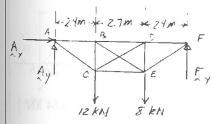


PROBLEM 6.64

The diagonal members in the center panel of the truss shown are very slender and can act only in tension; such members are known as *counters*. Determine the force in members BD and CE and in the counter which is acting when P = 12 kN.

SOLUTION

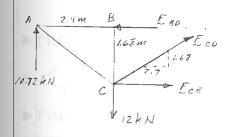
FBD Truss:



$$\Sigma F_x = 0$$
: $\mathbf{A}_x = 0$
 $(\Sigma M_F = 0)$: $(2.4 \text{ m})(8 \text{ kN}) + (5.1 \text{ m})(12 \text{ kN})$
 $-(7.5 \text{ m})A_y = 0$, $\mathbf{A}_y = 10.72 \text{ kN}$

Since only CD can provide an upward force necessary for equilibrium, it must be in tension, and $F_{\rm BF}=0$

FBD Section ABC:



$$\uparrow \Sigma F_y = 0: \quad 10.72 \text{ kN} - 12 \text{ kN} + \frac{1.68}{3.18} F_{CD} = 0$$

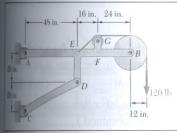
$$F_{CD} = 2.4229 \text{ kN}, \qquad F_{CD} = 2.42 \text{ kN T} \blacktriangleleft$$

$$(\Sigma M_C = 0: \quad (1.68 \text{ m}) F_{BD} - (2.4 \text{ m}) (10.72 \text{ kN}) = 0$$

$$F_{BD} = 15.3143 \text{ kN}, \qquad F_{BD} = 15.31 \text{ kN C} \blacktriangleleft$$

$$\Sigma F_x = 0: \quad F_{CE} + \frac{2.7}{3.18} (2.4229 \text{ kN}) - 15.3143 \text{ kN} = 0$$

 $F_{CE} = 13.26 \text{ kN T} \blacktriangleleft$

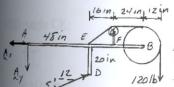


Neglecting the size of the pulley at G, (a) draw the shear and bendingmoment diagrams for the beam AB, (b) determine the maximum absolute values of the shear and bending moment.

SOLUTION

FBD AB + Pulley & Cord:

$$\left(\sum \Delta M_A = 0: (48 \text{ in.}) \left(\frac{5}{13}D\right) + (20 \text{ in.}) \left(\frac{12}{13}D\right) - (100 \text{ in.})(120 \text{ lb}) = 0$$



$$\mathbf{D} = 325 \text{ lb} / \text{so } \mathbf{D}_x = 300 \text{ lb} \longrightarrow, \ \mathbf{D}_y = 125 \text{ lb} \dagger$$

$$\uparrow \Sigma F_y = 0$$
: $-A_y + 125 \text{ lb} - 120 \text{ lb} = 0$ $A_y = 5 \text{ lb} \downarrow$

Neglecting the diameter of pulley G, the cord EG has slope 3/4,

and tension 120 lb,
$$\mathbf{E}_x = 96 \text{ lb} \longrightarrow$$
, $\mathbf{E}_y = 72 \text{ lb}$

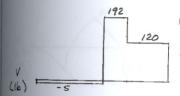
$$\mathbf{E}_y = 72 \text{ lb} \uparrow$$

Beam AB with forces at D and G replaced by forces and couples at Eand F. Horizontal forces are omitted to avoid clutter.

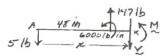




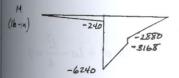
Along AE:
$$SIb = V = 0$$
, $V = -5 \text{ lb}$



$$\sum M_J = 0$$
: $x(5 \text{ lb}) + M = 0$, $M = (-5 \text{ lb})x$



$$^{\uparrow} \Sigma F_{v} = 0$$
: $-5 \text{ lb} + 197 \text{ lb} - V = 0$, $V = 192 \text{ lb}$



$$\sum M_K = 0$$
: $M + 6000 \text{ lb · in.} + x(5 \text{ lb}) - (x - 48 \text{ in.})(197 \text{ lb}) = 0$

 $M = (192 \text{ lb})x - 15456 \text{ lb} \cdot \text{in}.$

Along FB:

$$\Sigma F_{y} = 0: \quad V - 120 \text{ lb} = 0, \quad V = 120 \text{ lb}$$

$$\Sigma M_{L} = 0: \quad -M - x_{1}(120 \text{ lb}) = 0$$

$$M = -(120 \text{ lb}) x_{1}$$

$$\sum M_L = 0$$
: $-M - x_1(120 \text{ lb}) = 0$

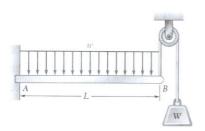
$$M = -(120 \text{ lb})x_1$$

From diagrams,

$$|V|_{\text{max}} = 192.0 \text{ lb along } EF \blacktriangleleft$$

$$|M|_{\text{max}} = 6240 \text{ lb} \cdot \text{in.} = 520 \text{ lb} \cdot \text{ft at } E \blacktriangleleft$$

PROPRIETARY MATERIAL. © 2007 The McGraw-Hill Companies, Inc. All rights reserved. No part of this Manual may be displayed, reproduced a distributed in any form or by any means, without the prior written permission of the publisher, or used beyond the limited distribution to teachers and abeators permitted by McGraw-Hill for their individual course preparation. If you are a student using this Manual, you are using it without permission.



In order to reduce the bending moment in the cantilever beam AB, a cable and counterweight are permanently attached at end B. Determine the magnitude of the counterweight for which the maximum absolute value of the bending moment in the beam is as small as possible and the corresponding value of $|M|_{max}$. Consider (a) the case when the distributed load is permanently applied to the beam, (b) the more general case when the distributed load may either be applied or removed.

SOLUTION

M due to distributed load:

M due to counter weight:



$$\sum M_J = 0: -M - \frac{x}{2}wx = 0$$

$$M = -\frac{1}{2}wx^2$$

$$\sum M_J = 0: -M + xw = 0$$

$$M = wx$$



$$M = W_x - \frac{w}{2}x^2$$

$$M = W_x - \frac{w}{2}x^2$$

$$\frac{dM}{dx} = W - wx = 0 \text{ at } x = \frac{W}{w}$$

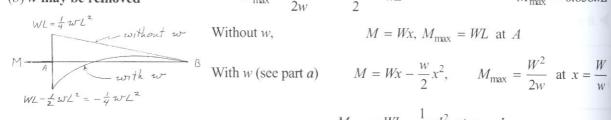
And here $M = \frac{W^2}{2w} > 0$ so M_{max} ; M_{min} must be at x = L

So $M_{\min} = WL - \frac{1}{2}wL^2$. For minimum $|M|_{\max}$ set $M_{\max} = -M_{\min}$, so

$$\frac{W^2}{2w} = -WL + \frac{1}{2}wL^2 \text{ or } W^2 + 2wLW - w^2L^2 = 0$$

$$W = -wL \pm \sqrt{2w^2L^2} \text{ (need +)}$$
 $W = (\sqrt{2} - 1)wL = 0.414wL \blacktriangleleft$

(b) w may be removed



$$M_{\text{max}} = \frac{W^2}{2w} = \frac{\left(\sqrt{2} - 1\right)^2}{2} wL^2$$

$$M = Wx M = WI$$
 at

$$M = Wx - \frac{w}{2}x^2,$$

$$M_{\text{max}} = \frac{W^2}{2w}$$
 at $x = \frac{W}{w}$

 $M_{\rm max} = 0.858wL^2$

$$M_{\min} = WL - \frac{1}{2}wL^2$$
 at $x = L$

PROPRIETARY MATERIAL. © 2007 The McGraw-Hill Companies, Inc. All rights reserved. No part of this Manual may be displayed, reproduced or distributed in any form or by any means, without the prior written permission of the publisher, or used beyond the limited distribution to teachers and educators permitted by McGraw-Hill for their individual course preparation. If you are a student using this Manual, you are using it without permission.

PROBLEM 7.57 CONTINUED

For minimum M_{max} , set M_{max} (no w) = $-M_{\text{min}}$ (with w)

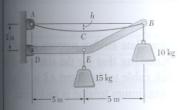
$$WL = -WL + \frac{1}{2}wL^2 \rightarrow W = \frac{1}{4}wL \rightarrow$$

$$M_{\rm max} = \frac{1}{4}wL^2 \blacktriangleleft$$

With

$$W = \frac{1}{4}wL \blacktriangleleft$$

PROPRIETARY MATERIAL. © 2007 The McGraw-Hill Companies, Inc. All rights reserved. No part of this Manual may be displayed, reproduced a distributed in any form or by any means, without the prior written permission of the publisher, or used beyond the limited distribution to teachers and aducators permitted by McGraw-Hill for their individual course preparation. If you are a student using this Manual, you are using it without permission.



The total mass of cable ACB is 10 kg. Assuming that the mass of the cable is distributed uniformly along the horizontal, determine (a) the sag h, (b) the slope of the cable at A.

SOLUTION

FBD whole:

$$\sum M_D = 0$$
: $(2m)T_{Ax} - (5m)(98.1 + 147.15) N = 0$

 $T_{Ax} = 1103.6 \text{ N}$

FBD half-cable:

$$ightharpoonup \Sigma F_x = 0: \quad T_0 - T_{Ax} = 0, \quad T_0 = 1103.6 \text{ N}$$

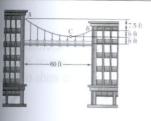
$$\Sigma F_y = 0$$
: $T_{Ay} = 49.05 \text{ N} = 0$, $T_{Ay} = 49.05 \text{ N}$

$$\Sigma F_y = 0$$
: $T_{Ay} = 49.05 \text{ N} = 0$, $T_{Ay} = 49.05 \text{ N}$
 $\Sigma M_A = 0$: $h(1103.6 \text{ N}) - (2.5 \text{ m})(49.05 \text{ N}) = 0$

$$h = 0.11111 \text{ m}$$

$$h = 111.1 \text{ mm}$$

(b)
$$\theta = \tan^{-1} \frac{T_{Ay}}{T_{Ax}} = \tan^{-1} \frac{49.05}{1103.6} = 2.5449^{\circ}, \quad \theta = 2.54^{\circ}$$

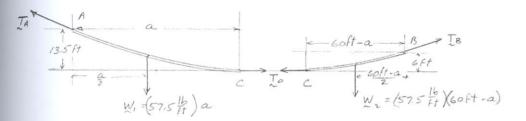


A steam pipe weighting 50 lb/ft that passes between two buildings 60 ft apart and is supported by a system of cables as shown. Assuming that the weight of the cable is equivalent to a uniformly distributed loading of 7.5 lb/ft, determine (a) the location of the lowest point C of the cable, (b) the maximum tension in the cable.

UTION

AC:

FBD CB:



$$(\Sigma M_A = 0: (13.5 \text{ ft})T_0 - \frac{a}{2}(57.5 \text{ lb/ft})a = 0$$

$$T_0 = (2.12963 \text{ lb/ft}^2)a^2$$
 (1)

$$\sum M_B = 0$$
: $\frac{60 \text{ ft} - a}{2} (57.5 \text{ lb/ft}) (60 \text{ ft} - a) - (6 \text{ ft}) T_0 = 0$

$$6T_0 = (28.75 \text{ lb/ft}^2) [3600 \text{ ft}^2 - (120 \text{ ft})a + a^2]$$
(2)

Using (1) in (2), $0.55a^2 - (120 \text{ ft})a + 3600 \text{ ft}^2 = 0$

Solving: $a = (108 \pm 72)$ ft, a = 36 ft (180 ft out of range)

So

C is 36 ft from A

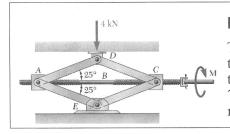
(a)
$$C ext{ is 6 ft below and 24 ft left of } B ext{ } \blacksquare$$

$$T_0 = 2.1296 \text{ lb/ft}^2 (36 \text{ ft})^2 = 2760 \text{ lb}$$

$$W_1 = (57.5 \text{ lb/ft})(36 \text{ ft}) = 2070 \text{ lb}$$

(b)
$$T_{\text{max}} = T_A = \sqrt{T_0^2 + W_1^2} = \sqrt{(2760 \text{ lb})^2 + (2070 \text{ lb})^2} = 3450 \text{ lb} \blacktriangleleft$$

ARY MATERIAL. © 2007 The McGraw-Hill Companies, Inc. All rights reserved. No part of this Manual may be displayed, reproduced in any form or by any means, without the prior written permission of the publisher, or used beyond the limited distribution to teachers and rmitted by McGraw-Hill for their individual course preparation. If you are a student using this Manual, you are using it without permission.

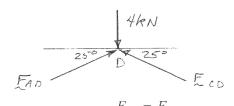


PROBLEM 8.70

The position of the automobile jack shown is controlled by a screw *ABC* that is single-threaded at each end (right-handed thread at *A*, left-handed thread at *C*). Each thread has a pitch of 2 mm and a mean diameter of 7.5 mm. If the coefficient of static friction is 0.15, determine the magnitude of the couple **M** that must be applied to raise the automobile.

SOLUTION

FBD joint D:

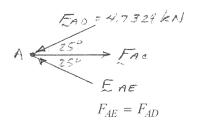


By symmetry:

$$\uparrow \Sigma F_y = 0: \quad 2F_{AD}\sin 25^\circ - 4 \text{ kN} = 0$$

$$F_{AD} = F_{CD} = 4.7324 \text{ kN}$$

FBD joint A:

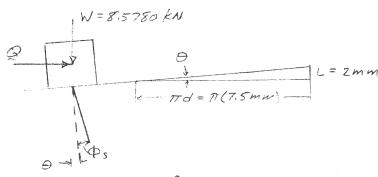


By symmetry:

$$\rightarrow \Sigma F_x = 0$$
: $F_{AC} - 2(4.7324 \text{ kN})\cos 25^\circ = 0$

$$F_{AC} = 8.5780 \text{ kN}$$

Block and incline A:



$$\theta = \tan^{-1} \frac{2 \text{ mm}}{\pi (7.5 \text{ mm})} = 4.8518^{\circ}$$

$$\phi_s = \tan^{-1} \mu_s = \tan^{-1} 0.15 = 8.5308^{\circ}$$

PROBLEM 8.70 CONTINUED

$$R$$
 $Q = (8.578 \text{ kN}) \tan(13.3826^{\circ})$

$$= 2.0408 \, kN$$

$$M_A = rQ$$

$$= rQ$$

$$= \left(\frac{7.5}{2} \text{ mm}\right) (2.0408 \text{ kN})$$

$$= 7.653 \, \text{N} \cdot \text{m}$$

$$= 7.033 \text{ N} \cdot \text{III}$$
where C and C and C are C and C are C are C are C and C are C are C and C are C are C and C are C are C and C ar

By symmetry: Couple at
$$C$$
: $M_C = 7.653 \text{ N} \cdot \text{m}$

Couple at *A*:

Total couple
$$M = 2(7.653 \text{ N} \cdot \text{m})$$

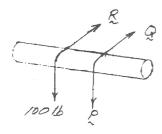


PROBLEM 8.106

Knowing that the coefficient of static friction is 0.30 between the rope and the horizontal pipe and that the smallest value of P for which equilibrium is maintained is 20 lb, determine (a) the largest value of P for which equilibrium is maintained, (b) the coefficient of static friction between the rope and the vertical pipe.

SOLUTION

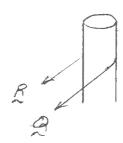
Horizontal pipe



Contact angles
$$\beta_H = \frac{\pi}{2}$$

$$\mu_{sH} = 0.30$$

Vertical pipe



Contact angle
$$\beta_V = \pi$$

$$\mu_{eV} = ?$$

For P_{\min} , the 100 lb force impends downward, and

100 lb =
$$\left(e^{\mu_{sH}\frac{\pi}{2}}\right)R = \left(e^{\mu_{sH}\frac{\pi}{2}}\right)\left(e^{\mu_{sV}\pi}\right)Q = \left(e^{\mu_{s\pi}\frac{\pi}{2}}\right)\left(e^{\mu_{sV}\pi}\right)\left(e^{\mu_{sH}\frac{\pi}{2}}\right)P$$

100 lb = $\left[e^{\pi(0.30 + \mu_{sV})}\right]$ (20 lb), so $e^{\pi(0.30 + \mu_{sV})} = 5$

- (a) For P_{max} the force **P** impends downward, and the ratios are reversed, so $P_{\text{max}} = 5(100 \text{ lb}) = 500 \text{ lb}$
- (b) $\pi(0.30 + \mu_{sV}) = \ln 5$

$$\mu_{sV} = \frac{1}{\pi} \ln 5 - 0.30 = 0.21230$$

 $\mu_{sV} = 0.212$

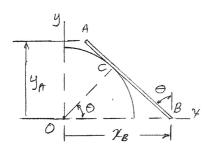
C θ B

PROBLEM 10.26

A slender rod of length l is attached to a collar at B and rests on a portion of a circular cylinder of radius r. Neglecting the effect of friction, determine the value of θ corresponding to the equilibrium position of the mechanism when l=14 in., r=5 in., P=75 lb, and Q=150 lb.

OC = r

SOLUTION



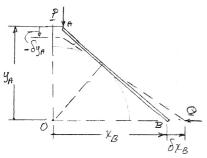
Geometry

$$\cos \theta = \frac{OC}{OB} = \frac{r}{x_B}$$

$$x_B = \frac{r}{\cos \theta}$$

$$\delta x_B = \frac{r \sin \theta}{\cos^2 \theta} \delta \theta$$

$$y_A = l \cos \theta; \qquad \delta y_A = -l \sin \theta \delta \theta$$



Virtual Work:

$$\delta U = 0: \quad P(-\delta y_A) - Q\delta x_B = 0$$

$$Pl\sin\theta \,\delta\theta - Q\frac{r\sin\theta}{\cos^2\theta} \,\delta\theta = 0$$

$$\cos^2\theta = \frac{Qr}{Pl} \tag{1}$$

Then, with l = 14 in., r = 5 in., P = 75 lb, and Q = 150 lb

$$\cos^2 \theta = \frac{(150 \text{ lb})(5 \text{ in.})}{(75 \text{ lb})(14 \text{ in.})} = 0.7143$$

or

$$\theta = 32.3115^{\circ}$$

 $\theta = 32.3^{\circ}$