

# Lecture 3

## Applications of the 1st and 2nd laws

Main message:

$$Tds = du + pdv$$

$$\begin{aligned} du &= Tds - pdv \\ &= Tds + \sum_i J_i dx_i \end{aligned}$$

- main equation in thermodynamics that we need to remember. By manipulating this, can get any thermodynamic identity that we want.

1) Dependence of U on V - relate to equation of state  $P = P(T, V)$

$$Tds = du + pdv = \left(\frac{\partial u}{\partial T}\right)_v dT + \left(\left(\frac{\partial u}{\partial v}\right)_T + p\right) dv$$

$$ds = \underbrace{\frac{1}{T} c_v dT}_{\left(\frac{\partial s}{\partial T}\right)_v} + \underbrace{\frac{1}{T} \left(\left(\frac{\partial u}{\partial v}\right)_T + p\right) dv}_{\left(\frac{\partial s}{\partial v}\right)_T}$$

$$S = S(T, V) \quad \left(\frac{\partial s}{\partial T}\right)_v \quad \left(\frac{\partial s}{\partial v}\right)_T$$

$$\left(\frac{\partial s}{\partial T}\right)_v = \frac{1}{T} \left(\frac{\partial u}{\partial T}\right)_v \Rightarrow \frac{\partial^2 s}{\partial T \partial T} = \frac{1}{T} \frac{\partial^2 u}{\partial T \partial T}$$

$$\left(\frac{\partial s}{\partial v}\right)_T = \frac{1}{T} \left(\left(\frac{\partial u}{\partial v}\right)_T + p\right) \Rightarrow \frac{\partial^2 s}{\partial T \partial v} = -\frac{1}{T^2} \left(\left(\frac{\partial u}{\partial v}\right)_T + p\right)$$

$$+ \frac{1}{T} \left(\frac{\partial^2 u}{\partial T \partial v} + \left(\frac{\partial p}{\partial T}\right)_v\right)$$

$$\Rightarrow \boxed{\left(\frac{\partial u}{\partial v}\right)_T = T \left(\frac{\partial p}{\partial T}\right)_v - p}$$

Example: Ideal gas  $p = \frac{NkT}{V} \Rightarrow \left(\frac{\partial u}{\partial v}\right)_T = 0$

(Actually used Joule's free expansion experiment  $\Rightarrow \left(\frac{\partial u}{\partial v}\right)_T = 0$   
- to identify thermodynamic & ideal gas temperature!)

so this is  
only  
consistency  
check

(enthalpy)

1') Similarly, dependence of H on p

$$H = U + pV$$

$$TdS = dU + pdV = dH - Vdp$$

$$S = S(T, p)$$

$$H = H(T, p)$$

identical manipulations

$$\Rightarrow \left( \frac{\partial H}{\partial p} \right)_T = -T \left( \frac{\partial V}{\partial T} \right)_p + V$$

; For ideal gas,

$$\left( \frac{\partial H}{\partial p} \right)_T = 0 \quad (H = U(T) + NKT)$$

$$TdS = \left( \frac{\partial H}{\partial T} \right)_p dT + \left[ \left( \frac{\partial H}{\partial p} \right)_T - V \right] dp =$$

$$= c_p dT - T \left( \frac{\partial V}{\partial T} \right)_p dp$$

Summary:

1) and 1')

$$TdS = c_v dT + T \left( \frac{\partial p}{\partial T} \right)_v dV$$

$$TdS = c_p dT - T \left( \frac{\partial V}{\partial T} \right)_p dp$$

- will use in the discussion of response properties

= slightly different derivation of  $\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial p}{\partial T} \right)_v$ :

$$F = U - TS$$

$$dF = -SdT - pdV \Rightarrow -S = \left( \frac{\partial F}{\partial T} \right)_v$$

$$-p = \left( \frac{\partial F}{\partial V} \right)_T$$

"Maxwell relation"

$$\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial p}{\partial T} \right)_v$$

More generally  $dF = -SdT + \sum J_i dx_i$

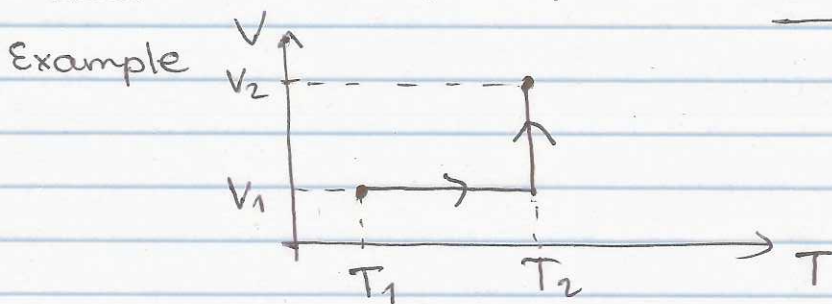
$$\left( \frac{\partial S}{\partial x_i} \right)_{T, x_{j \neq i}} = - \left( \frac{\partial J_i}{\partial T} \right)_{x_j}$$

scales, so this is only consistency check).

## 2) Experimental determination of $U, S$ from equation of state and $c_v$

Energy  $U = U(V, T)$

$$dU = c_v dT + \left( \frac{\partial U}{\partial V} \right)_T dV = c_v dT + \left( T \left( \frac{\partial P}{\partial T} \right)_V - P \right) dV$$



$$U_2 - U_1 = \int_{V_1, T_1}^{V_2, T_2} c_v(V_1, T) dT + \int_{V_1, T_2}^{V_2, T_2} \left( T_2 \left( \frac{\partial P}{\partial T} \right)_V - P \right) \Big|_{(V_1, T_2)} dV$$

Entropy  $S = S(V, T)$

$$T ds = \cancel{du} + p dV = c_v dT + T \left( \frac{\partial P}{\partial T} \right)_V dV$$

$$ds = \frac{c_v}{T} dT + \left( \frac{\partial P}{\partial T} \right)_V dV$$

$$S_2 - S_1 = \int_{V_1, T_1}^{V_2, T_2} \frac{c_v(V_1, T)}{T} dT + \int_{V_1, T_2}^{V_2, T_2} \left( \frac{\partial P}{\partial T} \right)_V (V, T_2) dV$$

⇒ all thermodynamics can be determined from  $c_v$  and equation of state

Example: Ideal gas:  $c_v = \frac{3}{2} NR$ ,  $pV = NRT$

$$U_2 - U_1 = \frac{3}{2} NR(T_2 - T_1) \Rightarrow U(V, T, N) = \frac{3}{2} NRT + \text{const}$$

$$S(V_2, T_2) - S(V_1, T_1) = \frac{3}{2} NR \ln \frac{T_2}{T_1} + NR \ln \frac{V_2}{V_1} \Rightarrow S(V, T, N) = NR \left[ \frac{3}{2} \ln T + \ln V + \text{const} \right]$$

For U & S to be extensive, we must have  $\text{const} \propto N$   
 $\text{const}' = \sigma - \ln N$

(~~to have~~ to have  $\ln \frac{V}{N} = \ln \frac{1}{\rho}$  - intensive quantity)

stat mech  $\Rightarrow \nu=0$ ,  $\sigma = \frac{3}{2} \ln \frac{2\pi mk}{h^2} + \frac{5}{2}$

### 3) Dependence of $C_V$ on $V$

$$dS = \underbrace{\frac{C_V}{T} dT}_{\left(\frac{\partial S}{\partial T}\right)_V} + \underbrace{\left(\frac{\partial P}{\partial T}\right)_V dV}_{\left(\frac{\partial S}{\partial V}\right)_T}$$

$$C_V = T \left(\frac{\partial S}{\partial T}\right)_V$$

$$\left(\frac{\partial C_V}{\partial V}\right)_T = \cancel{\left(\frac{\partial S}{\partial V}\right)_T} T \frac{\partial^2 S}{\partial V \partial T} = T \left(\frac{\partial^2 P}{\partial T^2}\right)_V$$

$$C_V(V, T) - C_V(V_0, T) = T \int_{V_0, T}^{V, T} \left(\frac{\partial^2 P}{\partial T^2}\right)_V (V', T) dV'$$

$\Rightarrow$  can calculate  $C_V(V, T)$  from  $C_V(V_0, T)$  and equation of state

All thermodynamics can be determined from  $C_V(V_0, T)$  and equation of state

~~Example: ideal gas  $C_V = \frac{3}{2} N k_B$~~

Example: ideal gas  $C_V = \frac{3}{2} N k_B$  - indep. of volume

- consistent with equation of state  $\Rightarrow \frac{\partial^2 P}{\partial T^2} = 0$ .

If this were not true, we could construct an engine that would violate the second law!

## Response functions

$$c_v \equiv \left( \frac{\partial U}{\partial T} \right)_v$$

$$dq = dU + pdV \stackrel{dp=0}{=} \left( \frac{\partial U}{\partial T} \right)_p dT + p \left( \frac{\partial V}{\partial T} \right)_p dT$$

$$c_p \equiv \left( \frac{\partial U}{\partial T} \right)_p + p \left( \frac{\partial V}{\partial T} \right)_p = \left( \frac{\partial H}{\partial T} \right)_p = T \left( \frac{\partial S}{\partial T} \right)_p$$

$$\alpha_p \equiv \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_p$$

- thermal expansion coefficient at constant  $p$

$$\alpha_T \equiv -\frac{1}{V} \left( \frac{\partial V}{\partial p} \right)_T$$

- isothermal compressibility

$$\alpha_s \equiv -\frac{1}{V} \left( \frac{\partial V}{\partial p} \right)_s$$

- adiabatic compressibility

Only 3 of the response functions are independent

Lemma: For any variables  $x, y, z$  constrained by  $f(x, y, z) = 0$

$x(y, z);$   
 $y(x, z);$   
 $z(x, y)$

$$\left( \frac{\partial x}{\partial y} \right)_z \left( \frac{\partial y}{\partial z} \right)_x \left( \frac{\partial z}{\partial x} \right)_y = -1$$

$$\left( \frac{\partial x}{\partial y} \right)_z = \frac{1}{\left( \frac{\partial y}{\partial x} \right)_z}$$

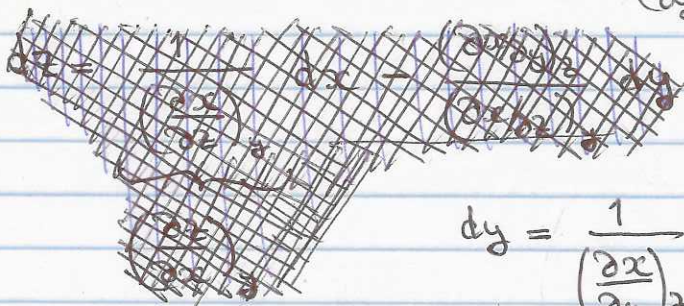
reciprocity theorem

mathematical result that allows faster manipulations of therm. quantities (no physical content)

Proof

$$x = x(y, z)$$

$$dx = \left( \frac{\partial x}{\partial y} \right)_z dy + \left( \frac{\partial x}{\partial z} \right)_y dz$$



$$dy = \frac{1}{\left( \frac{\partial x}{\partial y} \right)_z} dx - \frac{\left( \frac{\partial x}{\partial z} \right)_y}{\left( \frac{\partial x}{\partial y} \right)_z} dz$$

$$\left( \frac{\partial x}{\partial y} \right)_z \left( \frac{\partial y}{\partial z} \right)_x = - \left( \frac{\partial x}{\partial z} \right)_y = - \frac{1}{\left( \frac{\partial z}{\partial x} \right)_y}$$

! not chain differentiation!

$$* \left(\frac{\partial p}{\partial T}\right)_V \left(\frac{\partial T}{\partial V}\right)_P \left(\frac{\partial V}{\partial p}\right)_T = -1 \Rightarrow \boxed{\left(\frac{\partial p}{\partial T}\right)_V = - \frac{(\partial V/\partial T)_P}{(\partial V/\partial p)_T} = \frac{\alpha_P}{\alpha_T}}$$

$$* TdS = c_v dT + T \left(\frac{\partial p}{\partial T}\right)_V dV$$

$$dS=0 \Rightarrow c_v = -T \left(\frac{\partial p}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_S$$

$$* TdS = c_p dT - T \left(\frac{\partial V}{\partial T}\right)_P dp$$

$$dS=0 \Rightarrow c_p = T \left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial p}{\partial T}\right)_S$$

$$\frac{c_p}{c_v} = \frac{\left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial p}{\partial T}\right)_S}{-\left(\frac{\partial p}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_S} = \frac{(\partial V/\partial p)_T}{(\partial V/\partial p)_S} = \frac{\alpha_T}{\alpha_S}$$

$$-\left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial T}{\partial p}\right)_V$$

$$\left(\frac{\partial p}{\partial T}\right)_S \left(\frac{\partial T}{\partial V}\right)_S = \left(\frac{\partial p}{\partial V}\right)_S$$

$P=P(T,S)$   $T=T(V,S)$  here chain rule  
(same variable S is kept fixed)  
 $P=P(V,S) = P(T(V,S), S)$

$$\frac{1}{\left(\frac{\partial p}{\partial V}\right)_T} = \left(\frac{\partial V}{\partial p}\right)_T$$

$$* (c_p - c_v) dT - T \left(\frac{\partial p}{\partial T}\right)_V dV - T \left(\frac{\partial V}{\partial T}\right)_P dp = 0$$

$$\left(\frac{\partial T}{\partial V}\right)_P dV + \left(\frac{\partial T}{\partial p}\right)_V dp$$

$$\Rightarrow (c_p - c_v) \left(\frac{\partial T}{\partial V}\right)_P = T \left(\frac{\partial p}{\partial T}\right)_V = T \frac{\alpha_P}{\alpha_T}$$

$$\left(\frac{\partial T}{\partial p}\right)_V = T \left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial p}{\partial T}\right)_S$$

- not an indep. equation since  $\left(\frac{\partial T}{\partial p}\right)_V = \left(\frac{\partial p}{\partial T}\right)_V^{-1}$  etc

$$\boxed{(c_p - c_v) = T \frac{\alpha_P}{\alpha_T} \left(\frac{\partial V}{\partial T}\right)_P = T \cdot V \frac{\alpha_P^2}{\alpha_T}}$$

- function of equation of state

$\alpha_P$  &  $\alpha_T$  - obtained from equation of state.

$$TdS = \delta Q = dU + pdV = \left(\frac{\partial U}{\partial T}\right)_V dT + \underbrace{\left(\left(\frac{\partial U}{\partial V}\right)_T + p\right)}_{T\left(\frac{\partial p}{\partial T}\right)_V} dV$$

Response functions:

Specific heats

$$C_V \equiv T\left(\frac{\partial S}{\partial T}\right)_V = \left(\frac{\partial U}{\partial T}\right)_V \quad - \text{at const. } V$$

$$C_P \equiv T\left(\frac{\partial S}{\partial T}\right)_P = \left(\frac{\partial H}{\partial T}\right)_P \quad - \text{at const. } P$$

Thermal expansion coeff. at constant p

$$\alpha_P \equiv \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P$$

Compressibilities:

$$\kappa_T \equiv -\frac{1}{V} \left(\frac{\partial V}{\partial p}\right)_T \quad - \text{isothermal compressibility}$$

$$\kappa_S \equiv -\frac{1}{V} \left(\frac{\partial V}{\partial p}\right)_S \quad - \text{adiabatic compressibility.}$$

Theorem:

Of the 5 response functions  $C_V, C_P, \alpha_P, \kappa_T, \kappa_S$ , only 3 are independent (e.g.  $C_V, \alpha_P, \kappa_T$ ):

$$\otimes \quad C_P = \left(\frac{\partial U}{\partial T}\right)_V + T\left(\frac{\partial p}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_P = C_V + T\left(\frac{\partial p}{\partial T}\right)_V \underbrace{\left(\frac{\partial V}{\partial T}\right)_P}_{V \cdot \alpha_P}$$

$$\text{Use } \left(\frac{\partial p}{\partial T}\right)_V \left(\frac{\partial T}{\partial V}\right)_P \left(\frac{\partial V}{\partial p}\right)_T = -1$$

$$\Rightarrow \left(\frac{\partial p}{\partial T}\right)_V = -\frac{1}{\left(\frac{\partial T}{\partial V}\right)_P \left(\frac{\partial V}{\partial p}\right)_T} = -\frac{\left(\frac{\partial V}{\partial T}\right)_P}{\left(\frac{\partial V}{\partial p}\right)_T} = \frac{\alpha_P}{\kappa_T}$$

$$\Rightarrow \boxed{C_P = C_V + T \cdot V \cdot \frac{\alpha_P^2}{\kappa_T}}$$

$$\otimes \quad \frac{c_p}{c_v} = \frac{\left(\frac{\partial S}{\partial T}\right)_p}{\left(\frac{\partial S}{\partial T}\right)_v}$$

$$\text{Use } \left(\frac{\partial S}{\partial T}\right)_p \left(\frac{\partial T}{\partial p}\right)_s \left(\frac{\partial p}{\partial S}\right)_T = -1$$

$$\left(\frac{\partial S}{\partial T}\right)_v \left(\frac{\partial T}{\partial v}\right)_s \left(\frac{\partial v}{\partial S}\right)_T = -1$$

$$\frac{c_p}{c_v} = \frac{\left(\frac{\partial T}{\partial v}\right)_s \left(\frac{\partial v}{\partial S}\right)_T}{\left(\frac{\partial T}{\partial p}\right)_s \left(\frac{\partial p}{\partial S}\right)_T} = \frac{\left(\frac{\partial v}{\partial S}\right)_T \left(\frac{\partial S}{\partial p}\right)_T}{\left(\frac{\partial v}{\partial T}\right)_s \left(\frac{\partial T}{\partial p}\right)_s} = \frac{\left(\frac{\partial v}{\partial p}\right)_T}{\left(\frac{\partial v}{\partial p}\right)_s}$$

Here chain rule, e.s.

$$\left(\frac{\partial v}{\partial S}\right)_T \cdot \left(\frac{\partial S}{\partial p}\right)_T = \left(\frac{\partial v}{\partial p}\right)_T \quad \text{since } T \text{ is kept fixed}$$

$$V(p, T) = V(S(p, T), T)$$

$$\boxed{\frac{c_p}{c_v} = \frac{\alpha_T}{\alpha_S}}$$

Application (example): ideal gas

$$pV = Nk_B T$$

$$V = \frac{Nk_B T}{p}$$

$$\alpha_T = -\frac{1}{V} \left(\frac{\partial V}{\partial p}\right)_T = \frac{1}{p}$$

Invert: for isothermal process,  $-\frac{dV}{V \cdot dp} = \frac{1}{p}$ ,  $\frac{dV}{V} + \frac{dp}{p} = 0$

$$d(\ln V + \ln p) = 0 \Rightarrow \boxed{V \cdot p = \text{const}} \text{ - isotherm}$$



Adiabatic process assume  $\frac{c_p}{c_v} = \gamma = \text{const}$

$$\alpha_s = \frac{\alpha_T}{\gamma} = \frac{1}{\gamma} \cdot \frac{1}{P}$$

$$-\frac{1}{V} \frac{dV}{dp} = \frac{1}{\gamma} \cdot \frac{1}{P}, \quad \gamma \frac{dV}{V} + \frac{dp}{P} = 0, \quad pV^\gamma = \text{const}$$

adiabat

Appearance of  $\gamma = \frac{c_p}{c_v}$  is more "fundamental" than coincidence, since for any substance

$$\frac{\alpha_T}{\alpha_s} = \gamma = \frac{c_p}{c_v}$$

Remark:  $\alpha_p, \alpha_T$  are determined entirely by the equation of state  $V = V(p, T)$ . Conversely, if we know  $\alpha_p, \alpha_T$ , we can recover the equation of state.

Since  $c_v$  & equation of state  $\Rightarrow$  full thermodynamics, it is not surprising that we can express  $c_p, \alpha_s$  in terms of  $c_v, \alpha_p, \alpha_T$ . The above treatment provides concise such expressions.