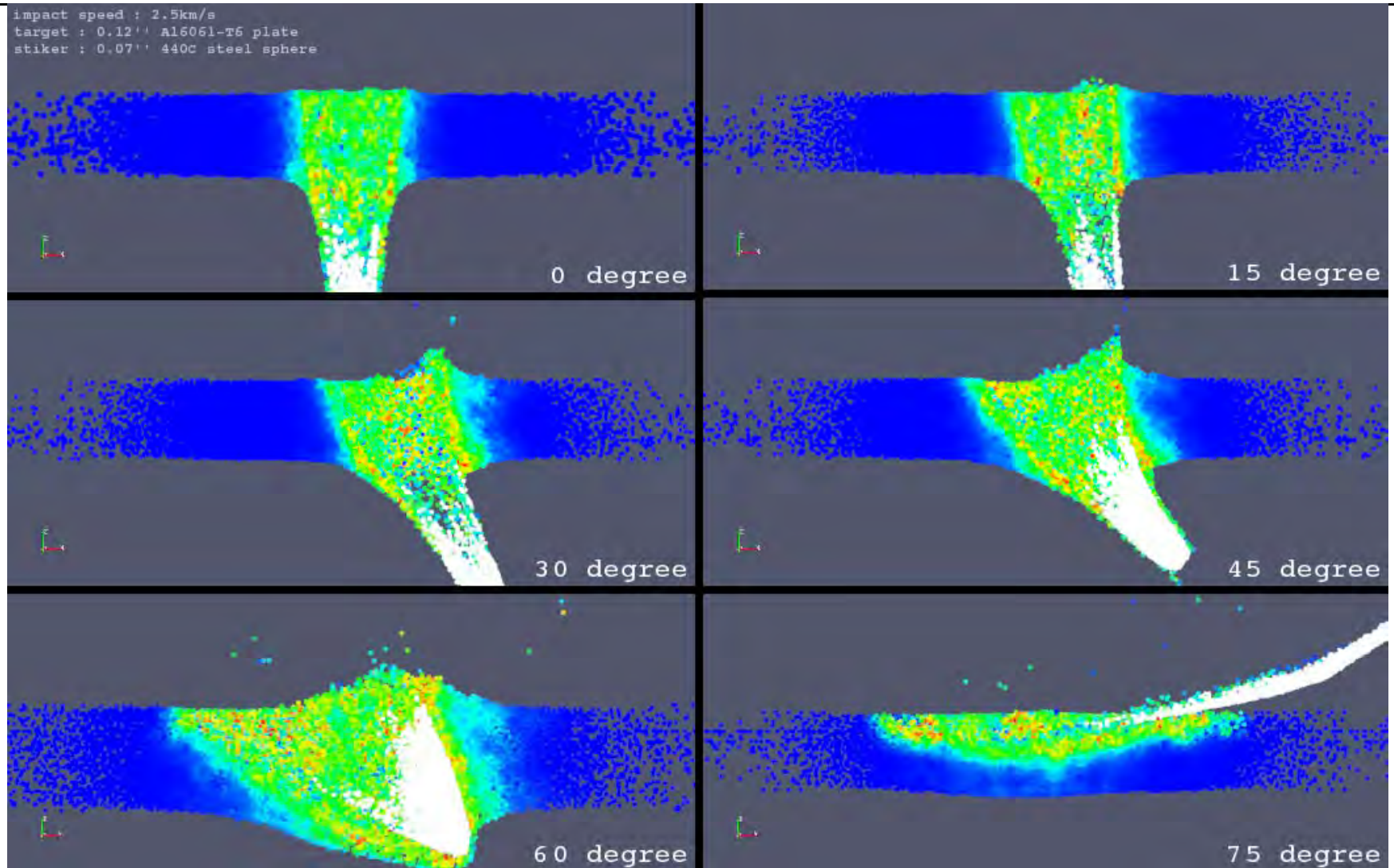
OTM – Terminal ballistics

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OTM – Terminal ballistics

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Case Study I – Steel/Al ballistics

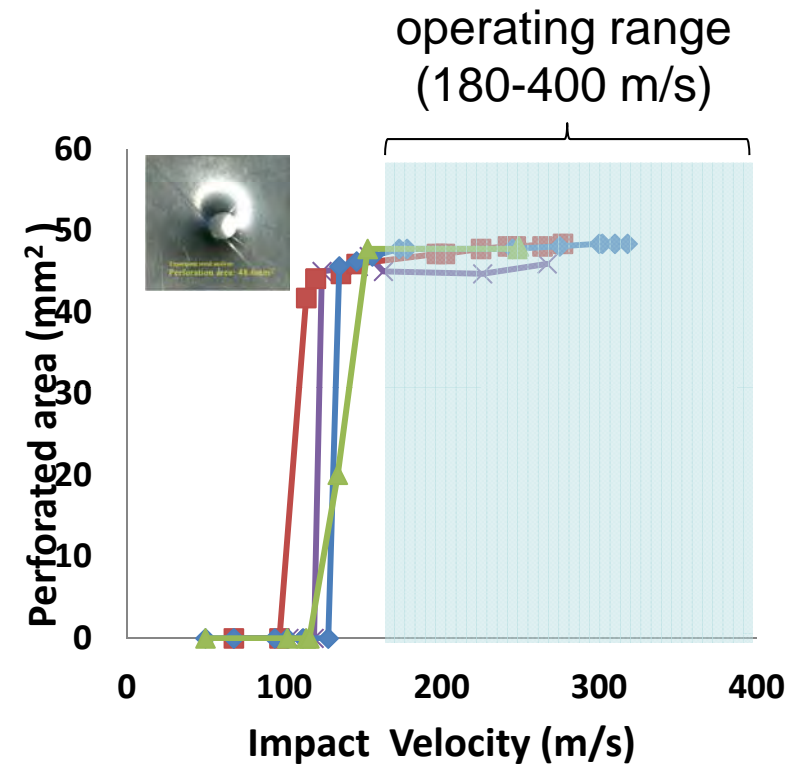


- McDiarmid inequality:

$$\text{PoF} = \mathbb{P}[F \leq a] \leq e^{-2CF^2}$$

$$CF = \frac{M}{U} = \frac{(\mathbb{E}[F] - a)_+}{D_F}$$

Model diameter D_F	thickness	4.33 mm ²
	velocity	4.49 mm ²
	total	6.24 mm ²
Model mean $E[F]$		47.77 mm ²
Confidence factor M/U		<u>7.66</u>



Steel/Al ballistics
response function

- Lethality can be certified with $\sim 10^{-51}$ confidence!
- Number of response function evaluations $\sim 2,000$

Uncertainty quantification ‘crimes’



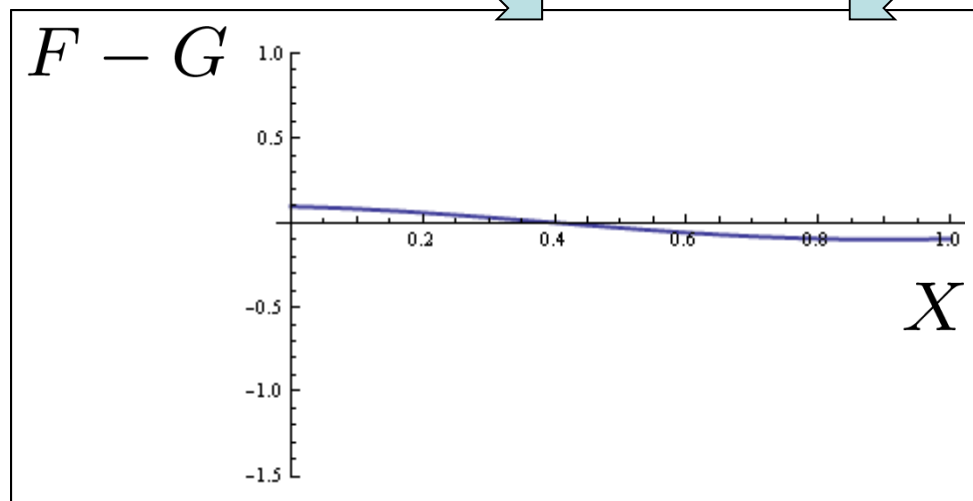
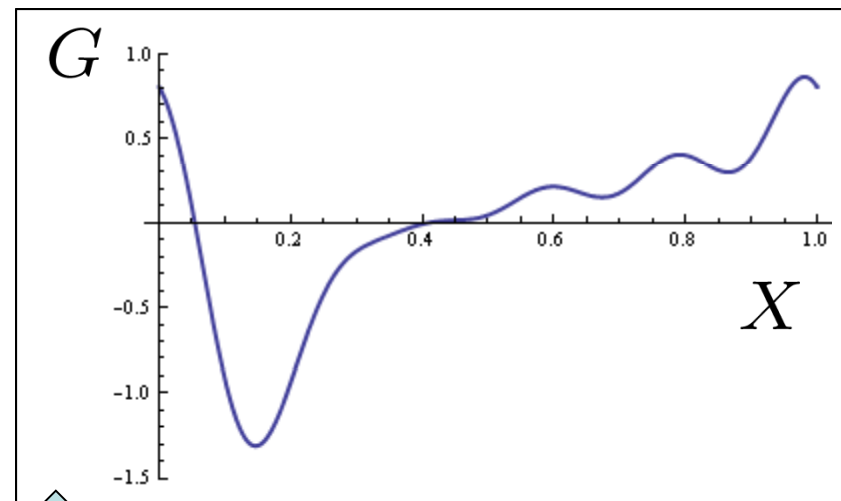
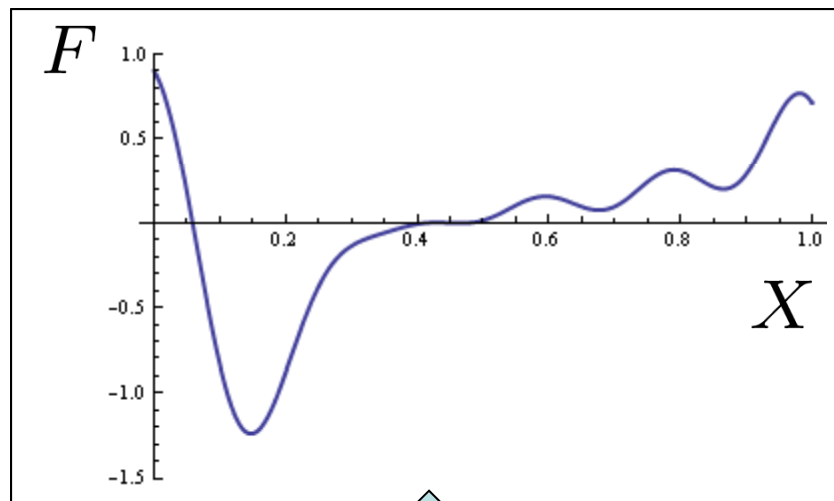
- Models are inexact in general!
- How does lack of model fidelity contribute to uncertainty?
- Is rigorous model-based certification possible in the face of modeling error?
- Mean performance $E[F]$ cannot be computed exactly for complex systems
- Instead, mean performance $E[F]$ is approximated by empirical mean:

$$\mathbb{E}[G] \approx \frac{1}{m} \sum_{i=1}^m Y^i \equiv \langle Y \rangle$$

- What is the effect of the empirical mean approximation on uncertainty quantification?

- Two functions that describe the system:
 - Experiment: $G(X)$
 - Model: $F(X)$
$$F(X) - G(X) \equiv \text{Modeling-error function}$$
- McDiarmid bound monotonic in diameter
- Triangular inequality: $D_G \leq D_F + D_{F-G}$
- Conservative certification criterion:
$$\mathbb{P}[G \leq a] \leq \exp \left(-2 \frac{(\langle Y \rangle - a + \alpha)_+^2}{(D_F + D_{F-G})^2} \right) \leq \epsilon,$$
- $\alpha = U m^{-\frac{1}{2}} (-\log \epsilon')^{\frac{1}{2}} : \textbf{Margin hit}$ (emp. mean)
- D_F : **Model diameter** (variability of model)
- D_{F-G} : **Modeling error** (badness of model)

Model-based QMU – McDiarmid



- Working assumptions:
 - $F-G$ far more regular than F or G alone
 - Global optimization for D_{F-G} converges fast (e.g. BFGS)
 - Evaluation of D_{F-G} requires few experiments

Model-based QMU – McDiarmid

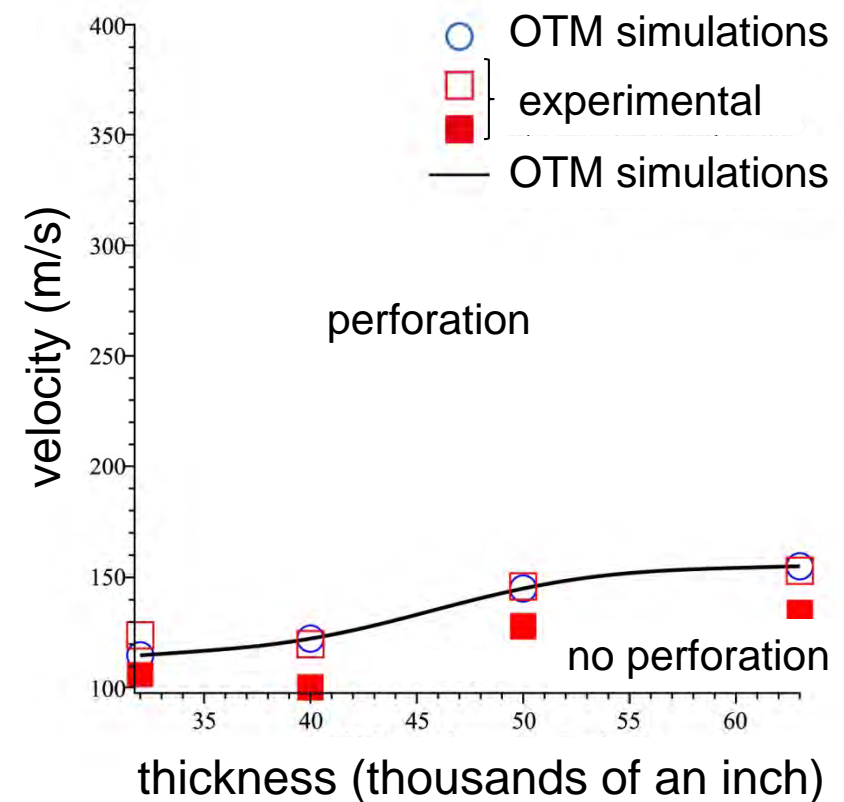
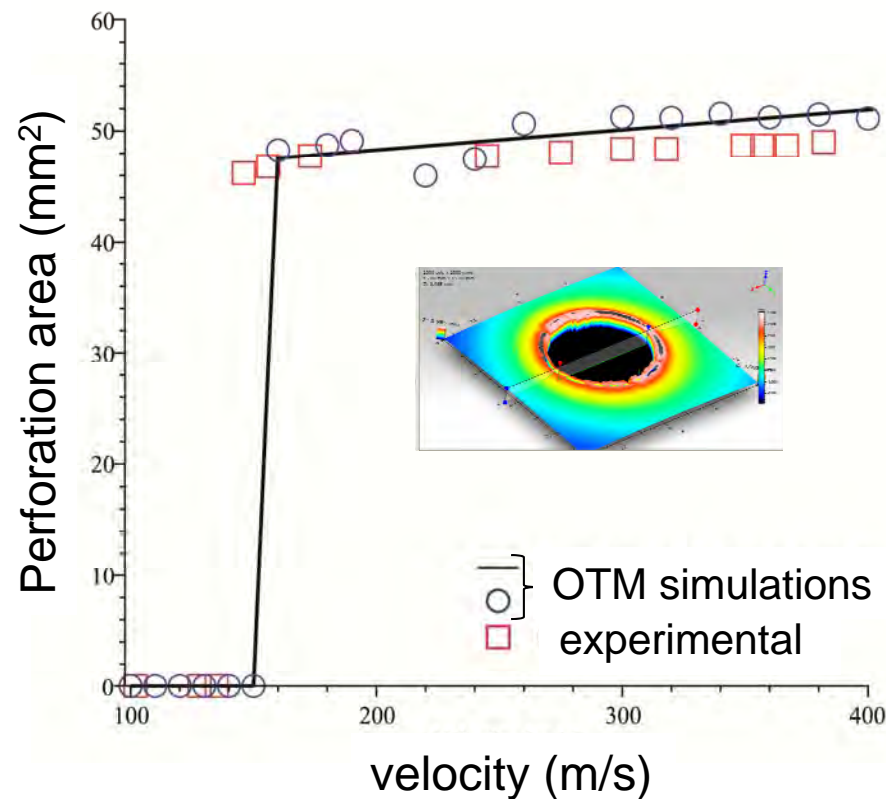


- Calculation of D_F requires exercising model only
- Uncertainty Quantification burden mostly shifted to modeling and simulation!



- Evaluation of D_{F-G} requires (few) experiments
- Rigorous certification not achievable by modeling and simulation alone!

Case Study – OTM modeling error

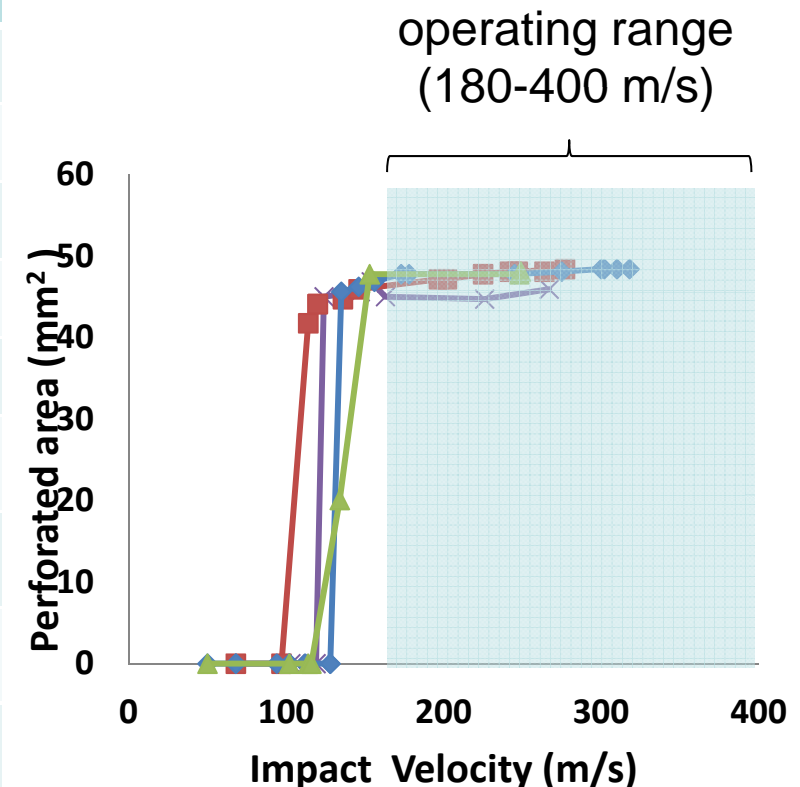


Measured vs. computed perforation area

Sample UQ Analysis – Ballistic range



Model diameter D_F	thickness	4.33 mm ²
	velocity	4.49 mm ²
	total	6.24 mm ²
Modeling error D_{F-G}	thickness	4.96 mm ²
	velocity	2.16 mm ²
	total	5.41 mm ²
Uncertainty $D_F + D_{F-G}$		11.65 mm ²
Empirical mean $\langle Y \rangle$		47.77 mm ²
Margin hit α ($\varepsilon' = 0.1\%$)		4.17 mm ²
Confidence factor M/U		<u>3.74</u>



- Perforation can be certified with $\sim 1-10^{-12}$ confidence!
- Total number of experiments $\sim 50 \rightarrow$ Approach feasible!

Beyond McDiarmid - Extensions

- A number of extensions of McDiarmid may be required in practice:
 - Some input parameters cannot be controlled
 - There are unknown input parameters (unknown unknowns)
 - There is experimental scatter (G defined in probability)
 - McDiarmid may not be tight enough (convergence?)
 - Model itself may be uncertain (epistemic uncertainty)
 - Data may not be available 'on demand' (legacy data)
- Extensions of McDiarmid that address these challenges include:
 - Martingale inequalities (unknown unknowns, scatter...)
 - Partitioned McDiarmid inequality (convergent upper bounds)
 - Optimal Uncertainty Quantification (OUQ)
 - Optimal models (least epistemic uncertainty)

Concluding remarks...

- QMU represents a paradigm shift in predictive science:
 - Emphasis on predictions with *quantified uncertainties*
 - Unprecedented integration between simulation and experiment
- QMU supplies a powerful organizational principle in predictive science: *Theorems run entire centers!*
- QMU raises theoretical and practical challenges:
 - Tight and measureable/computable probability-of-failure upper bounds (need theorems!)
 - Efficient global optimization methods for highly non-convex, high-dimensionality, noisy functions
 - Effective use of massively parallel computational platforms, heterogeneous and exascale computing
 - High-fidelity models (multiscale, effective behavior...)
 - Experimental science for UQ (diagnostics, rapid-fire testing...)...

Concluding remarks...

A background image of a red cannon on a wooden carriage with large spoked wheels, positioned in front of a classical building with a pedimented entrance. A palm tree is visible on the left, and a street lamp is on the right. The image has a light grid overlay.

Thank you!