

# Solid Dynamics

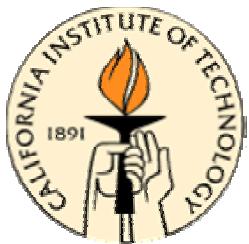
## Dynamic fracture and fragmentation

## Modeling and Simulation

M. Ortiz (Caltech) Group leader  
I. Arias, J. Knap, A. Mota

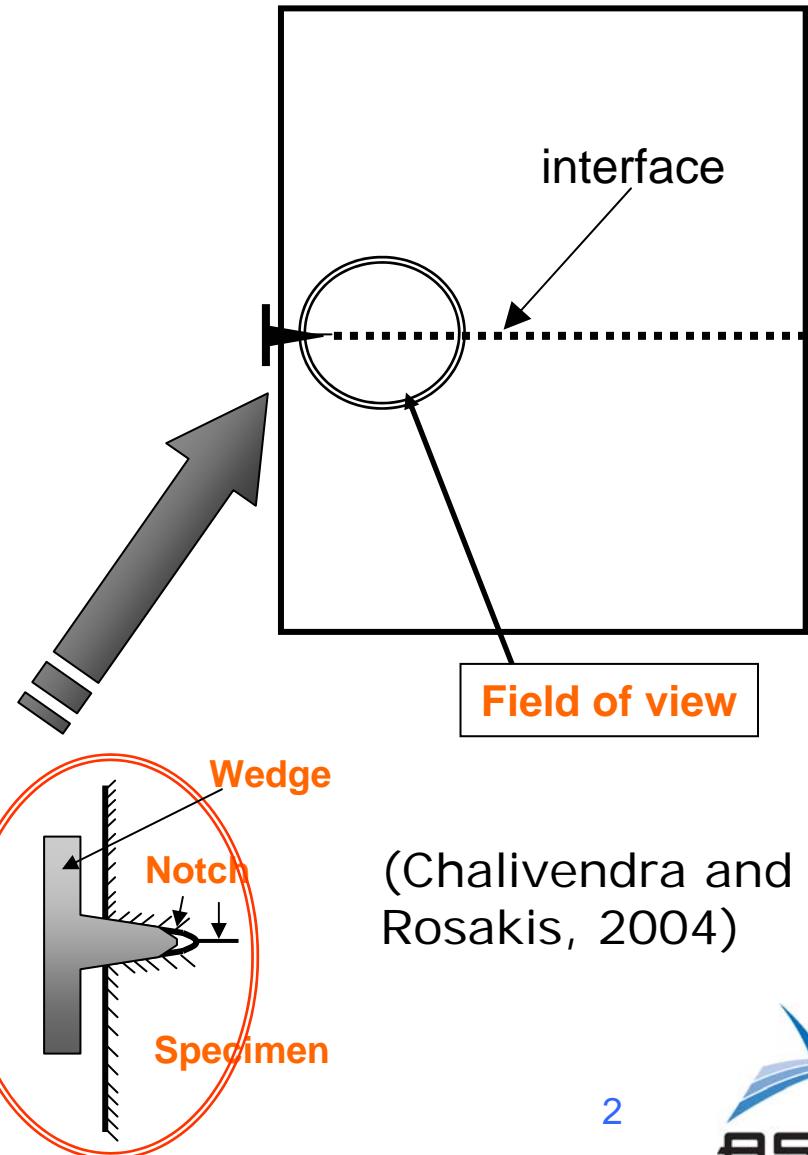
A.J. Rosakis, V. Chalivendra, S. Hong

Caltech ASC Center – Midyear review  
*April 13-24, 2005*



# Description of experiment (IV)

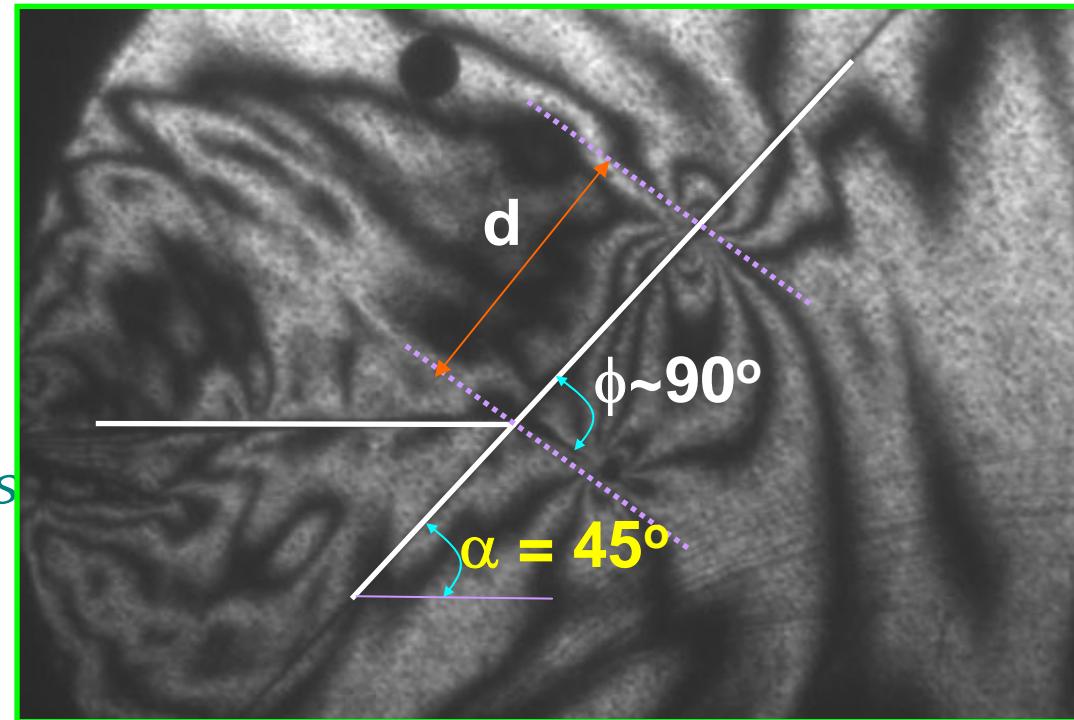
- Horizontal interface: Loctite 384
- Material: Homalite-100
- Sample size: 450 x 375 x 9.5 (mm)
- Boundary conditions: traction free
- Loading:
  - *Experiment: Hopkinson bar*
  - *Simulation: distributed tractions on notch surfaces*
- Linear cohesive law (*material properties from experiment*)
- $l_c = 1.267 \text{ [mm]} = 1267 \text{ [\mu m]}$



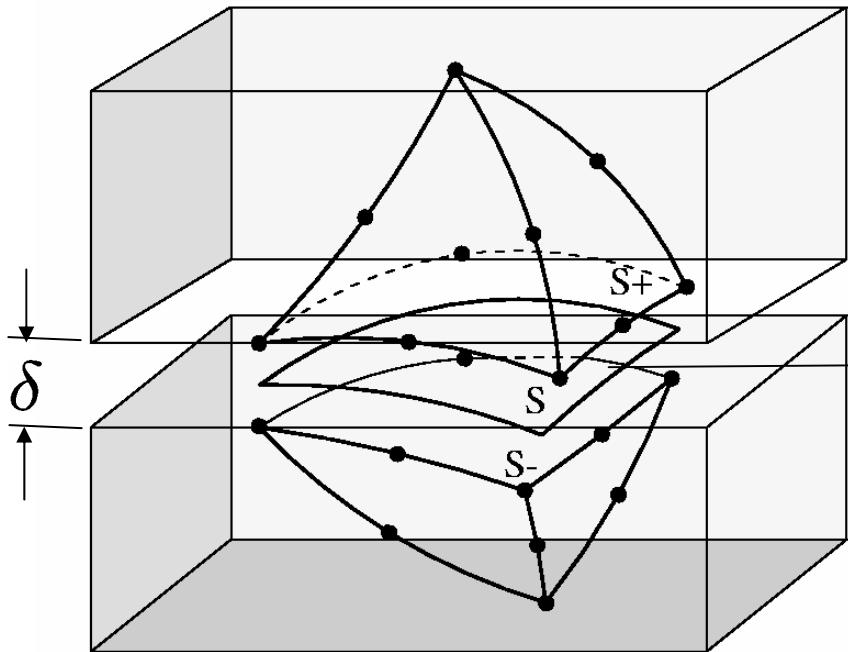
(Chalivendra and Rosakis, 2004)

# Validation metrics

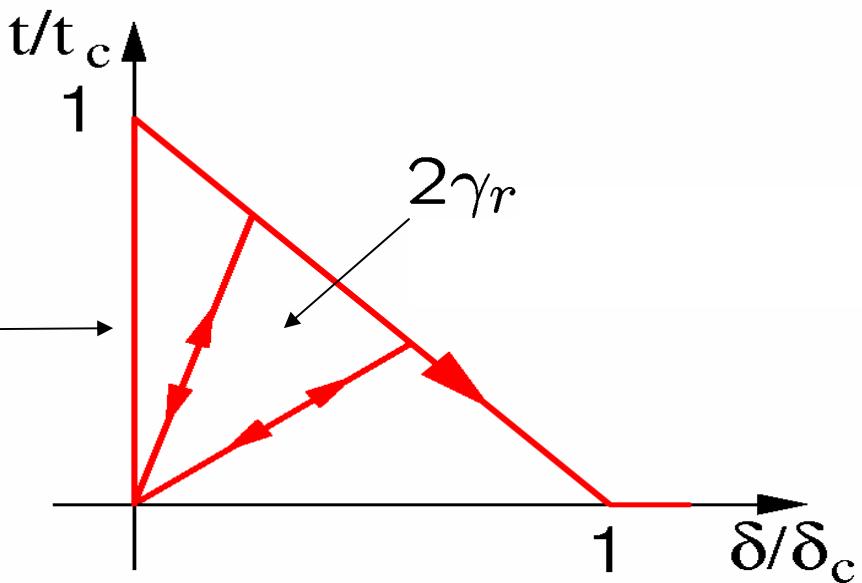
- Crack initiation time
- Crack tip arrival time at the interface
- Crack speed
- Crack length
- Deflection length ( $d$ )
- Penetration angle ( $\phi$ )
- Fracture parameters
  - *Mode-I/II stress intensity factors*
  - *Mode mixity*
  - *Non-singular stress*



# Approach – Cohesive elements



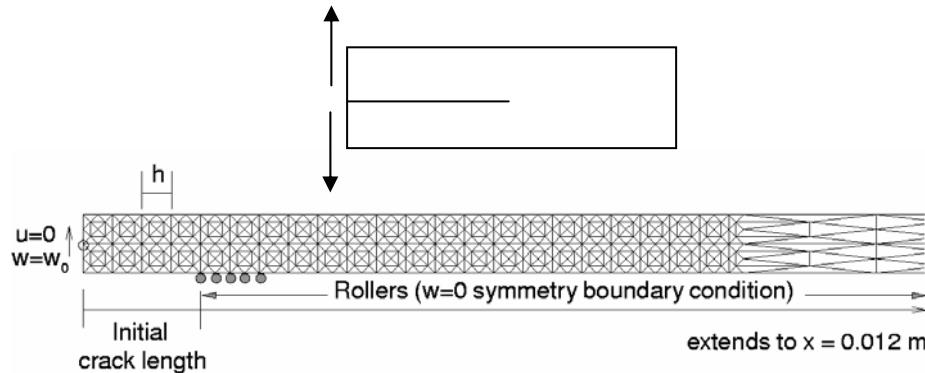
Quadratic cohesive element  
(Ortiz and Pandolfi '99)



Cohesive law  
(Camacho and Ortiz '96,  
Nguyen and Ortiz '02,  
Hayes, Ortiz and Carter '04)



# Approach – Cohesive elements



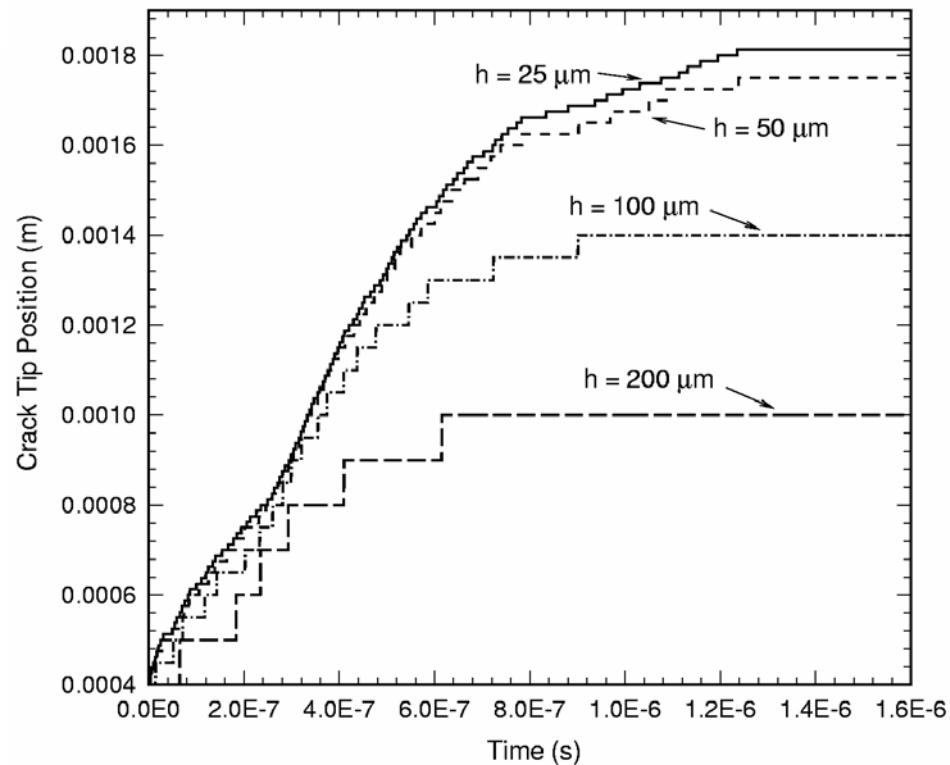
Double cantilever specimen

- Characteristic size:

$$l_c = \frac{\pi}{8} \frac{E}{1 - \nu^2} \frac{G_c}{\sigma_c^2}$$

- Characteristic time:

$$t_c = \frac{l_c}{c_R}$$



Crack-tip trajectory  
as a function of element size  
(Camacho and Ortiz, 1996)

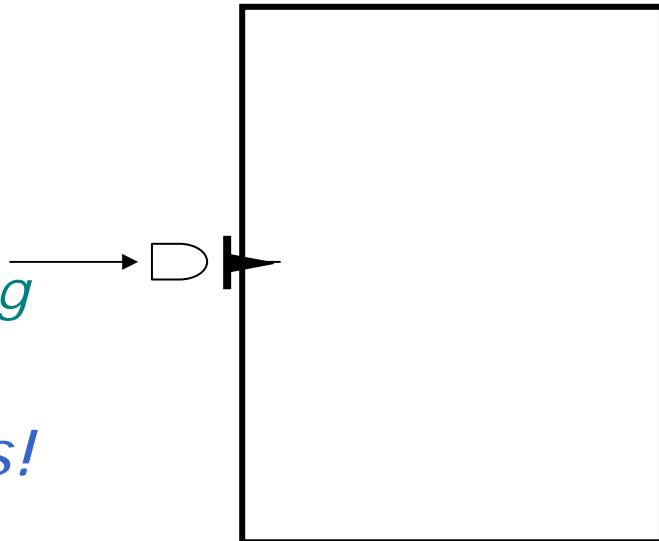


# Fracture model-Implementation issues

- Conflicting requirements:
  - *Experiment: need large sample size for proper instrumentation*
  - *Simulation: need small number of elements to reduce computational cost*
- Possible solutions
  - *Adaptive Mesh Refinement*
  - *Massively parallel computing*
- Model size:

2D - *100 million elements!*

3D - ?



508 x 154 x 6 (mm)



6

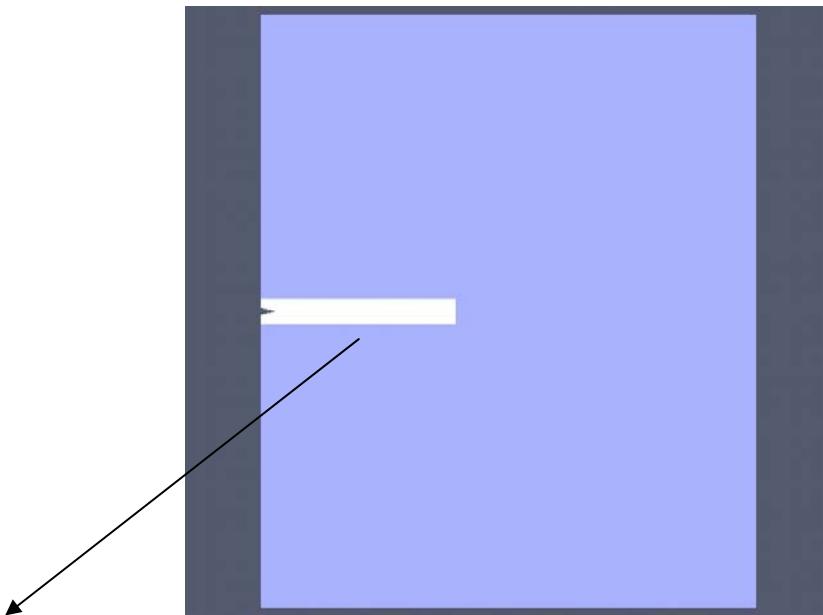


# Brittle fracture - Latest runs

- Two dedicated weekends of 450 ALC nodes (900 processors):
  - *Level 5 subdivision (~33 million elements) for 60 hours*
  - *Level 4 subdivision (~8 million elements); exploring parameter space; each run 12 hours*
- One dedicated weekend of 900 ALC nodes (1,800 processors):
  - *Level 6 subdivision (~133 million elements) for 60 hours (only 15μs mark reached)*
- Batch queues 256-450 ALC nodes (512-900 processors):
  - *Level 4 subdivision (~8 million elements) for 12-24 hours*
- Need lots of storage:
  - *checkpoints every 1μs i.e. 150-200 checkpoints per run*
  - *each checkpoint ~100MB/processor*
- ALC – great environment and outstanding level of technical support for these large runs.

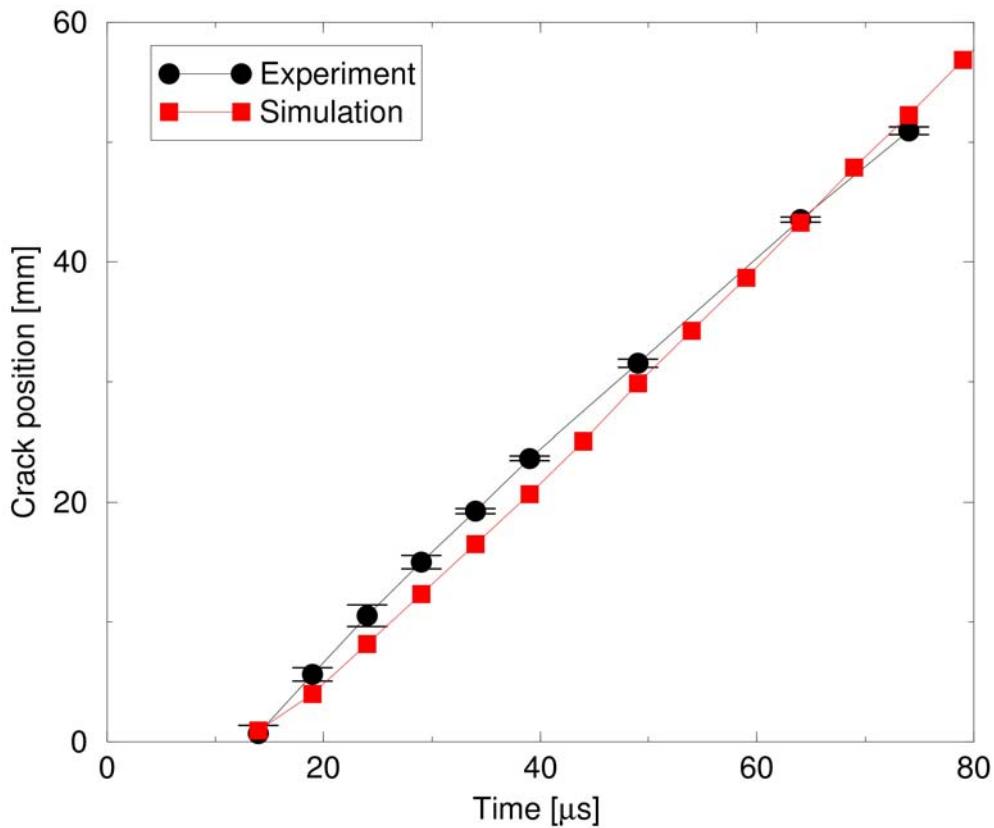


# Brittle fracture - Latest runs



(Knap and Ortiz, 2005)

# Metrics-Comparison (III)



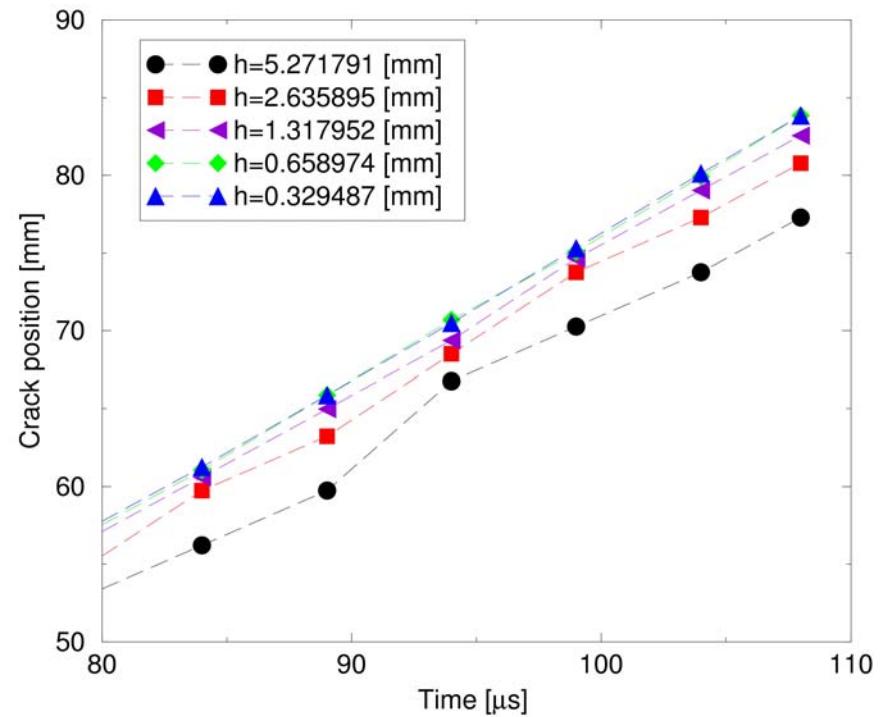
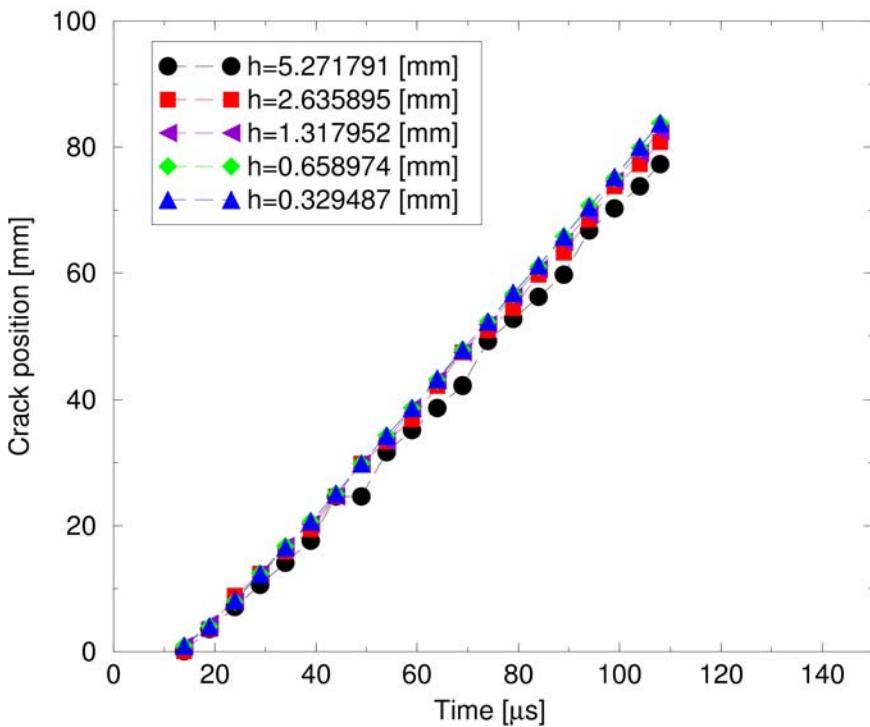
- Experimental velocity 832 [m/s]
- Simulation velocity 893 [m/s]
- Experimental crack initiation time: 13  $\mu$ m
- Simulation crack initiation time: 13-14  $\mu$ m

(Knap and Ortiz, 2005)



# Convergence analysis

$$l_c = 1.267 \text{ [mm]}$$

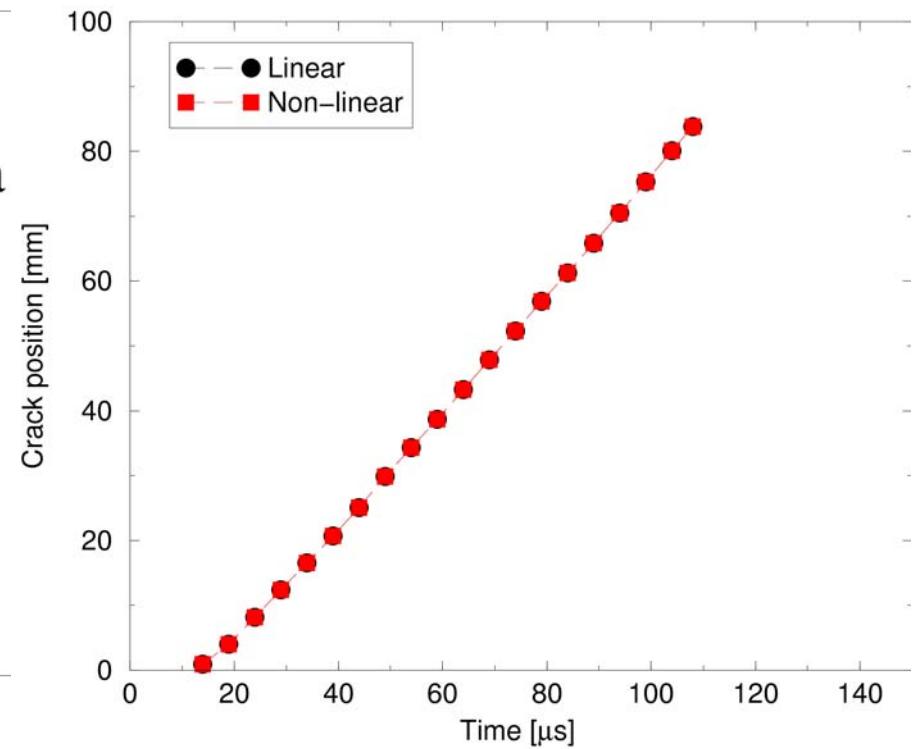
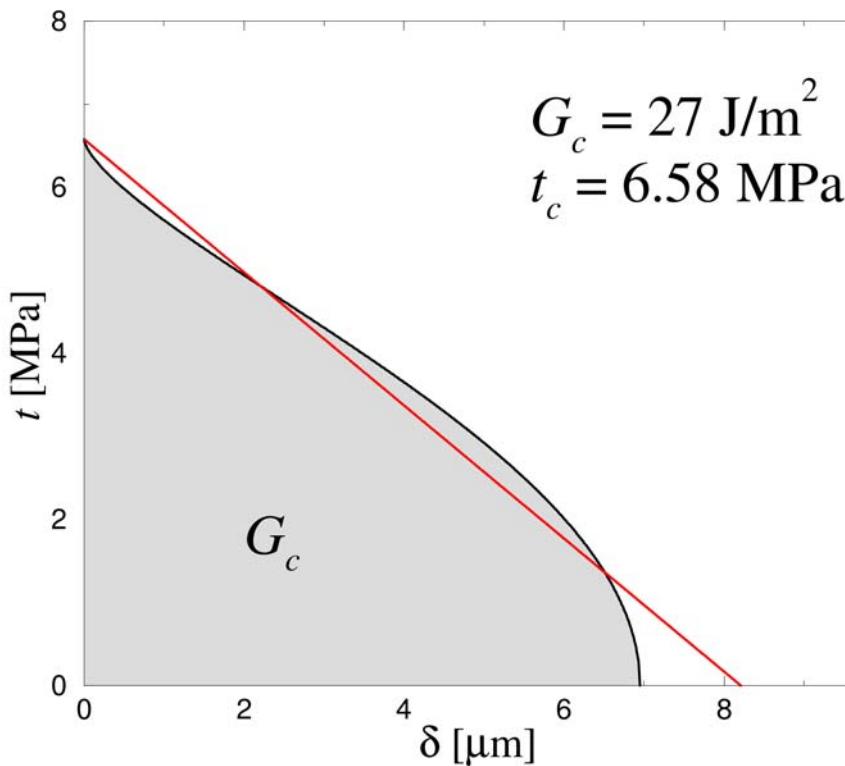


(Knap and Ortiz, 2005)



# Sensitivity to cohesive law

Level 4 subdivision ( $h=0.3295$  [mm])

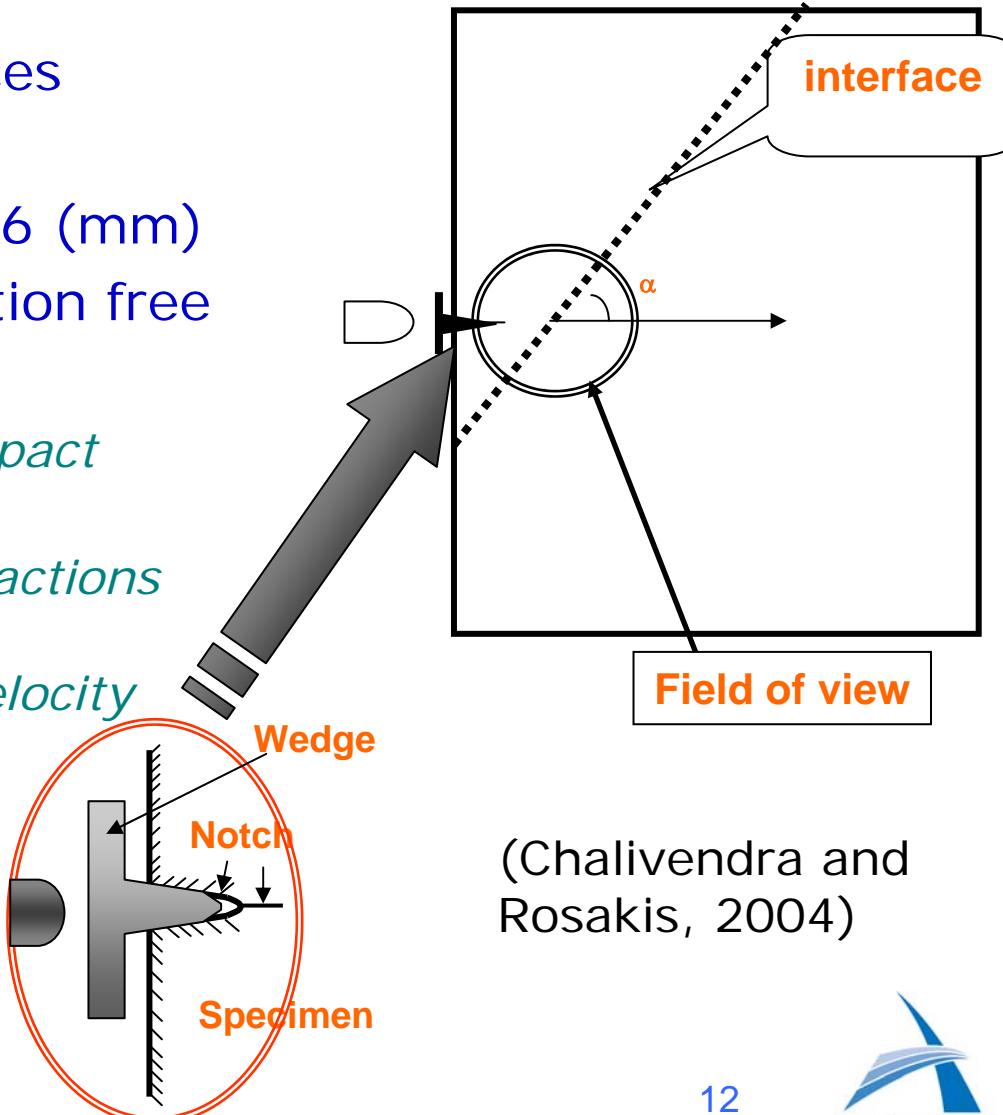


(Knap and Ortiz, 2005)



# Path forward - Experiments

- 45° and 60° weak interfaces
- Material: Homalite-100
- Sample size: 508 x 154 x 6 (mm)
- Boundary conditions: traction free
- Loading:
  - *Experiment: projectile impact velocity*
  - *Simulation: distributed tractions on notch surfaces (impact velocity dependent)*
- Linear cohesive law

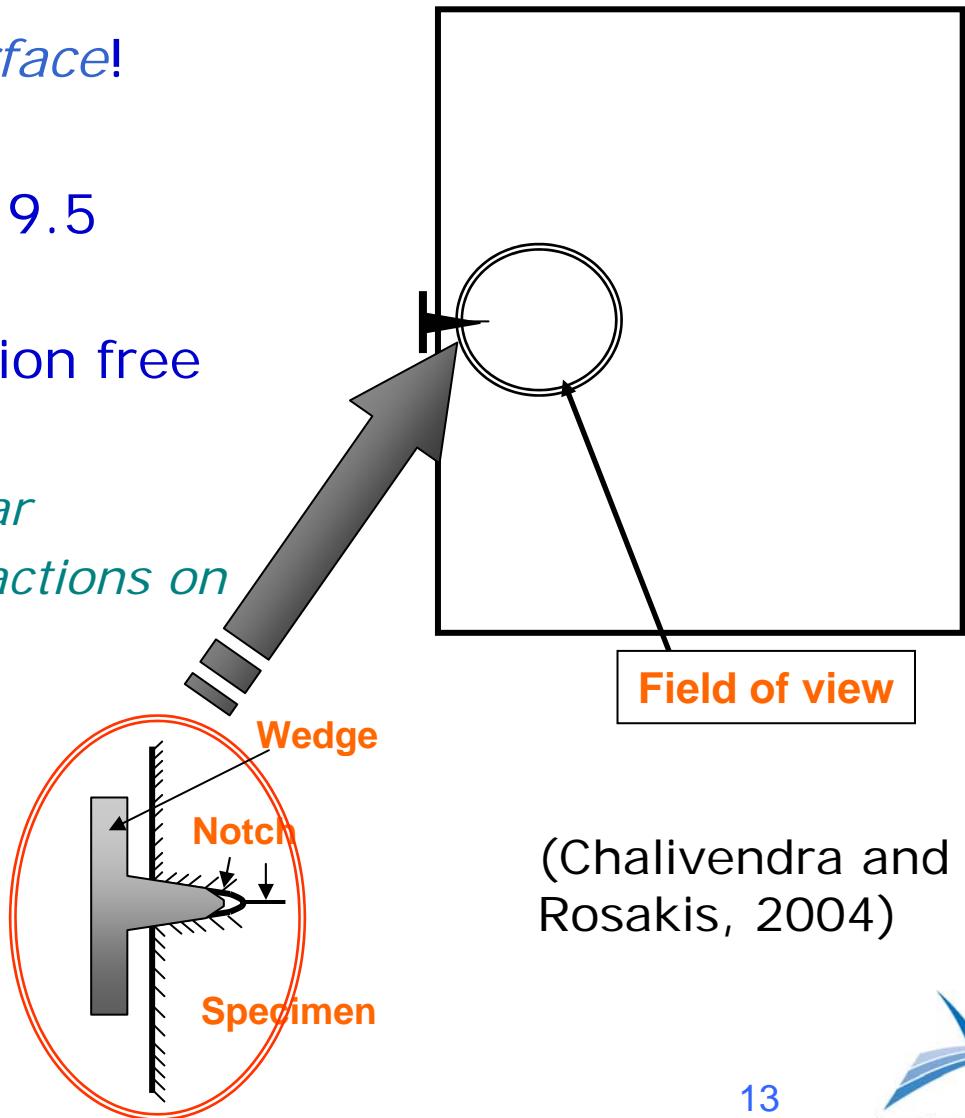


(Chalivendra and Rosakis, 2004)

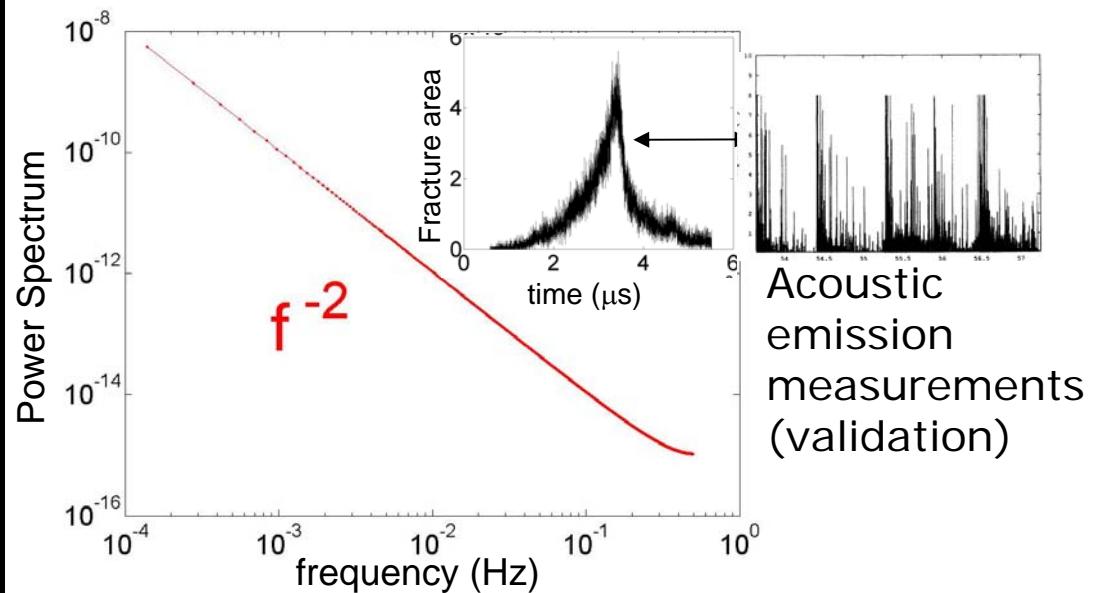
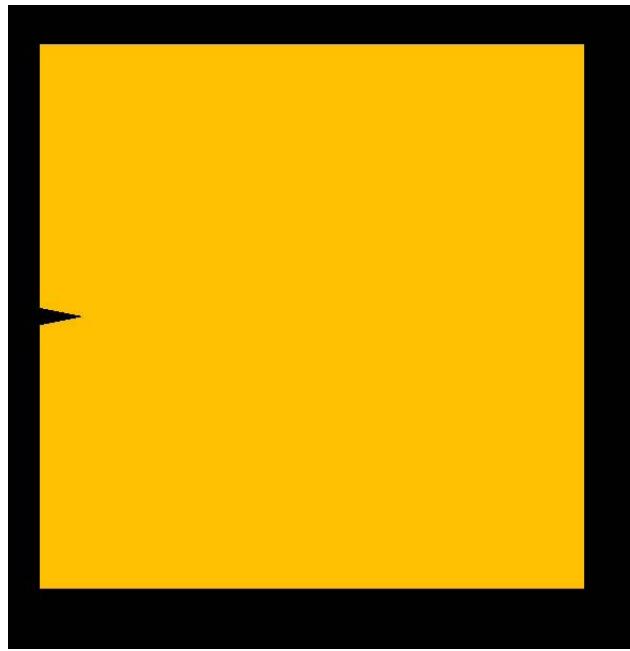


# Path forward - Experiments

- Monolithic sample-*no interface!*
- Material: Homalite-100
- Sample size: 450 x 375 x 9.5 (mm)
- Boundary conditions: traction free
- Loading:
  - *Experiment: Hopkinson bar*
  - *Simulation: distributed tractions on notch surfaces*
- Linear cohesive law
- $l_c = 0.094 \text{ [mm]} = 94 \text{ [\mu m]}$



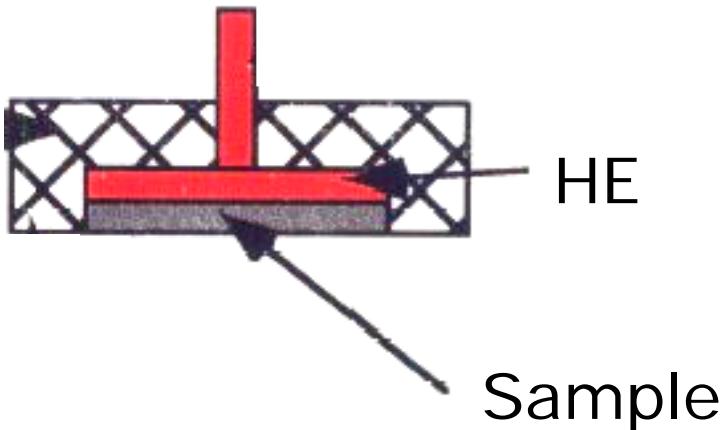
# Path forward – Highly driven systems



- Power spectrum  $1/f^2$  characteristic of diffusion!
- Results suggest that highly driven branching is governed by a diffusion equation
- Validation from acoustic emission measurements

(I. Arias, J. Knap and M. Ortiz '04)

# Path forward – Highly driven systems

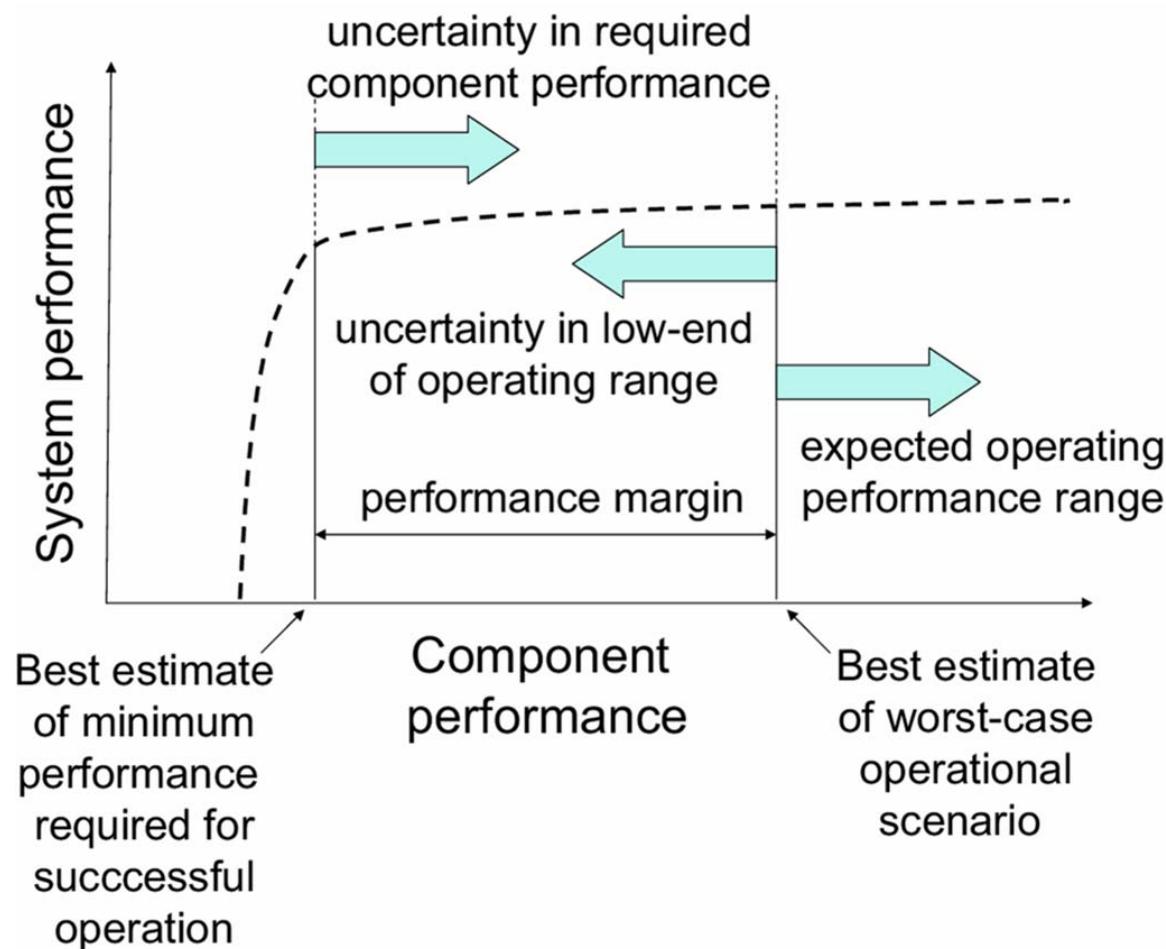


(Donald L. Griswold, LLNL)



# Part forward – Uncertainty Quantification

- Assess uncertainties in performance measures



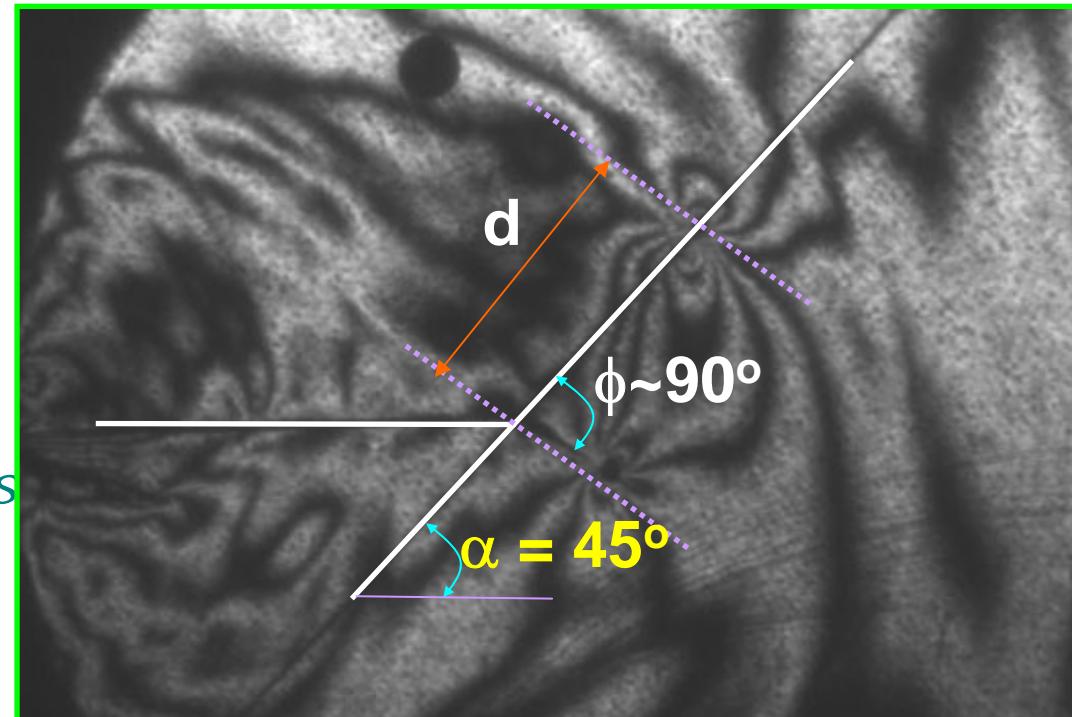
# Uncertainty Quantification – Input

- Finite element model:
  - *Sample dimensions (width x height x thickness)*
  - *Notch radius*
  - *Pre-crack length*
  - *Mesh size*
  - *Loading data*
- Bulk material data (Homalite):
  - *Constitutive relation (Neo-hookean)*
  - *Mass density*
  - *Young's modulus*
  - *Poisson's ratio*
- Interface material data (Loctite 384)
  - *Functional form of the cohesive law*
  - *Fracture strength  $t_c$*
  - *Critical strain-energy release rate  $G_c$*
  - *Shear/tension coupling coefficient  $\beta$*



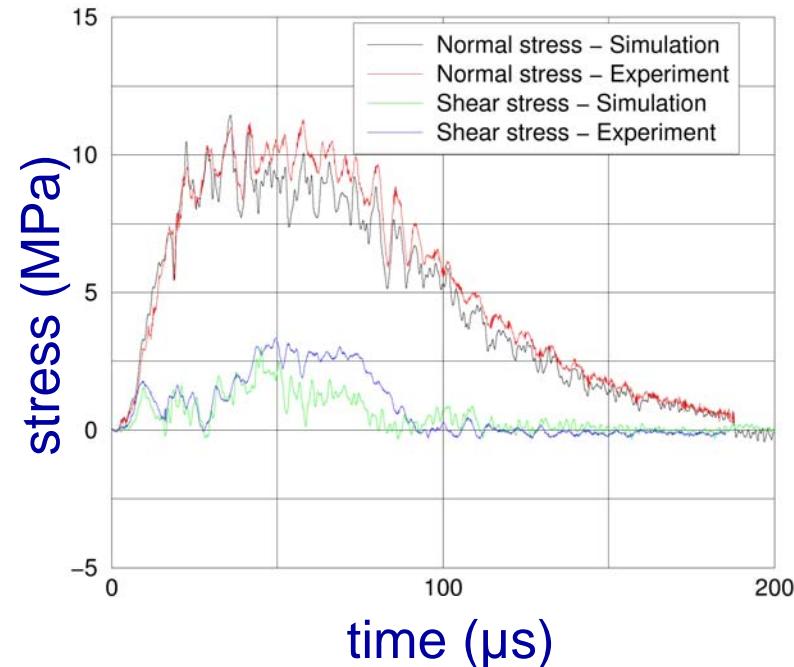
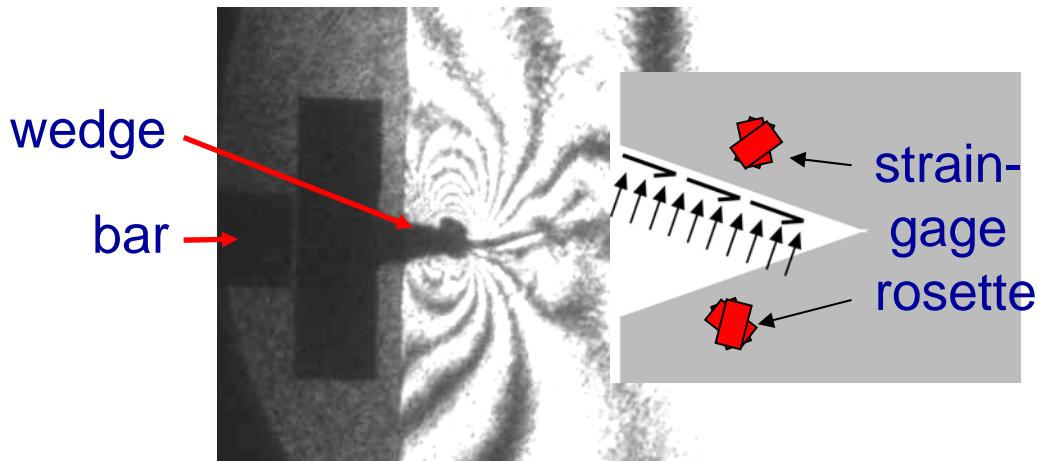
# Uncertainty Quantification - Measures

- Crack initiation time
- Crack tip arrival time at the interface
- Crack speed
- Crack length
- Deflection length ( $d$ )
- Penetration angle ( $\phi$ )
- Fracture parameters
  - *Mode-I/II stress intensity factors*
  - *Mode mixity*
  - *Non-singular stress*



# Uncertainty Quantification - Loading

## Direct loading measurements



Notch and fatigue pre-crack included in geometrical model, finite-element mesh



# Uncertainty Quantification – Resolution

- Homalite-100 characteristic length –  $l_c = 0.094$  [mm]
- Element sizes - *uniform subdivision*

Subdivision level	Element size [mm]	Number elements
0	5.271	32,440
1	2.636	129,760
2	1.318	519,040
3	0.659	2,076,160
4	0.329	8,304,640
5	0.165	33,218,560
6	0.082	132,874,240



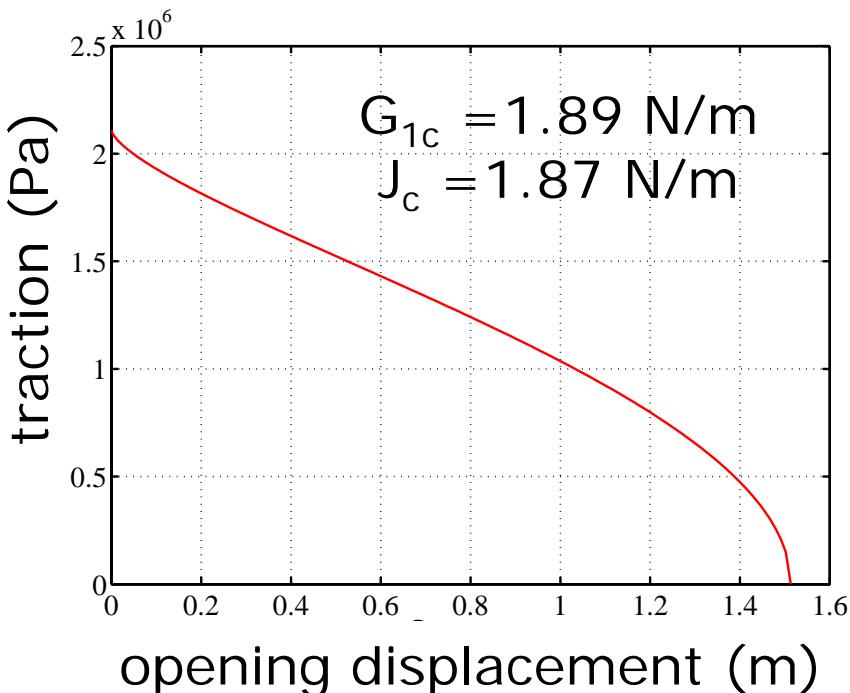
# Uncertainty Quantification – Resolution

- Level 4 subdivision – *unresolved mesh!*
- Need to run level 6 subdivision (132 million elements) for  $\sim 100 \mu\text{s}$ .
- 1,800 CPUs of *ALC* (LLNL) –  $15\mu\text{s}$  per 48h!
- Substantial performance improvements necessary (performance analysis and tuning in progress- S. Brunett).
- Modify the experimental setup to allow for changes in the material fracture properties- increase  $l_c$ .

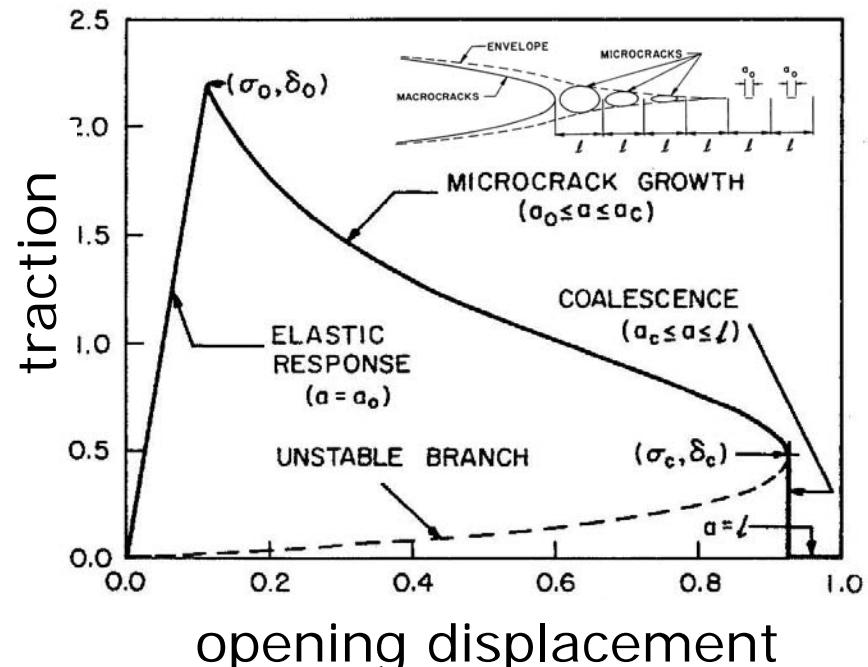


# Uncertainty Quantification - Physics

- Identification of cohesive law:



(S. Hong and A.J. Rosakis)



(M. Ortiz, *IJSS*, 1988)



# Uncertainty Quantification – TODO list

Regard performance measures as dynamical system:

$$\dot{\mathbf{x}}(t, \omega) = \mathbf{f}(\mathbf{x}(t, \omega), \omega).$$

- Stochastic Galerkin, Polynomial Chaos:

$$\mathbf{x}(t, \omega) = \sum_{m=1}^M \hat{\mathbf{x}}_m(t) \phi_m(\omega),$$

- Equation-free stochastic Galerkin projection

$$\hat{\mathbf{f}}_m = \frac{1}{\langle \phi_m^2(\omega) \rangle} \left\langle \mathbf{f} \left( \sum_{m=1}^M \hat{\mathbf{x}}_m(t) \phi_m(\omega), \omega \right), \phi_m(\omega) \right\rangle.$$

- Optimal sampling of parameters.

