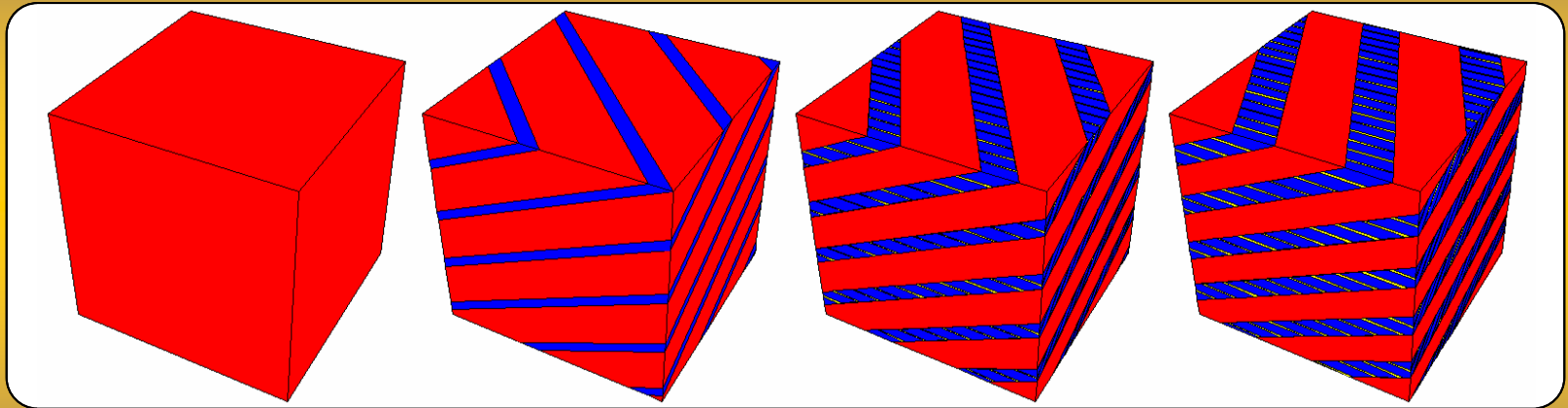


The importance of shear in the $bcc \rightarrow hcp$ transformation in iron



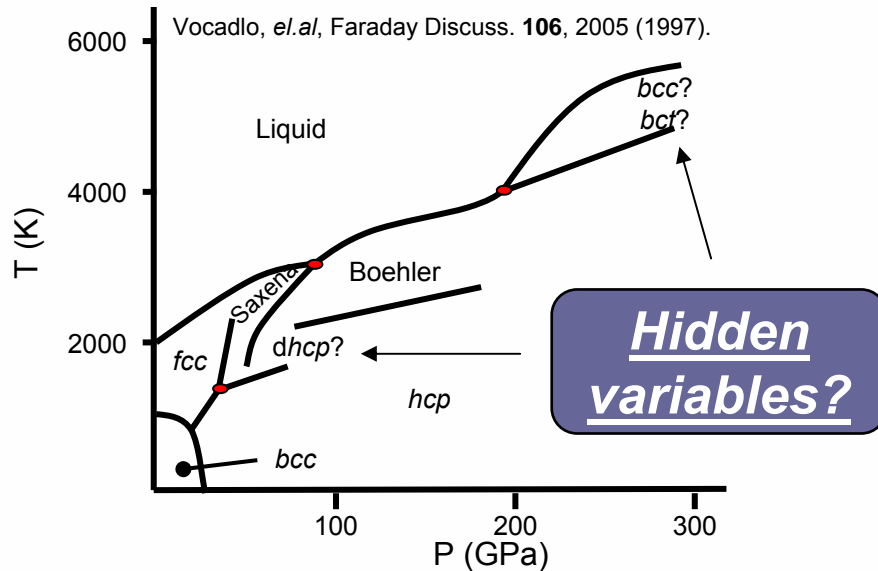
Kyle J. Caspersen and Emily Carter
Department of Chemistry and Biochemistry
University of California Los Angeles

Adrian Lew* and Michael Ortiz
Graduate School of Aeronautics
California Institute of Technology

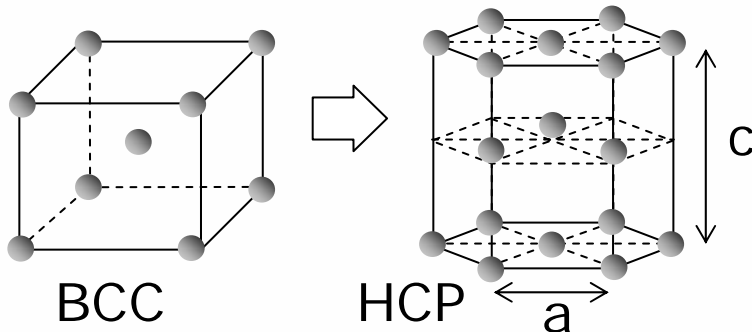
Funded by the Department of Energy - Accelerated Strategic Computing Initiative (DOE-ASCI)

*Stanford University

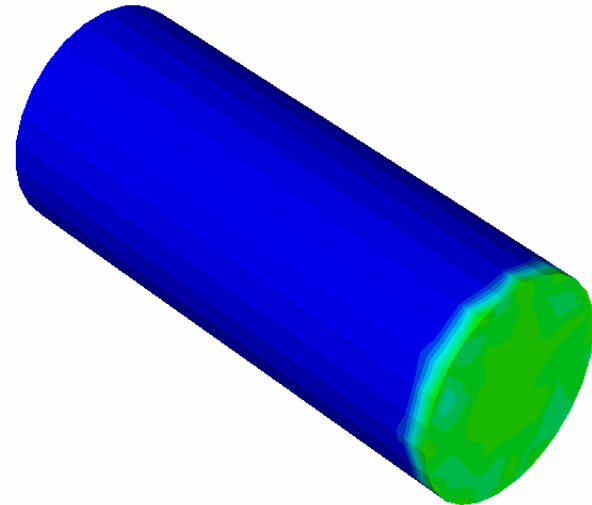
Phase transformations in iron



Ground state ferromagnetic *bcc* undergoes a *martensitic* phase transformation to non-magnetic *hcp* at ~10 GPa.



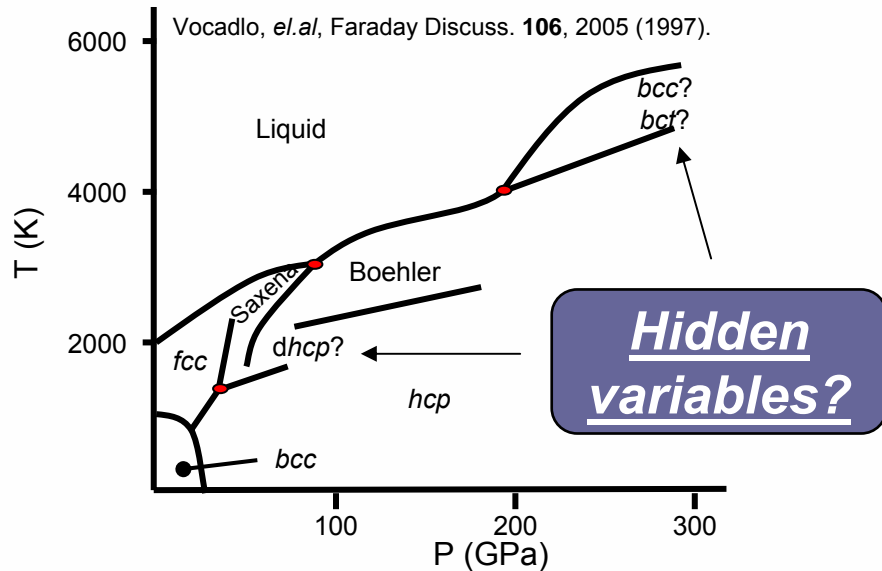
A strong shock wave will induce phase transitions producing complicated microstructure.



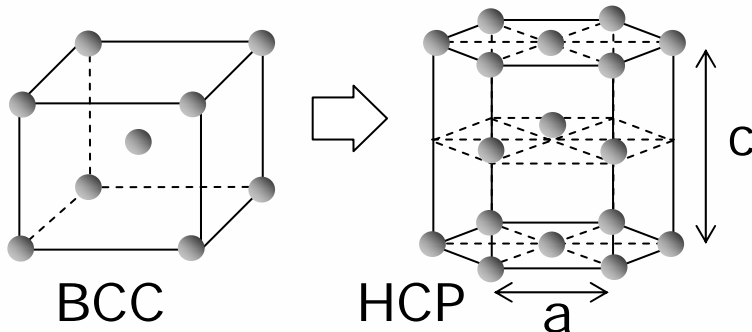
- Large scatter in the measured TP
- Fuzzy phase boundaries
- Mixed states
- Large hysteresis

Goal: understand scatter and hysteresis in transition pressures

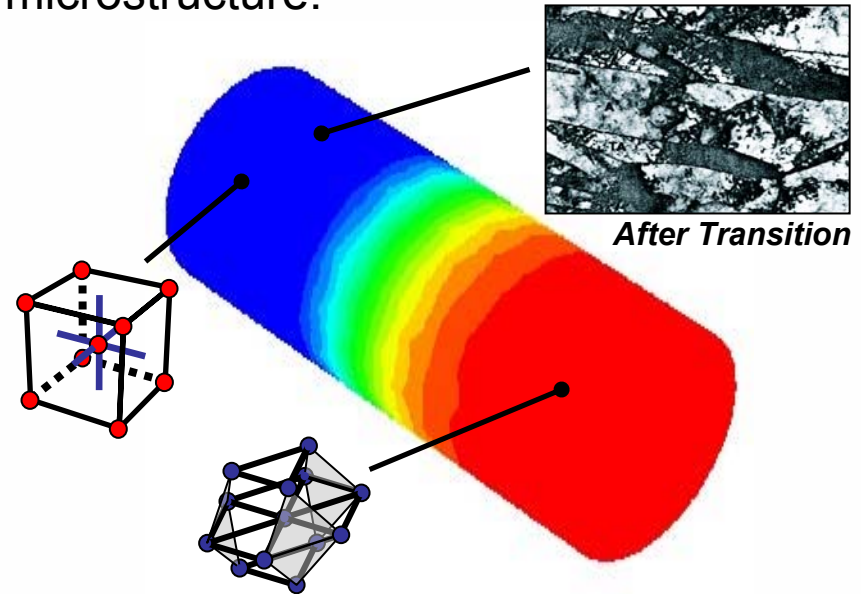
Phase transformations in iron



Ground state ferromagnetic *bcc* undergoes a *martensitic* phase transformation to non-magnetic *hcp* at ~10 GPa.



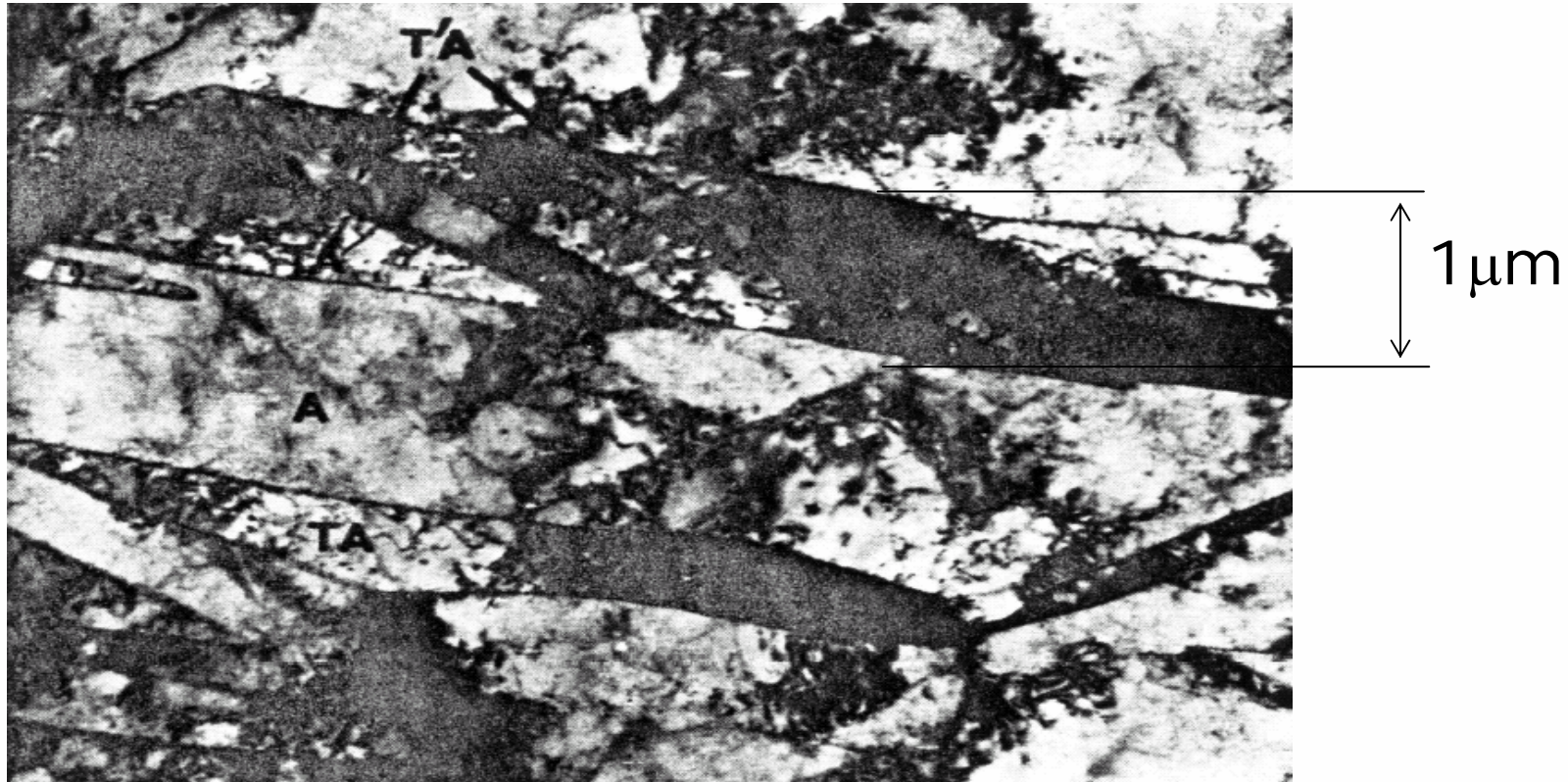
A strong shock wave will induce phase transitions producing complicated microstructure.



- Large scatter in the measured TP
- Fuzzy phase boundaries
- Mixed states
- Large hysteresis

Goal: understand scatter and hysteresis in transition pressures

Martensite in iron – length scales



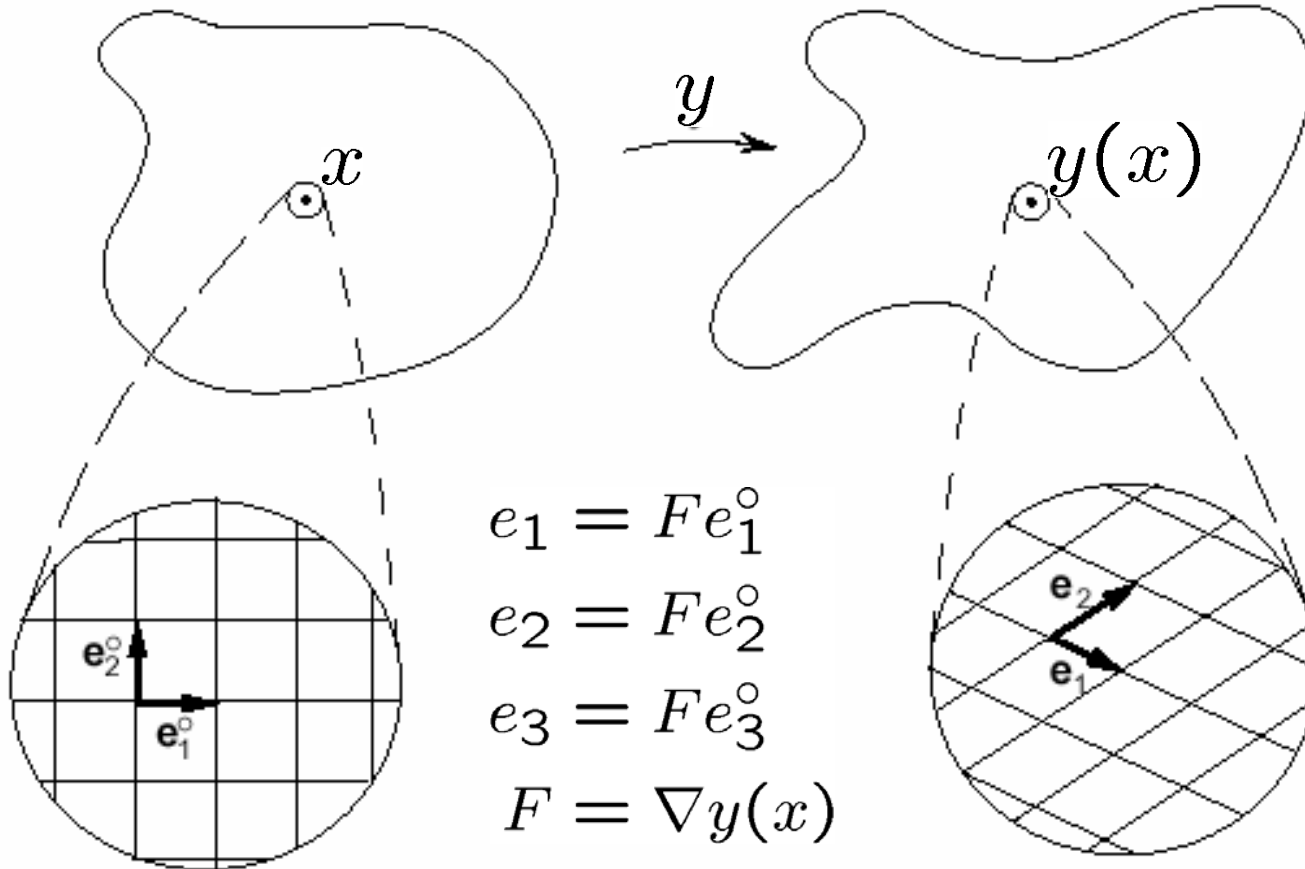
- Variants of bcc Fe produced by $\text{bcc} \rightarrow \text{hcp} \rightarrow \text{bcc}$ transformation induced by shock loading (Bowden and Kelly)
- Micron-length scales require continuum analysis!

Atomistic – continuum connexion

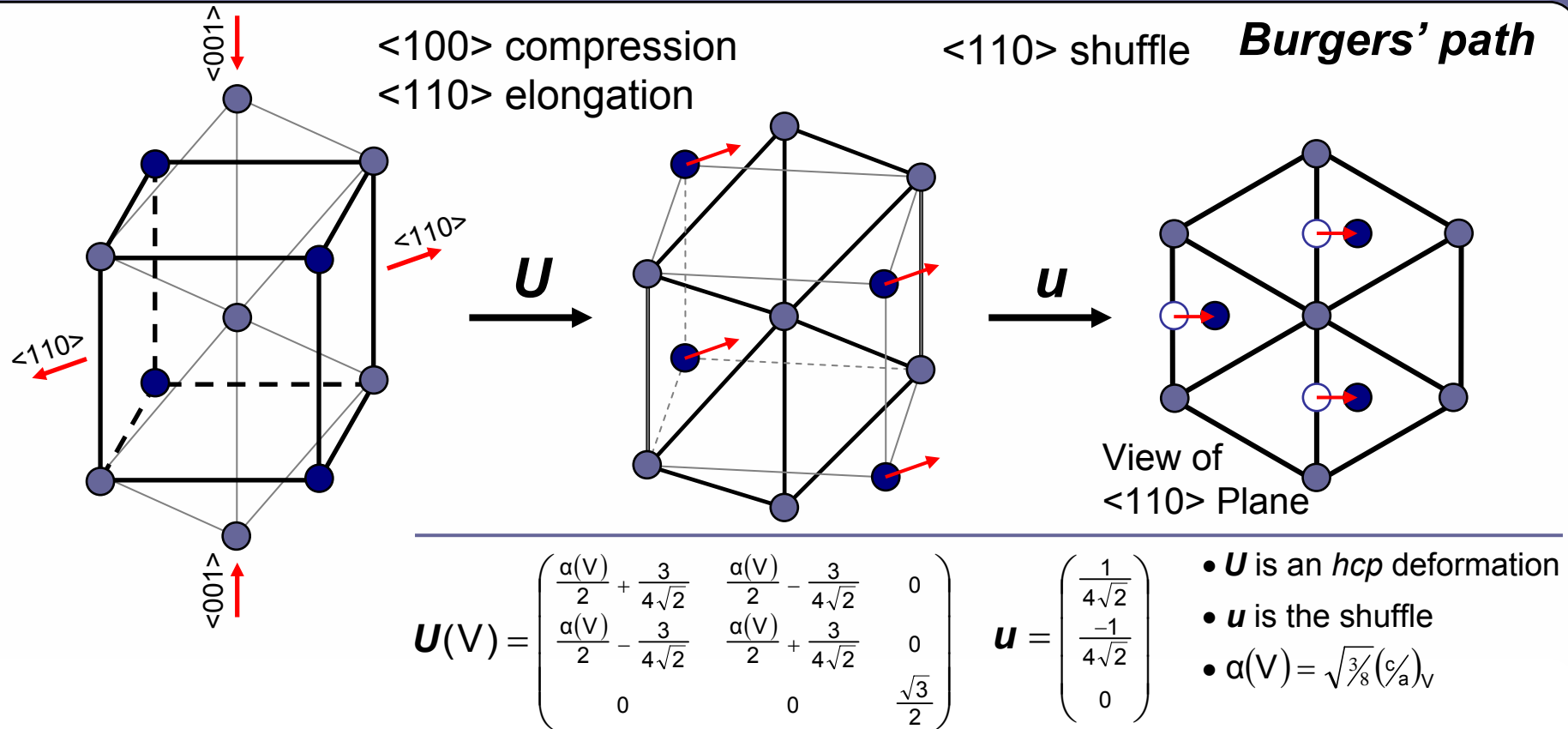
Cauchy-Born Rule

undeformed

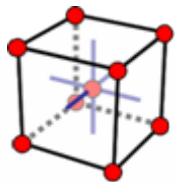
deformed



Kinematics of $bcc \rightarrow hcp \rightarrow bcc$ phase transformations

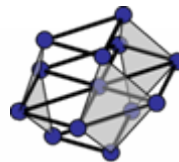


initial bcc variant



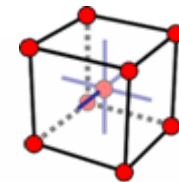
$G \in bcc$ point group

6 hcp variants



$H \in hcp$ point group

12 bcc variants



19 total variants

UG

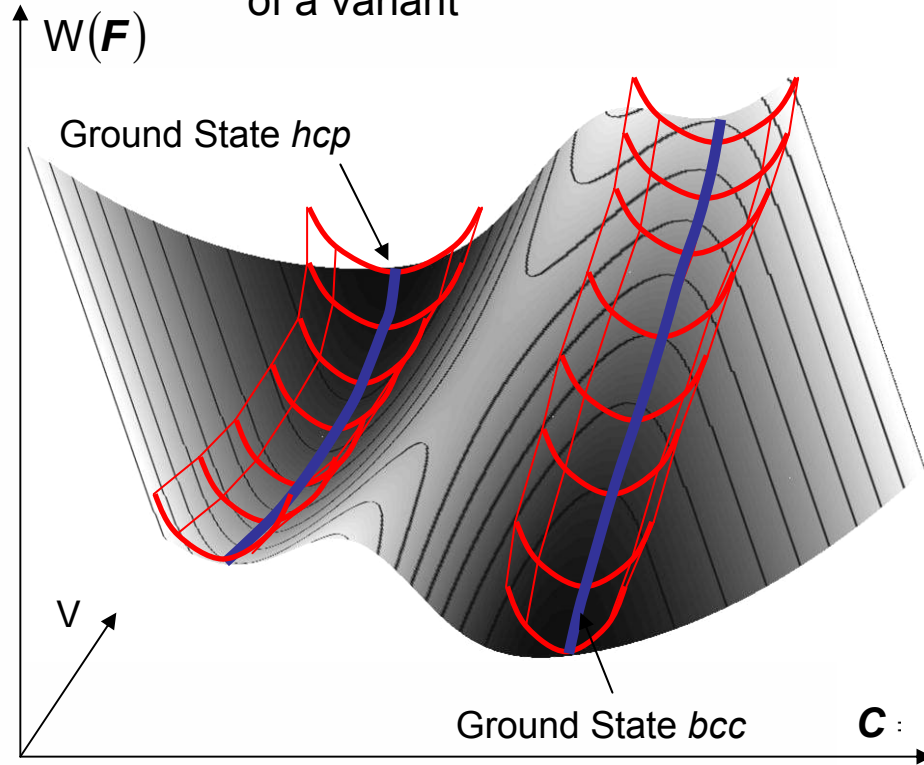
$G^{-1}U^{-1}HUG$

Multi-well elastic energy for iron

$$W(\mathbf{F}) = \min_{i=0,\dots,18} W^i(\mathbf{F})$$

DFT calculations prove to costly for on-the-fly $W(\mathbf{F})$ or tabulated $W(\mathbf{F})$

Assumption: each deformation close to deformation of a variant



Approximation: Taylor expansion around variant deformation

Taylor Expansion

$$W^i(\mathbf{C}) = W_0^i(V) + \frac{1}{2}(\mathbf{C} - \mathbf{C}^i(V))^T \boldsymbol{\Gamma}^i(V)(\mathbf{C} - \mathbf{C}^i(V))$$

$$\boldsymbol{\Gamma}^i(V) = \left. \frac{\partial^2 W^i}{\partial \mathbf{C}^2} \right|_{\mathbf{C}^i(V)} \quad \mathbf{C} = \mathbf{F}^T \mathbf{F}$$

DFT Calculations

- Variant deformation, $\mathbf{C}^i(V)$ (*hcp* *c/a* ratio)
- Equation of State, $W_0^i(V) = W^i(\mathbf{C}^i(V))$
- Non-Linear Elastic Constants, $\boldsymbol{\Gamma}(V)$
(Calculated using volume conserving shears)

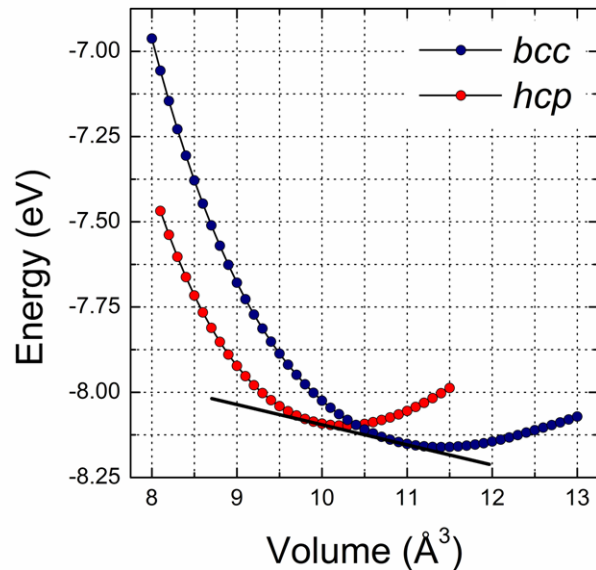
$$\text{bcc and fcc} : \Gamma_{11} \Gamma_{12} \Gamma_{44}$$

$$\text{hcp} : \Gamma_{11} \Gamma_{33} \Gamma_{12} \Gamma_{13} \Gamma_{44}$$

DFT Details

- Kohn-Sham DFT within VASP
- GGA and PW-91
- Projector Augmented Wave (PAW) all electron method
- 2 Ions/Cell
- $24 \times 24 \times 24$ Monkhorst Pack K-Point Grid
- 500 eV Kinetic Energy Cut Off
- Spin-Polarized for *bcc*

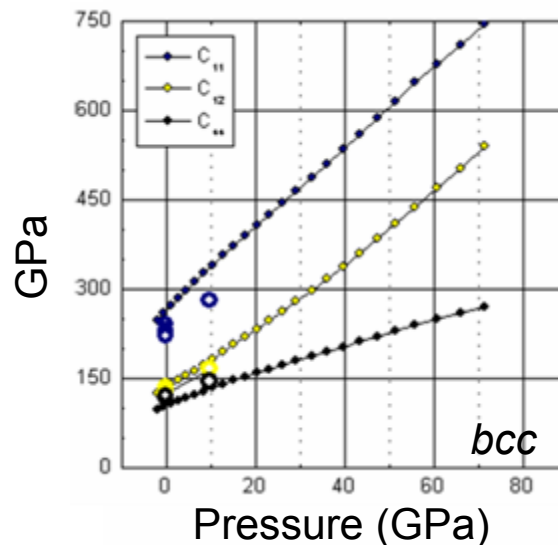
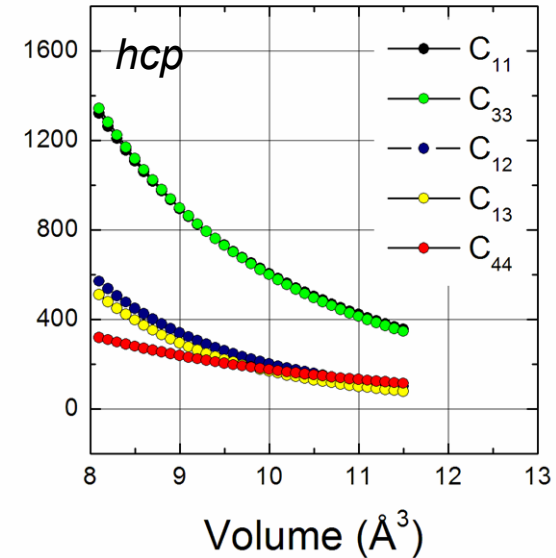
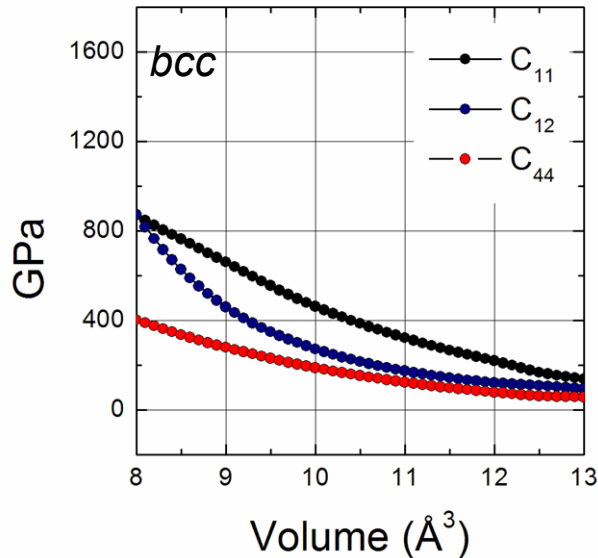
First-principles input into continuum model



<i>bcc</i> → <i>hcp</i>	Transition Pressure (GPa)
EXPERIMENT	10-15
FLAPW*	11.5
PAW	10

- PAW predicts the *bcc* to *hcp* transition pressure within the measured range

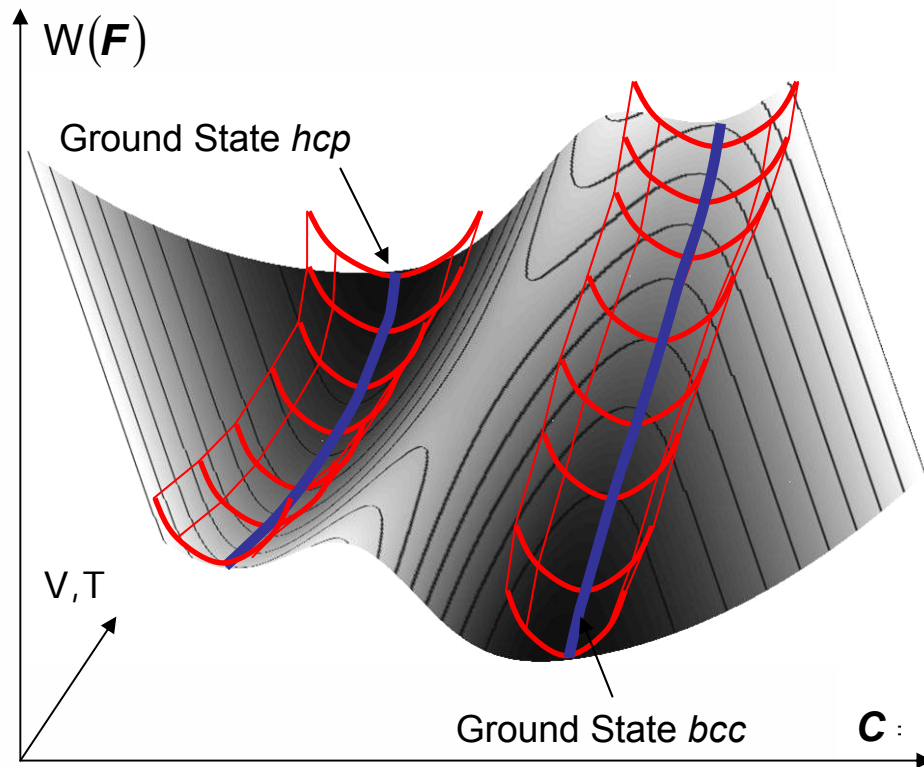
* Herper, et.al, Phys. Rev. B **60**, 3839 (1999).



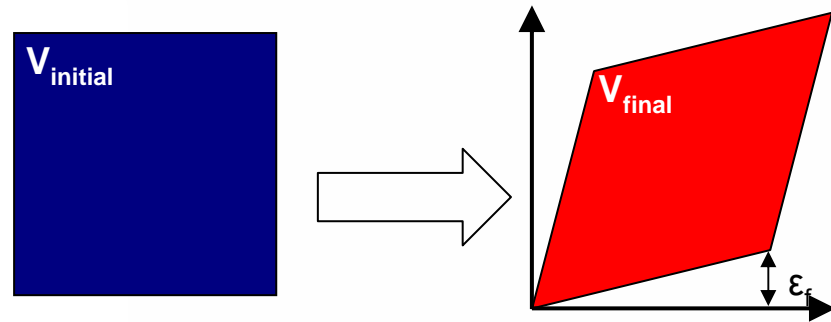
- *bcc* elastic constants compare well with experiment (C_{11} a bit high)
- little experimental data for *hcp*

Multi-well elastic energy \rightarrow phase mixing!

Multi-well free-energy density with 19 variants:



Approximation: Taylor expansion around variant deformation

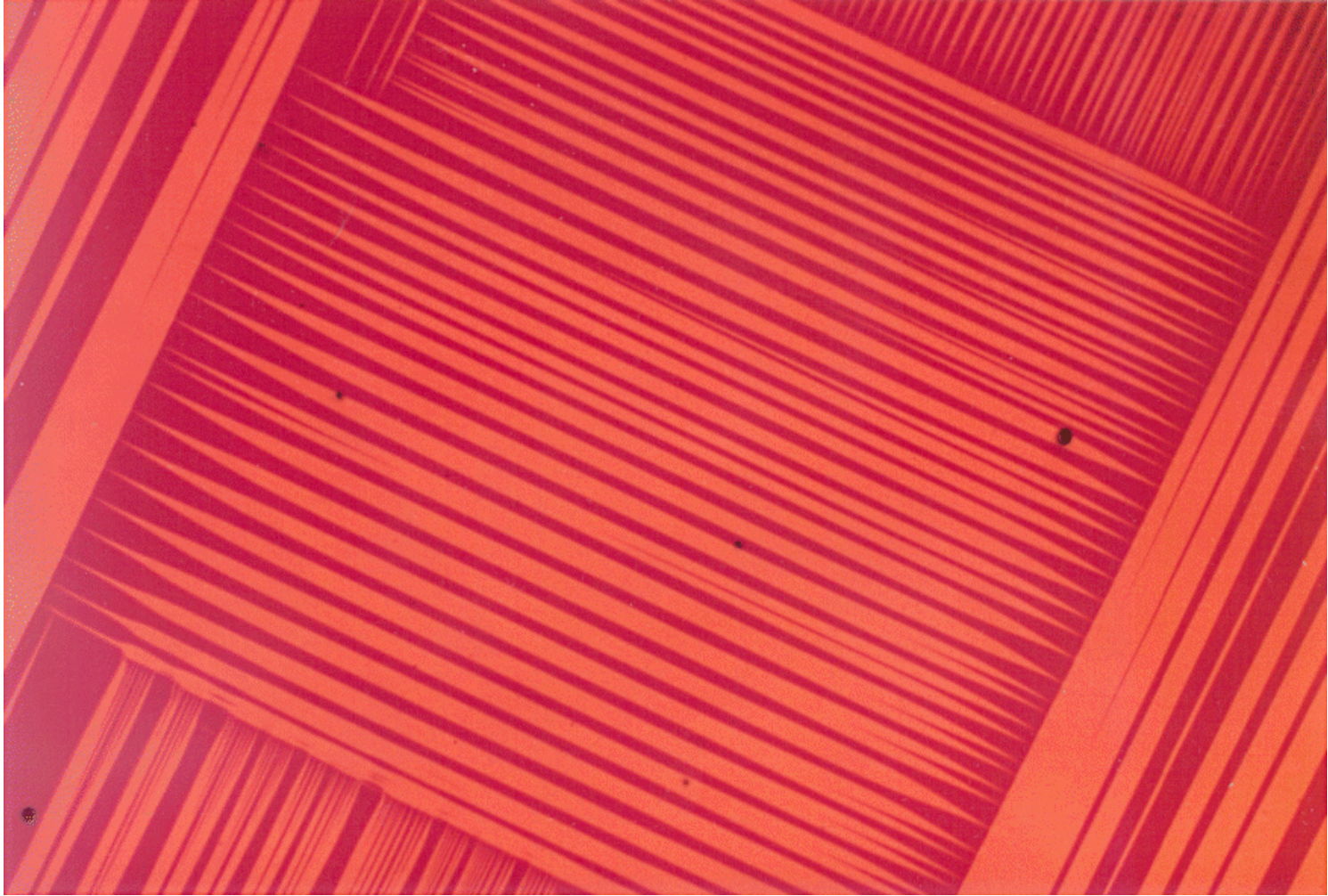


Prescribed average deformation

- Free-energy minimizers need not be uniform deformations (pure phases)
- Free energy can be reduced by mixing different phases (deformation patterning)

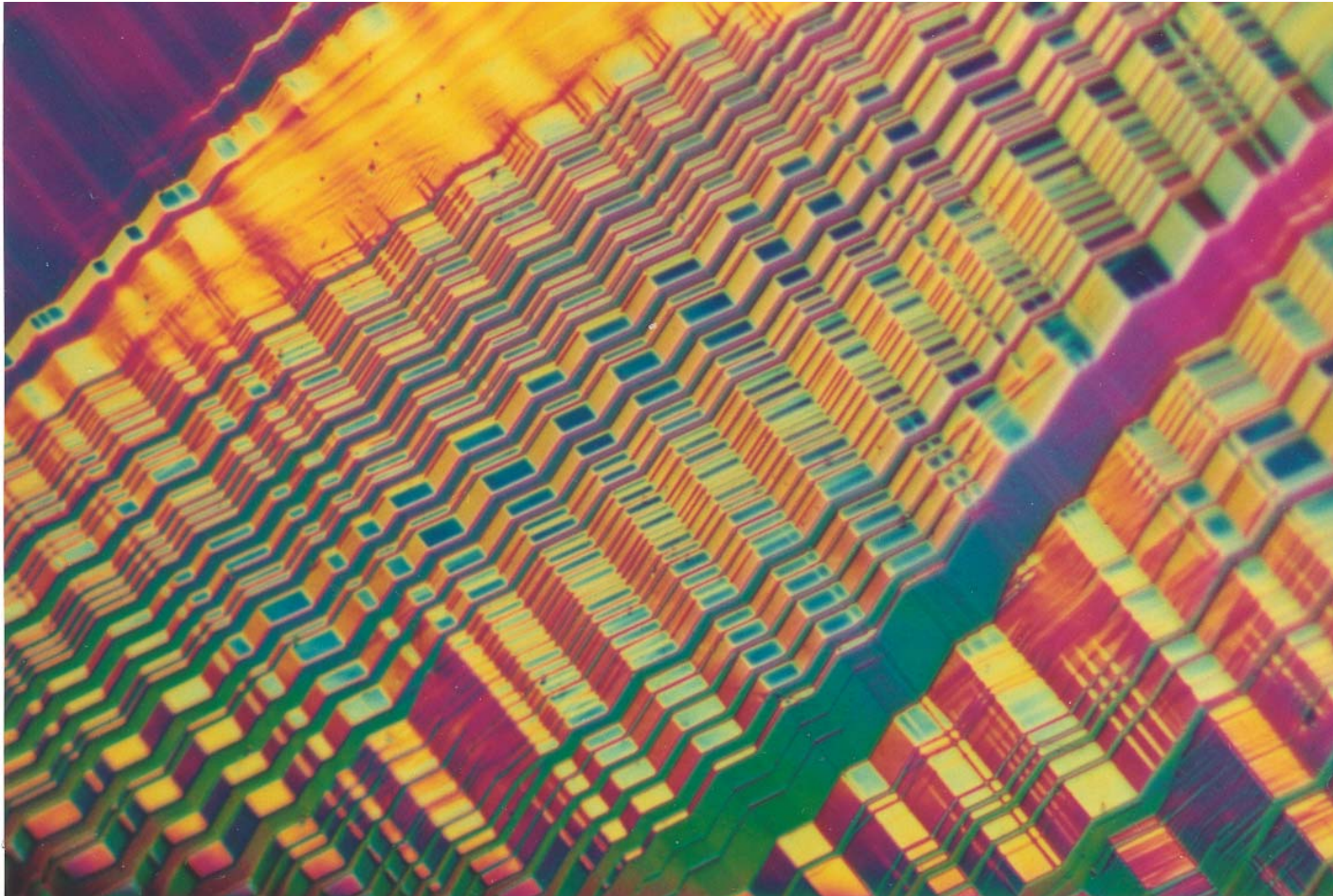
Goal: understand energy-minimizing deformation patterns (microstructures)

Microstructure of martensite



Cu-Al-Ni, Chunhua Chu and Richard D. James

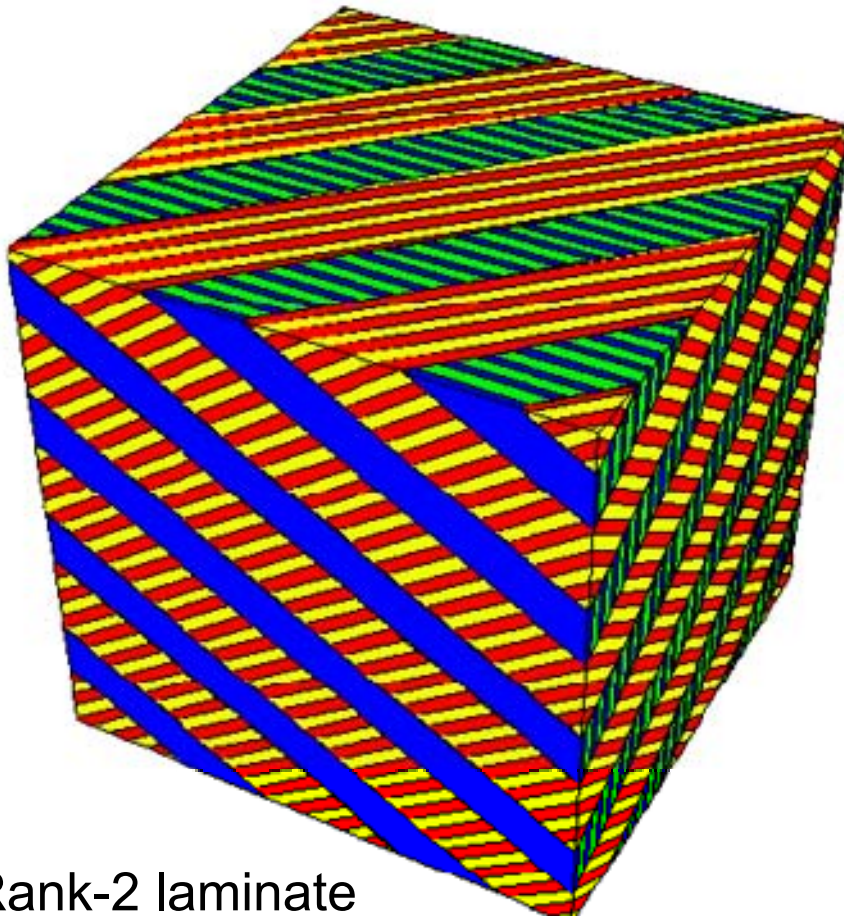
Microstructure of martensite



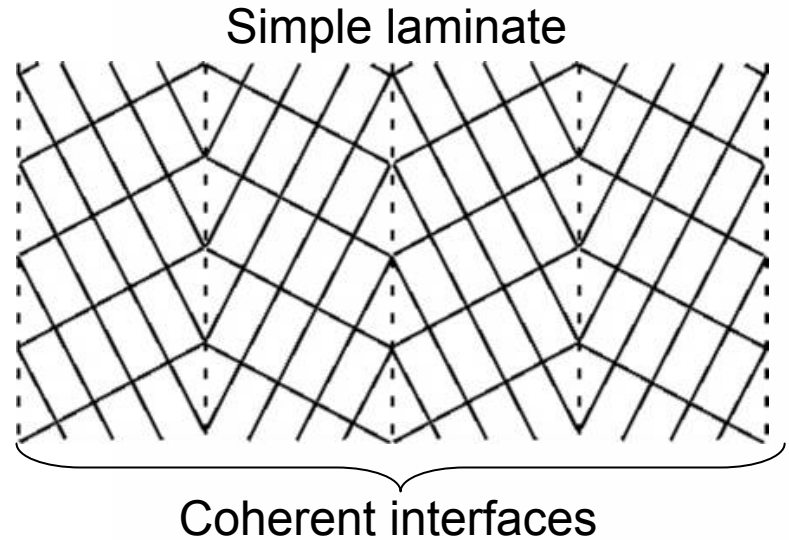
Cu-Al-Ni, Chunhua Chu and Richard D. James

Sequential laminates

Ansatz: Free-energy minimizing microstructures are sequential laminates



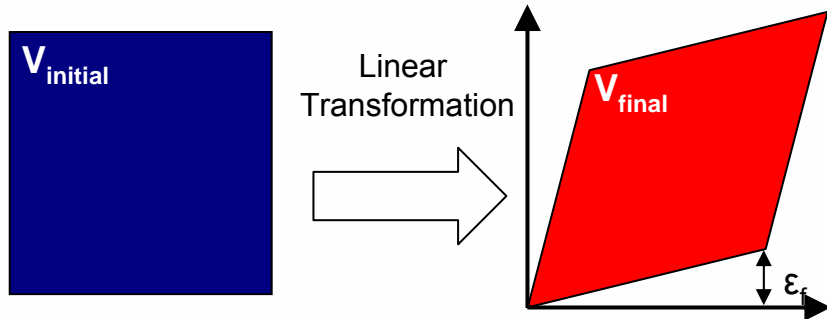
Rank-2 laminate



- Must optimize:
 - Interfacial orientations
 - Volume fractions
 - Nesting of laminates
 - Variant sizes
- Constraints:
 - Equilibrium at interfaces
 - Coherent interfaces

(Aubry, Fago and Ortiz, *CMAME*, 2003)

Shear Compression

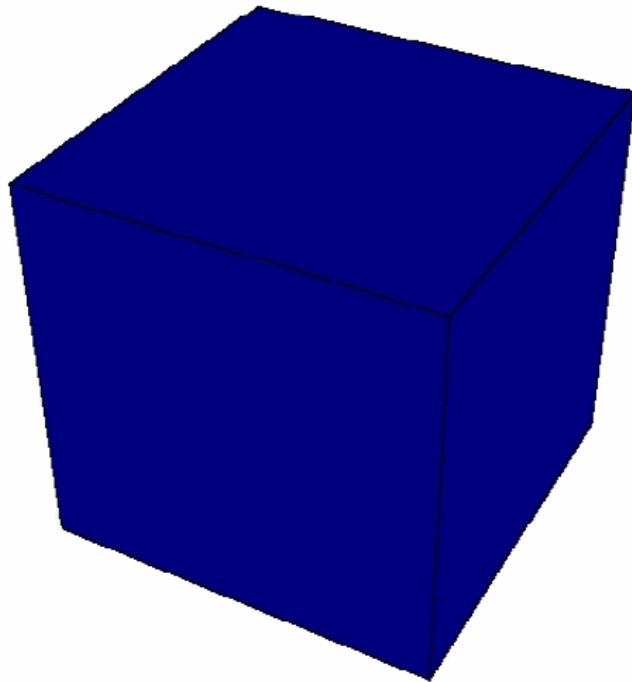


$$\mathbf{F}(\delta) = (1 - \delta) \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} + \delta \begin{pmatrix} \lambda & \epsilon_f & 0 \\ \epsilon_f & \lambda & 0 \\ 0 & 0 & \lambda \end{pmatrix}$$

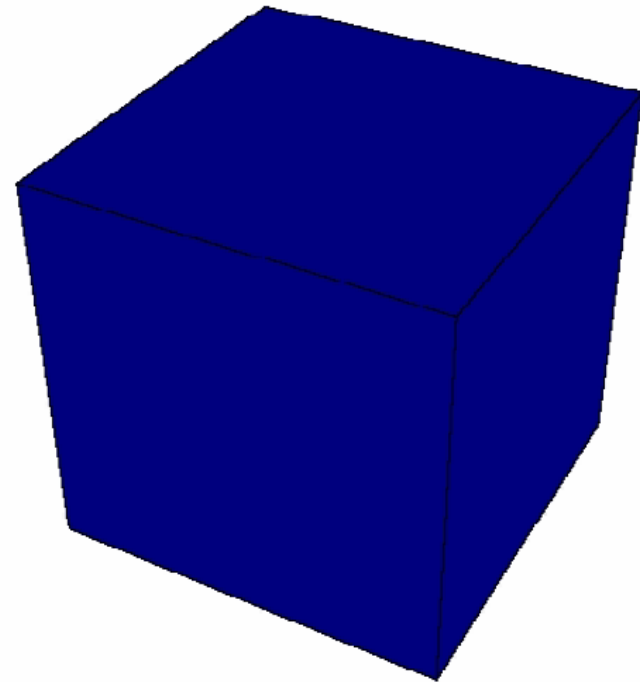
undeformed *bcc* λ is set such that $V = V_f$

(Note: $\det[\mathbf{F}] = V$)

$\epsilon_f = 0.03$

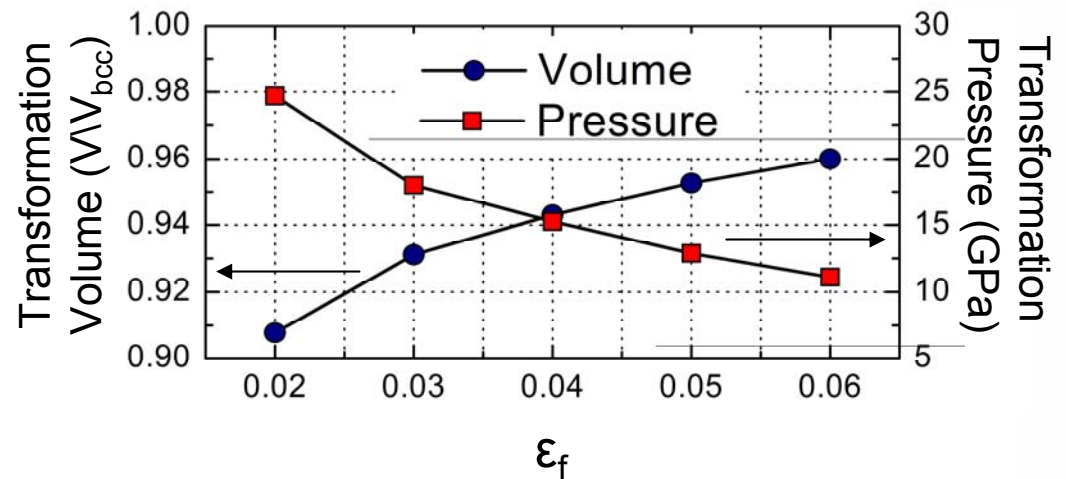
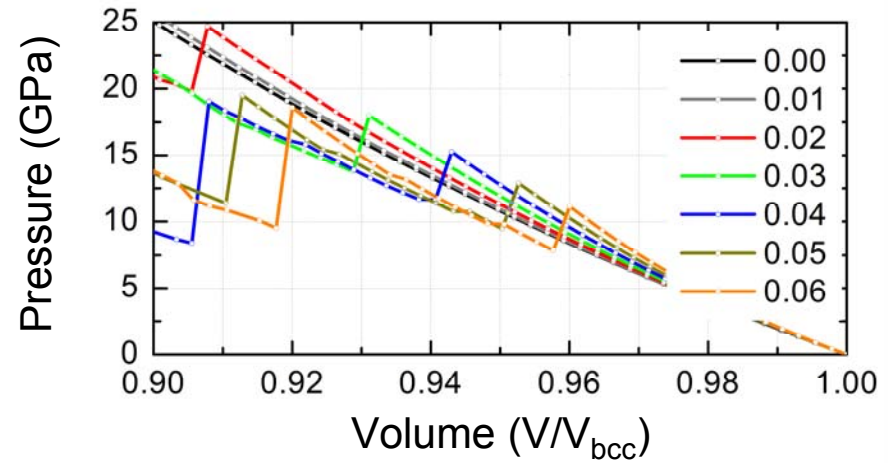
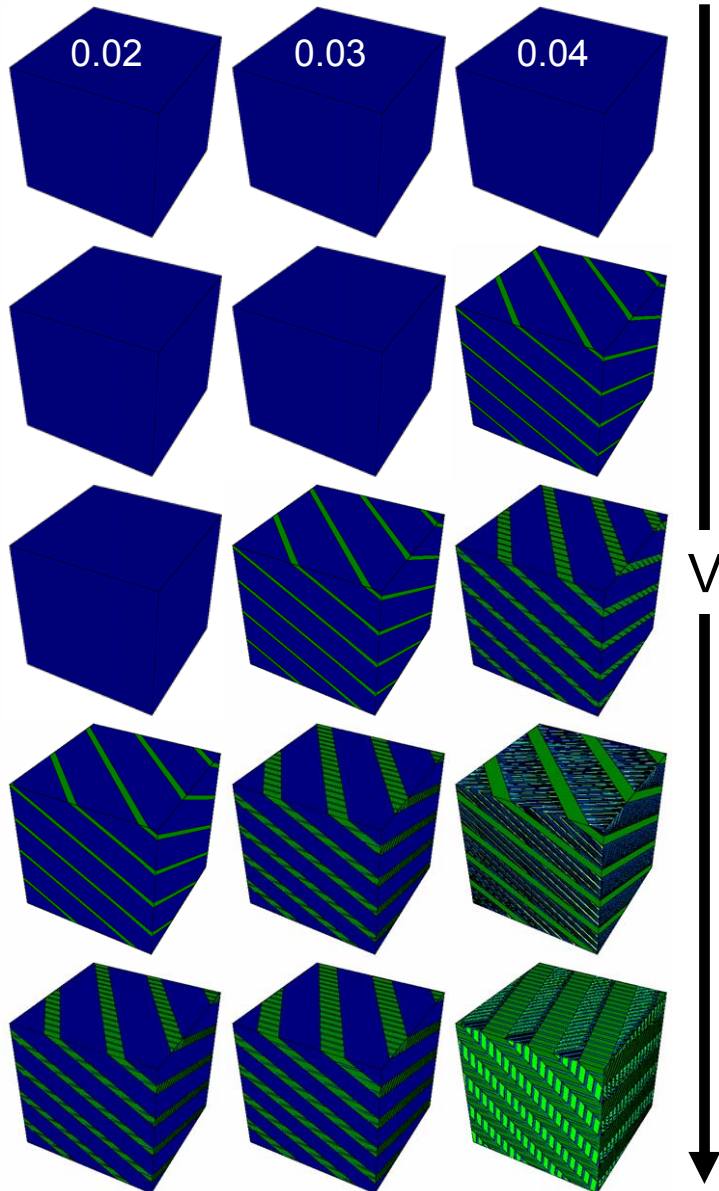


$\epsilon_f = 0.04$



Note: mapped deformed volume onto reference volume

Role of Shear

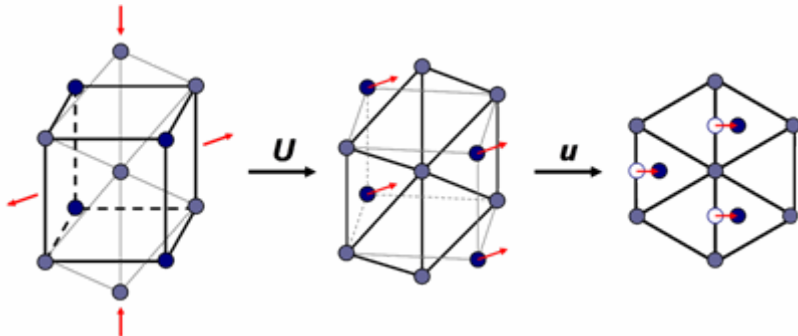


- shear is required to activate this transformation
- increasing shear lowers the TP and increases the TV
- variability in measured TPs may be due to shear states

$bcc \rightarrow hcp$ Phase Transformation

What are the average bulk properties of the $bcc \rightarrow hcp$ transformation?

To explore the transformation, we apply a series of volume-conserving deformations (F) along the transformation path.



$$U(V) = \begin{pmatrix} \frac{\alpha(V)}{2} + \frac{3}{4\sqrt{2}} & \frac{\alpha(V)}{2} - \frac{3}{4\sqrt{2}} & 0 \\ \frac{\alpha(V)}{2} - \frac{3}{4\sqrt{2}} & \frac{\alpha(V)}{2} + \frac{3}{4\sqrt{2}} & 0 \\ 0 & 0 & \frac{\sqrt{3}}{2} \end{pmatrix}$$

$$\alpha(V) = \sqrt{\frac{3}{8}} (c/a)_V$$

bcc deformation

$$F_{bcc}(V) = V^{1/3} I$$

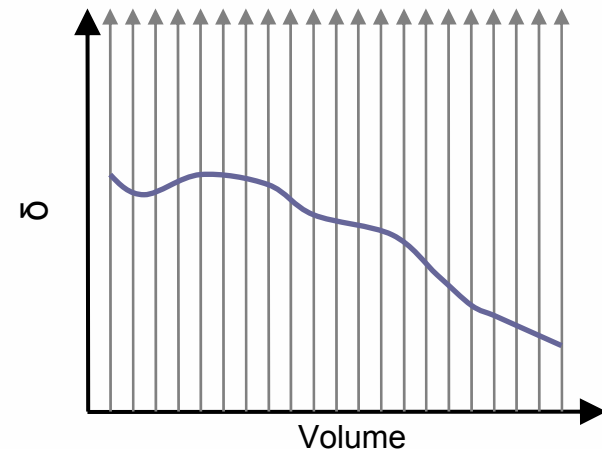
hcp deformation

$$F_{hcp}(V) = \left(\frac{V}{\det U(V)} \right)^{1/3} U(V)$$

linear transformation

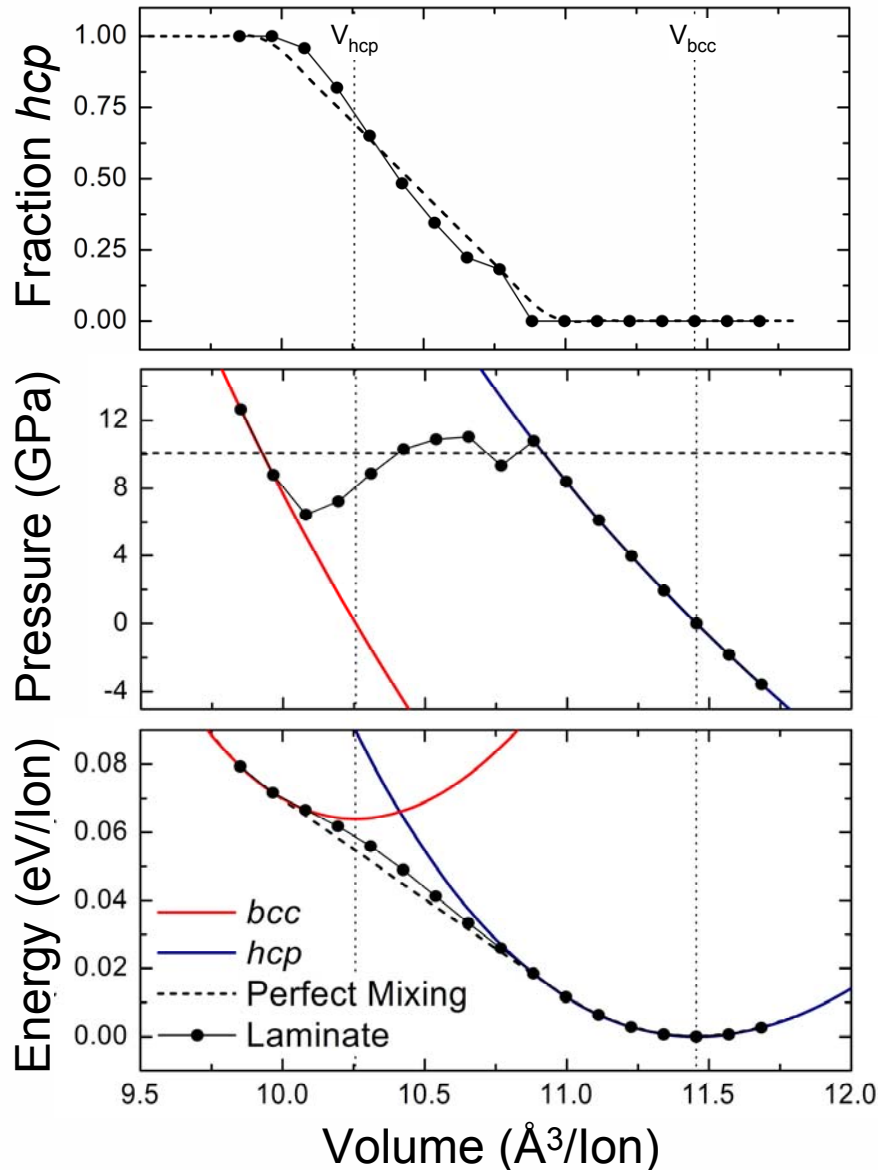
$$F(V, \delta) = \omega_{\delta} \left[(1 - \delta) F_{bcc}(V) + \delta F_{hcp}(V) \right]$$

ω = volume-conserving scale factor
 $0 \leq \delta \leq 1$



The $F(V, \delta)$ that minimizes W determines the transformation properties.

$bcc \rightarrow hcp$ Phase Transformation

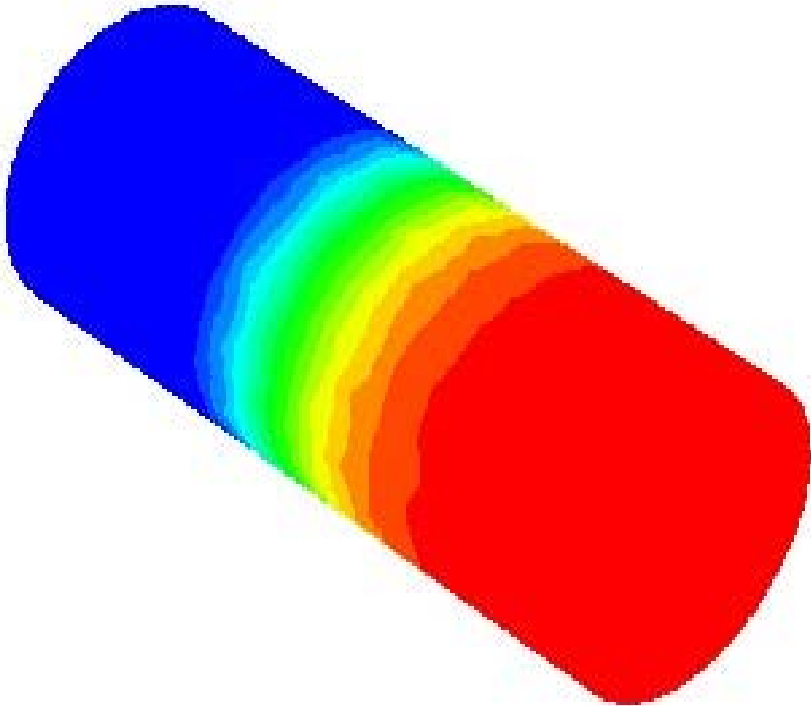


- **full conversion to hcp**
 - **transition pressure of 10 GPa**
 - **hallmarks of Gibbs construction**
 - the lowering of the energy
 - the lag to full conversion to hcp
 - **deviation from Gibbs construction**
 - no perfect tangent matching
 - energy is increased
 - caused by the two imposed constraints
 - Hadamard compatibility condition

$$\mathbf{F}_1 - \mathbf{F}_2 = \mathbf{a} \otimes \mathbf{n}$$
 - dependence on the transformation path
- The diagram illustrates the transformation of a body-centered cubic (bcc) unit cell into a hexagonal close-packed (hcp) unit cell through a shear deformation u . The first structure is a bcc cell with a central atom and eight corner atoms. The second structure is an intermediate state where the atoms are shifted by a vector u . The final structure is an hcp cell with a different arrangement of atoms. Red arrows indicate the direction of the shear deformation.
- constraints introduce frustration
 - **hysteresis width of ≈ 5.2 GPa observed**
 - loading TP = 10.2 GPa
 - unloading TP = 5.0 GPa
 - experimental width 6.2 GPa (Taylor et al.)

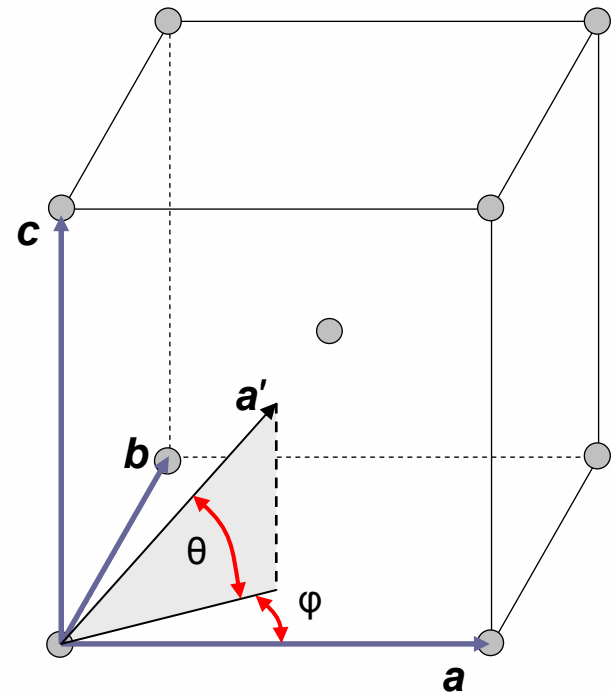
Directional Deformation of bcc Fe

- propagating shock waves apply load in specific directions



- what effect does the direction of applied load have on the transformation?

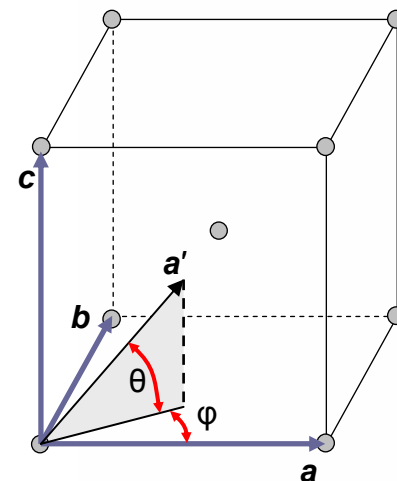
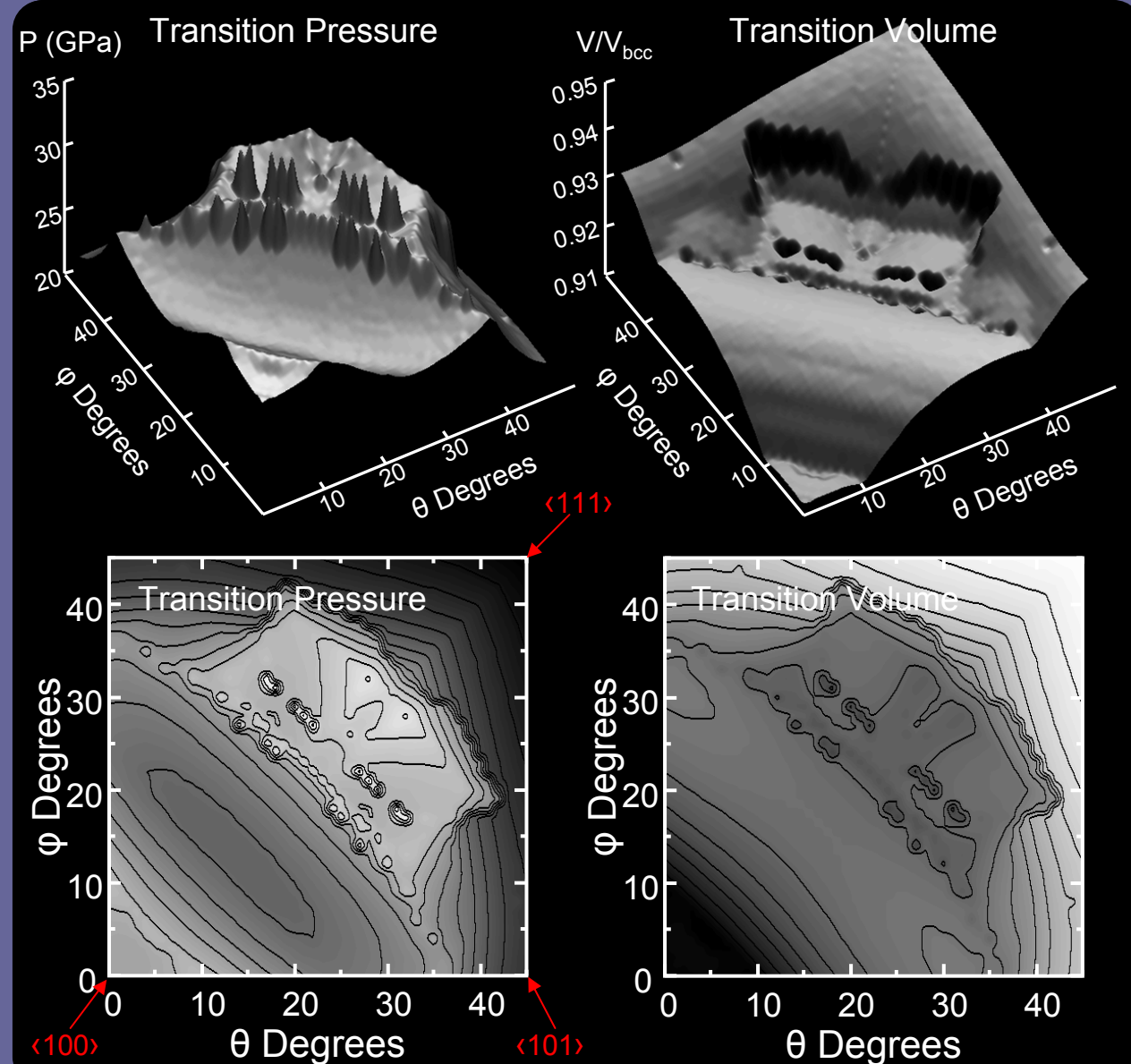
to investigate directional loading we applied directional deformation $\mathbf{F}_{\theta,\varphi}(\delta)$ spanning direction space (angle space)



$$(\mathbf{a}', \mathbf{b}', \mathbf{c}') = \begin{pmatrix} \cos\varphi & \sin\varphi & 0 \\ -\sin\varphi & \cos\varphi & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \cos\theta & 0 & \sin\theta \\ 0 & 1 & 0 \\ -\sin\theta & 0 & \cos\theta \end{pmatrix}$$

$$\mathbf{F}_{\theta,\varphi}(\delta) = \delta(\mathbf{a}' \otimes \mathbf{a}') + (\mathbf{b}' \otimes \mathbf{b}') + (\mathbf{c}' \otimes \mathbf{c}')$$

Directional Deformation of bcc Fe: TP and TV



TP for all angles is high, >20 GPa

- never optimal combination of contraction and and shear

region of high pressure for moderate angles

- perhaps no hcp variant along path

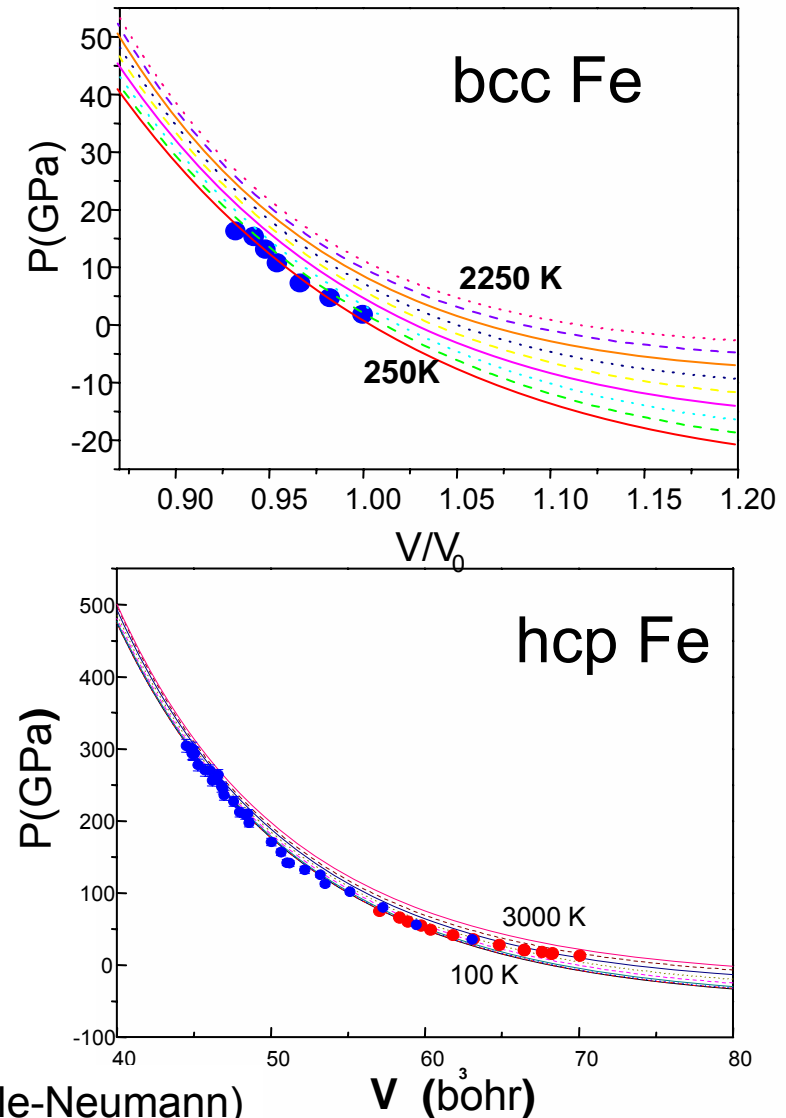
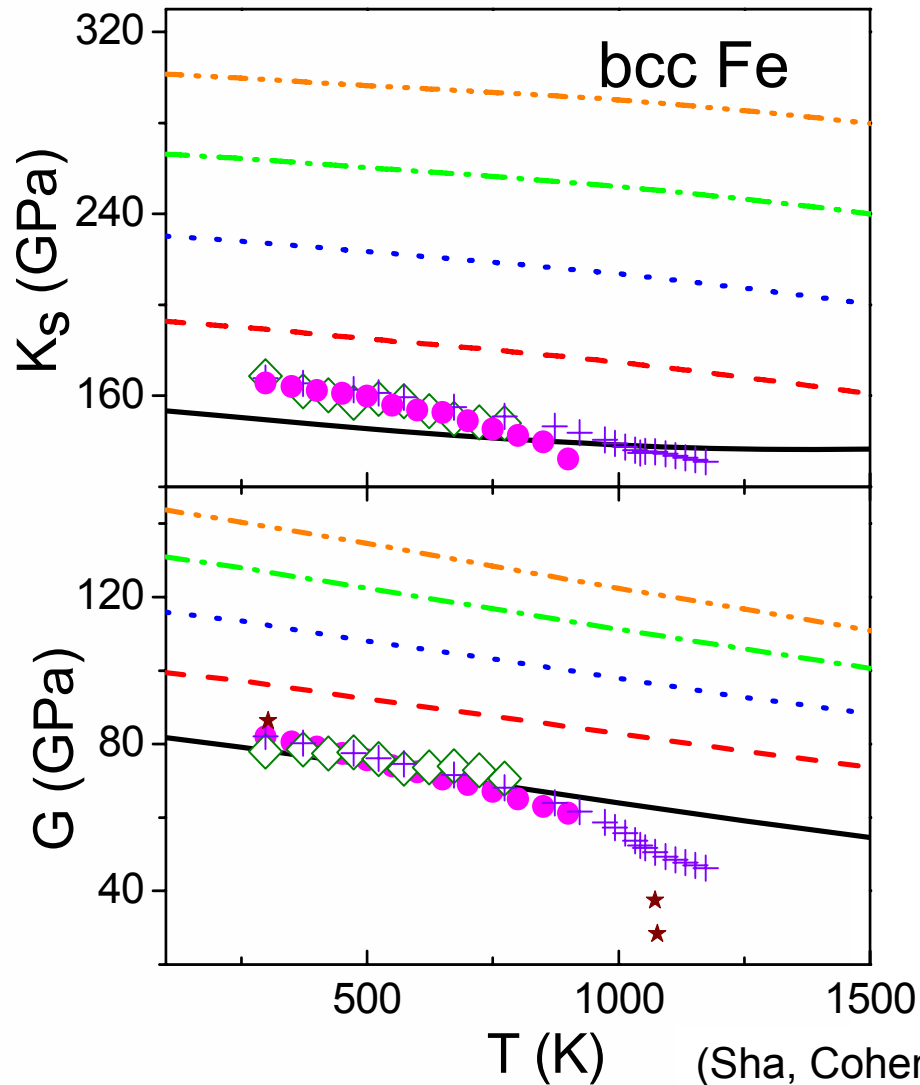
loading parallel to simple facets facilitates the transformation

- notably the $\langle 110 \rangle$ planes

loading along the simple axes recovers smallest TP in that region of angle space

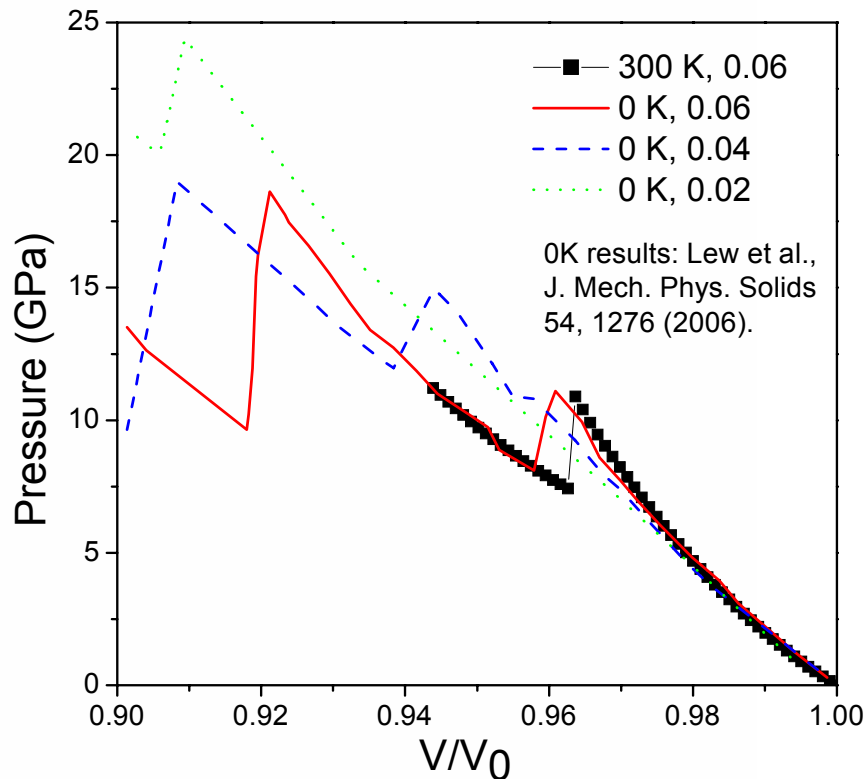
- $\langle 111 \rangle < \langle 101 \rangle < \langle 100 \rangle$

First-principles input at finite temperature



Effect of temperature and plasticity

The pressure/volume properties of Fe subject to external strain at room temperature



(Sha, Cohen, Steinle-Neumann)

Preliminary results show that the temperature effects are not very significant, but still the phase transformation tends to occur at lower pressures at room temperature than at zero temperature.

Plasticity also generates lamintes:

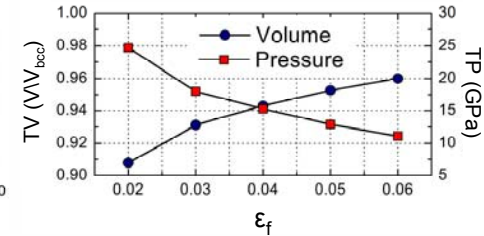
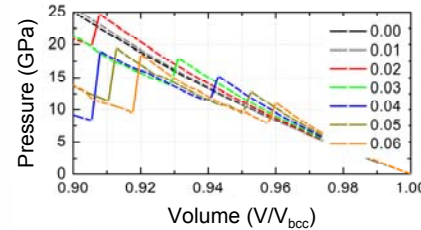


Shocked Ta (Meyers et al., 1995)

Conclusions

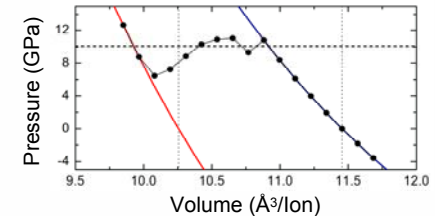
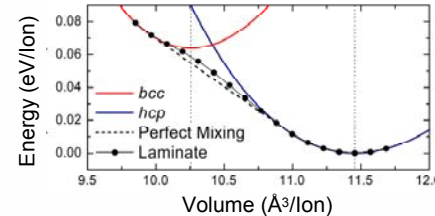
Shear Compression

- shear is required for transformation to occur
- increasing shear lowers the TP and increases the TV
- sensitivity to shear may be responsible for the variability in the measured TPs

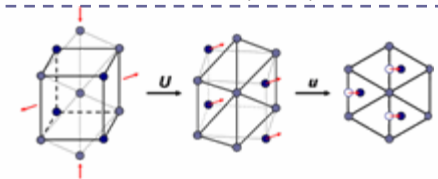


bcc-to-hcp Transformation

- full conversion to *hcp* at ≈ 10 GPa, consistent with the experimentally observed values
- hallmarks of the Gibbs construction
- deviation from “perfect” mixing due to imposed constraints
- shows hysteresis in the TP simply due to the crystalline kinematics

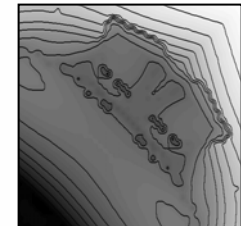
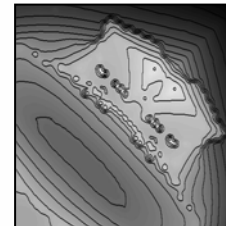


$$\mathbf{F}_1 - \mathbf{F}_2 = \mathbf{a} \otimes \mathbf{n}$$



Directional Deformation

- transformation pressure is > 20 GPa
- region of very high transformation pressure
- loading || to simple facets facilitates the transformation, in particular along simple axes



Acknowledgements

Matt Fago :S. Aubry, M. Fago, and M. Ortiz, Computer Methods in Applied Mechanics and Engineering **192**, 2823 (2003).
De-en Jiang Robin Hayes Emily Jarvis , Sha, Cohen, Steinle-Neumann